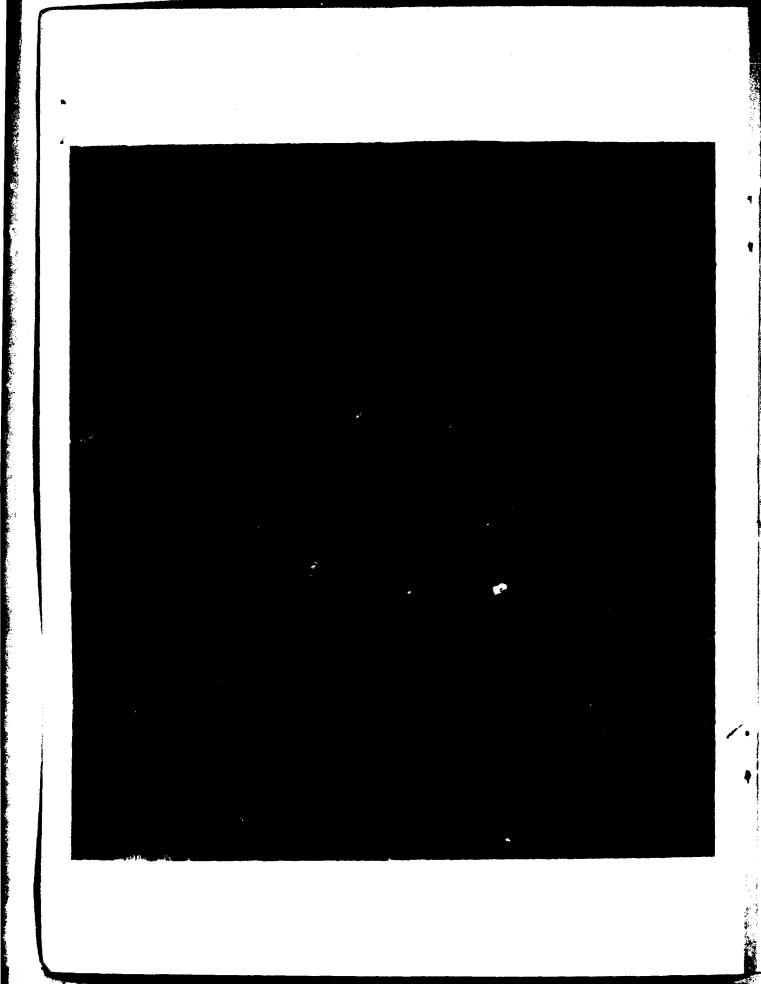


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1982 ANNUAL TROPICAL CYCLONE REPORT "ERRATA"

1. Substitute the following table for TABLE 2-4, on page 8.

TABLE 2-4. FIX PLATFORM	SUMMARY FOR	1982			
	FIX	PLATFORM SUMM	ARY	-	
WESTERN NORTH PACIFIC	AIRCRAFT	SATELLITE	RADAR	SYNOPTIC	TOTAL
TS MAMIE	7	68	.3		78
TY NELSON TY ODESSA	25 15	105	11		141 70
TY PAT	16	55 52	6	1	75
TY RUBY	15	63			78
TS TESS		40		8	48
ts skip ts val	5 2	24 14		1 4	30 20
TS WINONA	11	72			97
TY ANDY	16	82	14 38	7	143
STY BESS	30	101	4	4	139
TY CECIL TY DOT	16 23	86 66	92 3	3 2 3	197 94
TY ELLIS	23 24	87	64	3	178
TY FAYE	27	133	41	3	204
TY GORDON	36	90		4	126
TS HOPE	13	26	2 59	4	33 188
TY IRVING TY JUDY	26	109 68	10	7 5	109
TY KEN	33	84	32	3	152
TS LOLA		28			28
TD 22 STY MAC	2 32	10	35		12 140
TY NANCY	19	73 80	14	2	115
TD 25	i .	15			16
	27 .	128			155
TY PAMELA	44	160	22 25	3 3	229 75
TY ROGER	, 	44		J 	//
TOTAL	469	1963	475	63	2970
% OF TOTAL NR OF FIXES	15.8	66.1	16.0	· 2.1	100.0
INDIAN OCEAN		SATELLITE		SYNOPTIC	TOTAL
TC 20-82		46			46
TC 22-82		31			31
TC 23-82 TC 24-82		29 6		1	29 7
TC 25-82		10		i	14
TOTAL		122		5	127
% OF TOTAL NR OF FIXES		96.1	•	3.9	100.0

<sup>2.</sup> Page 140, TABLE 4-4. 24-hour posit error for ALL FORECASTS is missing, insert "138".

1.

# U.S. NAVAL OCEANOGRAPHY COMMAND CENTER JOINT TYPHOON WARNING CENTER COMNAVMARIANAS BOX 17 FPO SAN FRANCISCO 98630

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\*Transferred during 1982

# **FOREWORD**

The Annual Tropical Cyclone Report is prepared by the staff of the Joint Typhoon Warning Center (JTWC), a combined USAF/USN organization operating under the command of the Commanding Officer, U.S. Naval Oceanography Command Center/Joint Typhoon Warning Center, Guam. JTWC was established in April 1959 when CINCPAC directed CINCPACFLT to provide a single tropical cyclone warning center for the western North Pacific region. The operations of JTWC are guided by CINCPACINST 3140.1 (series).

The mission of the Joint Typhoon Warning Center is multi-faceted and includes:

- 1. Continuous meteorological monitoring of all tropical activity in the Northern and Southern Hemispheres, from 180 degrees longitude westward to the east coast of Africa, to anticipate tropical cyclone development.
- 2. Issuing warnings for all significant tropical cyclones in the above area of responsibility.
- Determination or reconnaissance requirements for tropical cyclone surveillance and assignment of appropriate priorities.
- 4. In depth post-storm analysis of all tropical cyclones occurring within the western North Pacific and North Indian Oceans for publication in this report.
- 5. Cooperation with the Naval Environmental Prediction Research Facility (NEPRF), Monterey, California, on the operation evaluation of tropical cyclone models and forecast aids, and the development of new techniques to support operational forecast scenarios.

Should JTWC become incapacitated, the Alternate JTWC (AJTWC), located at the U.S. Naval Western Oceanography Center, Pearl Harbor, Hawaii, assumes warning responsibilities. Assistance in determining satellite reconnaissance requirements, and in

obtaining the resultant data, is provided by Letachment 4, lWW, Hickman AFB, Hawaii.

Satellite imagery used throughout this report represents data obtained by the tropical cyclone satellite surveillance network. The personnel of Det 1, lww, colocated with JTWC at Nimitz Hill, Guam, coordinate the satellite acquisitions and tropical cyclone surveillance by the following units:

Det 5, lww, Clark AB, RP
Det 8, lww, Kadena AB, Japan
Det 15, 30wS, Osan AB, Korea
Det 4, lww, Hickam AFB, Hawaii
Air Force Global Weather Center,
Offutt AFB, Nebraska

In addition, the Naval Oceanography Command Detachment, Diego Garcia, and DMSP equipped U.S. Navy aircraft carriers have been instrumental in providing vital satellite position fixes of tropical disturbances in the Indian Ocean.

In line with the proposals to implement metric units of measurements within the United States over the next few years, various civilian and military organizations have begun extensive educational programs through use of metric equivalents in their publications. This report will include metric unit equivalent measures whenever possible.

A special thanks is extended to the men and women of: 27th Communication Squadron, Operating Location C, for their continuing support by providing high quality, real-time satellite imagery; the Pacific Fleet Audio-Visual Center, Guam, for their assistance in the reproduction of satellite and graphics data for this report; to the Navy Publications and Printing Service Branch Office, Guam, for their efforts to meet publication deadlines; and to Mrs. Cynthia Blevins for her patience and perseverance in typing the many drafts and the final manuscript of the report.



NOTE: Appendix 5 contains information on how to obtain past issues of the Annual Typhoon Report (redesignated Annual Tropical Cyclone Report in 1980).

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# CHAPTER I - OPERATIONAL PROCEDURES

### 1. GENERAL

The Joint Typhoon Warning Center (JTWC) provides a variety of routine services to the organizations within its area of responsibility, including:

- Significant Tropical Weather Advisories: issued daily, this product describes all tropical disturbances and assesses their potential for further development;
- Tropical Cyclone Formation Alerts: issued when synoptic, satellite and/or aircraft reconnaissance data indicate development of a significant tropical cyclone in a specified area is likely;
- Tropical Cyclone Warnings: issued periodically throughout each day for significant tropical cyclones, giving forecasts of position and intensity of the system; and
- Prognostic Reasoning Message: issued twice daily for tropical storms and typhoons in the western North Pacific; these messages discuss the rationale behind the most recent warnings.

The recipients of the services of JTWC essentially determine the content of JTWC's products according to their ever-changing requirements. Thus, the spectrum of the routine services is subject to change from year to year; such changes are usually the result of deliberations held at the Annual Tropical Cyclone Conference.

### 2. DATA SOURCES

### a. COMPUTER PRODUCTS:

A standard array of synoptic-scale computer analyses and prognostic charts are available from the Fleet Numerical Oceanography Center (FNOC) at Monterey, California. These products are provided via the Naval Environmental Data Network (NEDN).

### b. CONVENTIONAL DATA:

This data set is comprised of landbased and shipboard surface and upper-air observations taken at or near synoptic times, cloud-motion winds derived twice daily from satellite data, and enroute meteorological observations from commercial and military aircraft (AIREPS) within six hours of synoptic times. Conventional data charts are prepared daily at 0000Z and 1200Z using hand- and computer-plotted data for the surface/gradient, 500 mb (mid-tropospheric), and 200 mb (upper-tropospheric) levels. In addition to these charts, a 700 mb (lower-tropospheric) chart is computerplotted from rawinsonde/pibal observations received at FNOC for the 12-hour synoptic times.

### c. AIRCRAFT RECONNAISSANCE:

Aircraft weather reconnaissance data are invaluable for the position of the center of developing systems and essential for the accurate determination of numerous parameters, including:

- eye/center temperature and dewpoint maximum surface and flight level wind
- minimum sea level pressure
   horizontal wind distribution

In addition, wind and pressure-height data at the 500 and/or 400 mb level, provided by the aircraft while enroute to, or from fix missions, provide a valuable supplement to the all too sparse data fields of JTWC's area of responsibility. A comprehensive discussion of aircraft weather reconnaissance is presented in Chapter II.

#### d. SATELLITE RECONNAISSANCE:

Meteorological satellite data obtained rom Defense Meteorological Satellite data obtained from Defense Meteorological Satellite Program (DMSP), and National Oceanic and Atmospheric Administration (NOAA), space-craft played a major role in the early detection and tracking of tropical cyclones in 1982. A discussion of the role of these programs is presented in Chapter II.

### e. RADAR RECONNAISSANCE:

During 1982, as in previous years, land radar coverage was utilized extensively when available. Once a tropical cyclone moved within the range of land radar sites, their reports were essential for determination of small scale movement. Use of radar reports during 1982 is discussed in Chapter II.

### 3. COMMUNICATIONS

- JTWC currently has access to three primary communications circuits.
- (1) The Automated Digital Network (AUTODIN) is used for dissemination of warnings and other related bulletins to Department of Defense installations. These messages are relayed for further transmission over U.S. Navy Fleet Broadcasts, and U.S. Coast Guard CW (continuous wave Morse code) and voice broadcasts. Inbound message traffic for JTWC is received via AUTODIN addressed to NAVOCEANCONCEN GUAM or JTWC GUAM.
- The Air Force Automated Weather Network (AWN) provides weather data to JTWC through a dedicated circuit from the Automated Digital Weather Switch (ADWS) at Hickam AFB, Hawaii. The ADWS selects and routes the large volume of meteorological reports necessary to satisfy JTWC requirements for the right data at the right time. Weather bulletins prepared by JTWC are inserted into the AWN circuit via the NEDS and the Nimitz Hill Naval Telecommunication Center (NTCC) of the Naval Communications Area Master Station Western Pacific.
- (3) The Naval Environmental Data Network (NEDN) is the communications link with the computers at FNOC. JTWC is able to receive environmental data from FNOC and access the computers directly to run various programs.

b. The Naval Environmental Display Station (NEDS) has become the backbone of the JTWC communications system; it is the terminal that provides a direct interface with the NEDN and AWN; and it is capable of preparing messages for indirect AUTODIN transmission. The NEDS also provides a means for the Typhoon Duty Officer (TDO) to request forecast aids which are processed on the FNOC computers and transmitted to the TDO over the NEDN circuit.

### 4. ANALYSES

A composite surface/gradient level (3000 ft (915 m)) manual analysis of the JTWC area of responsibility is accomplished on the 00002 and 12002 conventional data. Analysis of the wind field using streamlines is stressed for tropical and subtropical regions. Analysis of the pressure field is accomplished routinely by the Naval Oceanography Command Center (NOCC) Operations watch-team and may be used in conjunction with JTWC's analysis of tropical wind fields.

Manual streamline analysis of the 500 mb level is accomplished on the 0000z and 1200z data. This analysis is used to delineate the mid-tropospheric steering currents, which can be extremely important to the tropical cyclone forecast.

A composite upper-tropospheric manual streamline analysis is accomplished daily utilizing rawinsonde data from 300 mb through 100 mb, winds derived from cloud motion analysis, and AIREPS (plus or minus 6 hours) at or above 29,000 feet (8,839 m). Wind and height data are used to arrive at a representative analysis of tropical cyclone outflow patterns, mid-latitude steering currents, and features that may influence tropical cyclone intensity. All charts are hand-plotted over areas of tropical cyclone activity to provide all available data as soon as possible to the TDO. These charts are augmented by the computer-plotted charts for the final analysis.

A 700 mb computer-plotted chart is available for streamline or height-change analysis from the 0000Z and 1200Z data base. Additional sectional charts at intermediate synoptic times and auxiliary charts such as station-time plot diagrams and pressure-change charts are also analyzed during periods of significant tropical cyclone activity.

### 5. FORECAST AIDS

The following objective techniques were employed in tropical cyclone forecasting during 1982 (a description of these techniques is presented in Chapter IV):

### a. MOVEMENT

- (1) 12-HR EXTRAPOLATION
- (2) CLIMATOLOGY
- (3) HPAC (Extrapolation/Climatology)
- (4) BPAC (Extrapolation/Climatology)
- (5) CYCLOPS (Steering)
- (6) TYAN78 (Analog)

- (7) ONE-WAY TROPICAL CYCLONE MODEL (Dynamic)
- (8) NESTED TROPICAL CYCLONE MODEL (Dynamic)
- (9) TAPT (Empirical)

### b. INTENSITY

- (1) THETA E (Empirical)
- (2) WIND RADIUS (Analytical)

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(3) DVORAK (Empirical)

### 6. FORECAST PROCEDURES

#### a. INITIAL POSITIONING:

In the preparation of each warning an accurate location (fix) of the tropical cyclone's surface center within two to three hours of warning time is of prime importance. JTWC uses the Selective Reconnaissance Program (SRP) to levy an optimal mix of available resources to obtain the necessary fix information. Whenever a tropical cyclone is poorly defined or the actual surface center cannot be determined, and when conflicting fix information is received, the "best estimate" of the surface location is subjectively determined from the analysis of all available data. If the fix data are not available due to reconnaissance platform malfunctions or communication problems, synoptic data or extrapolation from previous fixes are used. The warning position is then obtained by determining the "best track" of the tropical cyclone up to the last fix, or best estimate of the position of its surface center, and forecasting its movement to the warning time.

### b. TRACK FORECASTING:

A preliminary forecast track is developed based on an evaluation of the rationale behind the previous warning and the guidance given by the most recent objective techniques and numerical prognoses. This preliminary track is subjectively modified based on the following considerations:

- (1) The prospects for recurvature or erratic movement are evaluated. This evaluation is based primarily on the present and forecast, positions and amplitudes of the middle-tropospheric, mid-latitude troughs as depicted on the latest upper air analyses and numerical prognoses.
- (2) Determination of the best steering level is partly influenced by the maturity and vertical extent of the tropical cyclone. For mature tropical cyclones located south of the subtropical ridge, forecast changes in speed of movement are closely correlated with anticipated changes in the intensity or relative position of the ridge. When steering currents are relatively weak, the tendency for tropical cyclones to move northward due to internal forces is an important consideration.
- (3) Over the 12- to 72-hour forecast period, speed of movement during the early forecast period is usually biased toward persistence, while the subsequent forecast periods are biased toward objective

techniques. When a tropical cyclone moves poleward, and toward the mid-latitude steering currents, speed of movement becomes increasingly more biased toward a selective group of objective techniques capable of estimating significant increases in speed of movement.

(4) The proximity of the tropical cyclone to other tropical cyclones is closely evaluated to determine if there is a possibility of a Fujiwhara interaction (the apparent rotation of two or more cyclones about a common axis or axes).

A final check is made against climatology to determine whether the forecast track is reasonable. If the forecast deviates greatly from one of the climatological tracks, the forecast rationale may be reappraised.

### c. INTENSITY FORECASTING:

In this parameter, heavy reliance is placed on intensity trends from aircraft reconnaissance reports, wind and pressure data from ships and land stations in the vicinity of the tropical cyclone, the Dvorak satellite interpretation model and other objective techniques. An evaluation of the entire synoptic situation is made, including the location of major troughs and ridges, the position and intensity of any nearby tropical upper-tropospheric troughs (TUTT), the vertical and horizontal extent of the tropical cyclone's circulation and the extent of the associated upper-level outflow pattern. An essential element affecting each intensity forecast is the accompanying forecast track and the influence of environmental parameters along that track, such as: sea thermal fronts, terrain influences, vertical wind shear, and an extratropical environment.

Once the forecast intensities have been derived, the horizontal distribution of destructive winds (greater than 30-, 50- and 100-knots) is determined. The most recent wind radii and associated asymmetries are deduced from all available surface wind observations and reconnaissance aircraft reports. Based on the current wind distribution, preliminary estimates of future wind radii are provided by an empirically derived objective technique. These estimates may be subjectively modified based on the anticipated interaction of the tropical cyclone's circulation with forecast locations of large-scale wind regimes and significant landmasses. Other factors including the tropical cyclone's speed of movement and possible extratropical transition are considered.

### .. WARNINGS

Tropical cyclone warnings are issued when a definite closed circulation is evident and maximum sustained surface winds are forecast to increase to 34 knots (18 meters per second) within 48 hours, or if the tropical cyclone is in such a position that life or property may be endangered within 72 hours. Warnings may also be issued in other situations if it is determined that there is a need to alert military or civil interests to conditions which may become hazardous in a short period of time.

Each tropical cyclone warning is numbered sequentially and includes the following information: the position of the surface center; estimate of the position accuracy and the supporting reconnaissance (fix) platforms; the direction and speed of movement in the past six hours; the intensity and radial extent of surface winds over 30-, 50-, and 100-knots, when applicable. At forecast intervals of 12-, 24-, 48- and 72-hours, information on the tropical cyclone's anticipated position, intensity and wind radii is also provided.

Warnings within the western North Pacific Occan are issued within two hours of 00002, 06002, 12002 and 18002 with the constraint that consecutive warnings may not be more than seven hours apart. Warnings in the North Indian Ocean are issued within two hours of 02002, 08002, 14002 and 20002, again with the constraint that consecutive warnings may not be more than seven hours apart. Warning forecast positions are verified against the corresponding "best track" positions. A summary of the verification results from 1982 is presented in Chapter IV.

As of 1 January 1980, JTWC issues tropical cyclone warnings in an Automated Data Processing (ADP) format. This formatted warning possesses readability for all users and allows activities with ADP equipment to enter tropical cyclone warning data directly into ADP equipment data bases.

### 8. PROGNOSTIC REASONING MESSAGE

For tropical storms and typhoons in the western North Pacific Ocean, prognostic reasoning messages are transmitted following the 0000Z and 1200Z warnings, or whenever the previous reasoning is no longer valid. This plain language message is intended to provide meteorologists with the reasoning behind the latest JTWC forecast.

Included in the prognostic reasoning message are confidence statements for the 24- and 48-hour forecast positions. These confidence values are percentage probabilities that forecast position errors will be less than 100 and 150 nm, and 200 and 300 nm for 24 and 48 hours, respectively. These probabilities are based on objective data from error analysis studies of past tropical cyclones and are a function of current position, initial forecast movement, intensity, and the number of tropical cyclones in warning status in the western North Pacific Ocean.

In addition to this message, prognostic reasoning information applicable to all customers is provided in the remarks section of warnings when significant forecast changes are made or when deemed appropriate by the TDO.

# 9. SIGNIFICANT TROPICAL WEATHER ADVISORY

This product contains a general, non-technical description of all tropical disturbances in the JTWC area of responsibility and an assessment of their potential for further (tropical cyclone) development. In addition, all tropical cyclones in warning status are briefly discussed. This message is issued by 0600Z daily and is reissued whenever the situation warrants.

# 10. TROPICAL CYCLONE FORMATION ALERT

Formation alerts are issued whenever interpretation of satellite imagery and other meteorological data indicates that the formation of a significant tropical cyclone is likely. These formation alerts will specify a valid period not to exceed 24 hours and must either be cancelled, reissued, or superseded by a tropical cyclone warning prior to the expiration of the valid time.

### **CHAPTER II - RECONNAISSANCE AND FIXES**

### 1. GENERAL

The Joint Typhoon Warning Center depends on reconnaissance to provide necessary, accurate, and timely meteorological information in support of each warning. JTWC relies primarily on three reconnaissance platforms: aircraft, satellite, and radar. In data rich areas synoptic data are also used to supplement the above. Optimum utilization of all available reconnaissance resources is obtained through the Selective Reconnaissance Program (SRP); various factors are considered in selecting a specific reconnaissance platform including capabilities and limitations, and the tropical cyclone's threat to life/property afloat and ashore. A summary of reconnaissance fixes received during 1982 is included in Section 6 of this Chapter.

### 2. RECONNAISSANCE AVAILABILITY

#### a. Aircraft

Aircraft weather reconnaissance in the JTWC area of responsibility is performed by the 54th Weather Reconnaissance Squadron (54th WRS) located at Andersen Air Force Base, Guam. The 54th WRS is presently equipped with six WC-130 aircraft and, from July through October, is augmented by the 53rd WRS from Keesler Air Force Base, Mississippi, bringing the total number of available aircraft to nine. The JTWC reconnaissance requirements, provided daily throughout the year to the Tropical Cyclone Aircraft Reconnaissance Coordinator (TCARC), include system(s) to be fixed, fix times, and forecast positions for each fix. The following priorities are utilized in acquiring meteorological data from reconnaissance aircraft in the western North Pacific area in accoudance with CINCPACINST 3140.1 (series):

- (1) Investigative flights and vortex or center fixes.
- (2) Synoptic data acquisition in support of tropical cyclone warnings.
- (3) Supplementary fixes on tropical cyclones.

As in previous years, aircraft reconnaissance provided direct measurements of height, temperature, flight-level winds, sea level pressure, estimated surface wind (when observable), and numerous additional parameters. The meteorological data are gathered by the Aerial Reconnaissance Weather Officers (ARWO) and dropsonde operators of Detachment 4, Hq AWS, who fly with the 54th WRS. These data provide the Typhoon Duty Officer (TDO) with indications of changing tropical cyclone characteristics, radii of associated winds, and current tropical cyclone position and intensity. Another important aspect is the availability of the data for research on tropical cyclone analysis and forecasting.

### b. Satellite

Satellite fixes from USAF/USN ground sites and USN ships provide day and night

coverage 1 the JTWC area of responsibility. Interpretation of this satellite imagery provides tropical cyclone positions and estimates of current and forecast intensities through the Dvorak technique (for daytime [asses).

#### c. Radar

Land radar provides positioning data on well developed tropical cyclones when in the proximity (usually within 175 nm (324 km)) of the radar sites in the Philippines, Taiwan, Hong Kong, Japan, South Korea, Kwajalein, and Guam.

### d. Synoptic

In 1982 JTWC also determined tropical cyclone positions based on the analysis of the surface/gradient level synoptic data. These positions were helpful in situations where the vertical structure of the tropical cyclone was weak or accurate surface positions from aircraft were not available due to flight restrictions.

# 3. AIRCRAFT RECONNAISSANCE SUMMARY

During the 1982 tropical season, the JTWC levied 276 vortex fixes and 50 investigative missions of which 17 were flown into disturbances which did not develop. In addition to the levied fixes, 180 supplemental fixes were also obtained. The average vector error for all aircraft fixes received at the JTWC during 1982 was 11 nm (20 km).

Aircraft reconnaissance effectiveness is summarized in Table 2-1 using the criteria as set forth in CINCPACINST 3140.1 (series).

TABLE 2-1. AIRCRAF	T RECONNAIS	SANCE PEPE	CTIVENESS			
	1 ADCOMMILE	JOHN CO LITT	CIIVENESS			
	NUMBER	OF				
EFFECTIVENESS	LEVIED	FIXES	PERCENT			
COMPLETED ON TIME	239		86.5			
EARLY	239					
LATE	14		2.2 5.1			
MISSED	17		6.2			
MISSED	17		0.2			
TOT	AL 276	;	100.0			
LEVIED	VS. MISSED  LEVIED 507	MISSED	PERCENT;			
1971	802	61	7.6			
1972	624	126	20.2			
1973	227	13	5.7			
1974	358	30	8.4			
1975	217	7	3.2			
1976	317	11	3.5			
1977	203	3	1.5			
1978	290	2	0.7			
1979	289	14	4.8			
1980	213	4	1.9			
1981	201	3	1.5			
1982	276	17	6.2			

# 4. SATELLITE RECONNAISSANCE SUMMARY

The Air Force provides satellite reconnaissance support to JTWC using imagery from a variety of spacecraft. The tropical cyclone satellite surveillance network consists of both tactical and centralized facilities. Tactical DMSP sites are located at Nimitz Hill, Guam; Clark AB, Republic of the Philippines; Kadena AB, Japan; Osan AB, Korea; and Hickam AFB, Hawaii. The These sites provide a combined coverage that includes most of the JTWC area of responsibility in the western North Pacific from near the dateline westward to the Malay Peninsula. The Naval Oceanography Command Detachment, Diego Garcia, provides NOAA polar-orbiting coverage in the central South Indian Ocean; this reconnaissance supplements the Air Force Global Weather Central (AFGWC) support in this data sparse region.

AFGWC, located at Offutt AFB, Nebraska, is the centralized member of the tropical cyclone satellite surveillance network.
support to JTWC, AFGWC processes imagery from DMSP and NOAA spacecraft. Imagery processed at AFGWC is recorded on-board the spacecraft as it passes over the earth. Later, these data are downlinked to AFGWC via a network of command/readout sites and communications satellites. This enables AFGWC to obtain the coverage necessary to fix all tropical systems of interest to JTWC. AFGWC has the primary responsibility to provide tropical cyclone surveillance over the entire Indian Ocean and portions of the western North Pacific on both sides of the dateline. Additionally, AFGWC can be tasked to provide tropical cyclone positions in the western North Pacific and South Pacific as backup to coverage routinely available in those regions.

The hub of the network is Det 1, lWW, colocated with JTWC on Nimitz Hill, Guam. Based on available satellite coverage, Det 1 coordinates satellite reconnaissance requirements with JTWC and tasks the individual network sites for the necessary tropical cyclone fixes. Therefore, when a position from a polar-orbiting satellite is required as the basis for a warning, called a "levied fix", a dual-site tasking concept is applied. Under this concept, two sites are tasked to fix the tropical cyclone from the same satellite pass. This provides the necessary redundancy to virtually guarantee JTWC a successful satellite fix on the tropical cyclone. Using this dual-site concept, the satellite reconnaissance network is capable of meeting all of JTWC's levied satellite fix requirements. Dual-site tasking can also be applied in portions of the North Indian Ocean by tasking AFGWC and the Navy site at Diego Garcia.

The network provides JTWC with several products and services. The main service is one of surveillance. Each site reviews its daily satellite coverage for indications of tropical cyclone development. If an area exhibits the potential for development, JTWC is notified. Once JTWC issues either a formation alert or warning, the network is tasked to provide three products: tropical cyclone positions, intensity estimates, and 24-hour intensity forecasts. Satellite tropical cyclone positions are assigned position code numbers (PCN) depending on the availability of geography for precise gridding and the degree of organization of the tropical cyclone's circulation center (Table 2-2). During 1982, the network provided JTWC with a total of 2026 satellite fixes on tropical systems in the western North Pacific. 146 were made for tropical systems in the North Indian Ocean. A comparison of those fixes made on numbered tropical cyclones in the western North Pacific with their corresponding JTWC best track positions is shown in Table 2-3. Estimates of the tropical cyclone's current intensity and a 24-hour intensity forecast are made once each day by applying the Dvorak technique (NOAA Technical Memorandum NESS 45 as revised) to daylight visual data.

The availability of polar-orbiting meteorological satellites declined again in 1982, after an improvement in 1981. At th beginning of 1982, there were three polar-At the orbiting satellites available; F-3 (FTV 14537) with limited coverage and availability, and NOAA 6 and 7 which were functioning normally, In February, NOAA 6 developed scanning problems and provided very little imagery data except for brief periods through most of the 1982 season. In November, the problem was corrected and NOAA 6 began functioning normally once again. NOAA 7, with nearly 8,000 orbits at the end of 1982, provided excellent data throughout the year and served as the network's primary reconnaissance satellite. A DMSP spacecraft, F-6 (FTV 17540), was launched on 20 December and is expected to be operational in January, 1983. F-6 replaces F-3 and may become the network's primary reconnaissance satellite in 1983. The outlook for 1983 looks even better, with projected launches of NOAA-E in February and F-7 in the latter part of the year.

### TABLE 2-2. POSITION CODE NUMBERS

### PCN METHOD OF CENTER DETERMINATION/GRIDDING

- EYE/GEOGRAPHY
- 2 EYE/EPHEMERIS
- WELL DEFINED CC/GEOGRAPHY
  WELL DEFINED CC/EPHEMERIS
- POORLY DEFINED CC/GEOGRAPHY
- POORLY DEFINED CC/EPHEMERIS
  - CC = Circulation Center

TABLE 2-3. MEAN DEVIATION (NM) OF ALL SATELLITE DERIVED TROPICAL CYCLONE POSITIONS FROM THE JTWC BEST TRACK POSITIONS. NUMBER OF CASES (IN PARENTHESES).

	WESTERN NORTH PA	ACIFIC OCEAN	NORTH INDIAN OCEAN						
	1974-1981 AVERAGE	1982	1980-1981 AVERAGE	1982					
PCN	(ALL SITES)	(ALL SITES)	(ALL SITES)	(ALL SITES)					
1 2	13.7 (428) 17.9 (85)	12.9 (109) 11.5 (291)	17.0 (9) 9.5 (2)	15.4 (18) 8.5 (2)					
3 4	19.5 (652) 24.4 (120)	16.8 (113) 15.7 (293)	29.7 (6) (0)	15.8 ( 3) 19.1 ( 3)					
5 6	36.6 (1514) 44.1 (317)	32.3 (325) 32.8 (732)	32.0 (22) 37.0 (33)	33.3 (43) 33.6 (31)					
162	14.4 (513)	11.9 (400)	15.6 (11)	14.7 (20)					
364	20.4 (772)	16.0 (406)	29.7 (6)	17.5 (6)					
546	37.9 (1831)	32.6 (1057)	35.0 (55)	33.4 (74)					

Besides fixes from the network, JTWC also received satellite-derived tropical cyclone positions from several secondary sources during 1982. These included: U.S. Navy ships equipped for direct readout; the National Environmental Satellite Service (NESS) using NOAA and GOES data; and the Naval Polar Oceanography Center, Suitland, Maryland using stored DMSP and NOAA data. Fixes from these secondary sources are not included in the network statistics.

### 5. RADAR RECONNAISSANCE SUMMARY

Eighteen of the 28 significant tropical cyclones occurring over the western North Pacific during 1982 passed within range of land based radars with sufficient cloud pattern organization to be fixed. The hourly and oftentimes, half-hourly land radar fixes that were obtained and transmitted to JTWC totaled 475.

The WMO radar code defines three categories of accuracy: good (within 10 km (5 nm)), fair (within 10 to 30 km (5 to 16 nm)), and poor (within 30 to 50 km (16 to 23 nm)). This year, 475 radar fixes were coded in this manner; 243 were good, 145 fair, and 87 poor. Compared to the JTWC best track, the mean vector deviation for land radar sites was 16 nm (30 km). Excellent support through timely and accurate radar fix positioning allowed JTWC to track and forecast tropical cyclone movement through even the most difficult and erratic tracks.

No radar fixes were made by reconnaissance aircraft during the 1982 tropical cyclone season in the western North Pacific area and, as in previous years, no radar reports were received on North Indian Ocean tropical cyclones.

# 6. TROPICAL CYCLONE FIX DATA

A total of 2970 fixes on 28 western North Pacific tropical cyclones and 127 fixes on five North Indian Ocean tropical cyclones were received at JTMC. Table 2-4, Fix Platform Summary, delineates the number of fixes per platform for each individual tropical cyclone. Season totals and percentages are also indicated.

Annex A includes individual fix data for each tropical cyclone. Fix data are divided into four categories: Satellite, Aircraft, Radar, and Synoptic. Those fixes labelled with an asterisk (\*) were determined to be unrepresentative of the surface center and were not used in determining the best tracks. Within each category, the first three columns are as follows:

FIX NO. - Sequential fix number

TIME (Z) - GMT time in day, hours and minutes

 $\begin{tabular}{ll} FIX POSITION - Latitude and longitude \\ to the nearest tenth of a degree \\ \end{tabular}$ 

Depending upon the category, the remainder of the format varies as follows:

### a. Satellite

- (1) ACCRY Position Code Number (PCN) is used to indicate the accuracy of the fix positon. A "1" indicates relatively high accuracy and a "6" relatively low accuracy.
- (2) DVORAK CODE Intensity evaluation and trend utilizing visual satellite data (Figure 2-1, Table 2-5). (For specifics, refer to NOAA TM; NESS-45)
- (3) COMMENTS For explanation of abbreviations, see Appendix I.
- (4) SITE ICAO call sign of the specific satellite tracking station.

### b. Aircraft

- (1) FLT LVL The constant pressure surface level, in millibars or altitude, in feet, maintained during the penetration. The normal level flown in developed tropical cyclones, due to turbulence factors, is 700 mb. Low-level missions are normally flown at 1500 ft (457 m).
- (2) 700 MB HGT Minimum height of the 700 mb pressure surface within the vortex recorded in meters.

TABLE 2-4. FIX PLATFORM SUMMARY FOR 1982

# FIX PLATFORM SUMMARY

WESTERN NORTH PACIFIC	AIRCRAFT	SATELLITE	RADAR	SYNOPTIC	TOTAL
		· · · · · · · · · · · · · · · · · · ·			
TS MAMIE	7 25	68 105	3 11		78 141
TY NELSON TY ODESSA	25 15	105 55	11		141
TY PAT	16	52		1	70 75 78 48
TY RUBY	15	63	6 		73 78
TS TESS		40		_	48
TS SKIP	4	25		ĭ	30
TS VAL	ž	14		4	20
TS WINONA	16		92	3	197
TY ANDY	11	86 72 101 82 66	14		97
STY BESS	30	101	4	4	139
TY CECIL	16	82 66	38	7	143
TY DOT	23		3	2	94
TY ELLIS	24		64	3	178 204
TY FAYE	27	133	41	3	204
TY GORDON	36	90			126
TS HOPE	1 13	26	92 14 4 38 3 64 41  2 59 10 32 	4	33
TY IRVING	13	109	59	7 5	188
TY JUDY	<b>2</b> 6 33	68	10	3	109
TY KEN TS LOLA		8 <b>4</b> 28	32		152
TD 22	2	10			28 12
CTV MAC	32	72	35		140
TY NANCY	19	80	35 14	2	115
TD 25	í	15			16
TY OWEN	27	128			155
TY PAMELA	44	160	22	3	229
TY ROGER	19 1 27 44 3	80 15 128 160 44			
TOTAL	468	1964		63	
% OF TOTAL					
	15. R	66.1	16.0	2.1	100.0
MA OI I TALB	13.0	00.1	10.0	2.1	100.0
INDIAN OCEAN		SATELLITE		SYNOPTIC	TOTAL
TC 20-82		46			46
TC 22~82		31			31
TC 23-82		29			29
TC 24-82		6		1	7
TC 25~82		10		4	14
TOTAL		122		5	127
% OF TOTAL NR OF FIXES		96.1		3.9	100.0

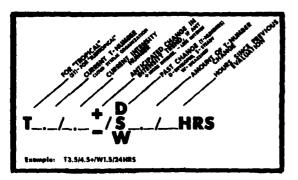


Figure 2-1. The current T-number is 3.5 but the current intensity estimate is 4.5 (equivalent to 77 kt). The cloud system has weakened by 1.5 T-numbers since the previous evaluation conducted 24 hours earlier. The plus (+) symbol indicates an expected reversal of the weakening trend or very little further weakening of the tropical cyclone during the next 24-hour period.

TABLE 2-5.	MAXIMUM SUSTAINED WIND SPEED (KT) AS A FUNCTION OF DVORAK CI & FI
	(CURRENT & FORECAST INTENSITY)
	NUMBER AND MINIMUM SEA LEVEL
	PRESSURE (MSLP)

TROPICAL CYCLONE	WIND	MSLP
INTENSITY NUMBER	SPEED	(NW PACIFIC)
1.0	25	
1.5	25	
2.0	30	1003
	35	999
2.5		994
3.0	45	
3.5	55	988
4.0	65	981
4.5	77	973
5.0	90	964
5.5	102	954
6.0	115	942
	127	929
6.5	140	915
7.0		900
7.5	155	
8.0	170	884
_		

- center can be visually detected (e.g., in the eye), the minimum sea level pressure is obtained by a dropsonde released above the surface vortex center. If the fix is made at the 1500-foot level, the sea level pressure is extrapolated from that level.
- (4) MAX-SFC-WND The maximum surface wind (knots) is an estimate made by the ARWO based on sea state. This observation is limited to the region of the flight path and may not be representative of the entire tropical cyclone. Availability of data is also dependent upon the absence of undercast conditions and the presence of adequate illumination. The positions of the maximum flight level wind and the maximum observed surface wind do not necessarily coincide.

- (knots) at flight level is measured by the AN/APN 147 doppler radar system aboard the WC-130 aircraft. Values entered in this category represent the maximum wind measured prior to obtaining a scheduled fix. This measurement may not represent the maximum flight level wind associated with the tropical cyclone because the aircraft only samples those portions of the tropical cyclone along the flight path. In many instances, the flight path is through the weak sector of the tropical cyclone. In areas of heavy rainfall, the doppler radar may track energy reflected from precipitation rather than from the sea surface, thus, preventing accurate wind speed measurement. In obvious cases, such erroneous wind data will not be reported. In addition, the doppler radar system on the WC-130 restricts wind measurements to drift angles less than or equal to 27 degrees if the wind is normal (perpendicular) to the aircraft heading.
- (6) ACCRY Fix position accuracy. Both navigational (OMEGA and LORAN) and meteorological (by the ARWO) estimates are given in nautical miles.
- (7) EYE SHAPE Geometrical representation of the eye based on the aircraft radar presentation. The eye shape is reported only if the center is 50 percent or more surrounded by wall cloud.
- (8) EYE DIAM/ORIENTATION Diameter of the eye in nautical miles. When an elliptical eye is present, the lengths of the major and minor axes and the orientation of the major axis are respectively listed. When concentric eye walls are present, each diameter is listed.

### c. Radar

- (1) RADAR Specific type of platform (land, aircraft, or ship) utilized for fix.
- (2) ACCRY Accuracy of fix position (good, fair, or poor) as given in the WMO ground radar weather observation code (FM20-V).
- (3) EYE SHAPE Geometrical representation of the eye given in plain language (circular, elliptical, etc.).
- (4) EYE DIAM Diameter of eye given in kilometers.
- (5) RADOB CODE Taken directly from WMO ground weather radar observation code FM20-V. The first group specifies the vortex parameters, while the second group describes the movement of the vortex center.
- (6) RADAR POSITION Latitude and longitude of tracking station given in tenths of a degree.
- (7) SITE WMO station number of the specific tracking station.

# **CHAPTER III - SUMMARY OF TROPICAL CYCLONES**

# 1. WESTERN NORTH PACIFIC TROPICAL CYCLONES

During 1982, the western North Pacific experienced the fourth consecutive year of below average tropical cyclone activity. Twenty-eight tropical cyclones occurred in 1982, three and one-half less than the annual average. Only two significant tropical cyclones failed to develop beyond the tropical depression (TD) stage and seven tropical storms (TS) failed to reach typhoon intensity. Of the 19 tropical cyclones that developed to typhoon (TY) intensity (the highest frequency since 1972), only two reached the 130 kt (67 m/sec) intensity necessary to be classified as super typhoons (STY). In the western North Pacific, tropical cyclones reaching tropical storm intensity or greater are assigned names in alphabetical

order from a list of alternating male/ female names (refer to Appendix 3). Table 3-1 provides a summary of key statistics for western North Pacific tropical cyclones. Each tropical cyclone's maximum surface winds (in knots) and minimum observed sea level pressure (in millibars) were obtained from best estimates based on all available data. The distance traveled (in nautical miles) was calculated from the JTWC official best tracks (see Annex A).

Table 3-2 through 3-5 provide further information on the monthly distribution of tropical cyclones and statistics on Tropical Cyclone Formation Alerts and Warnings.

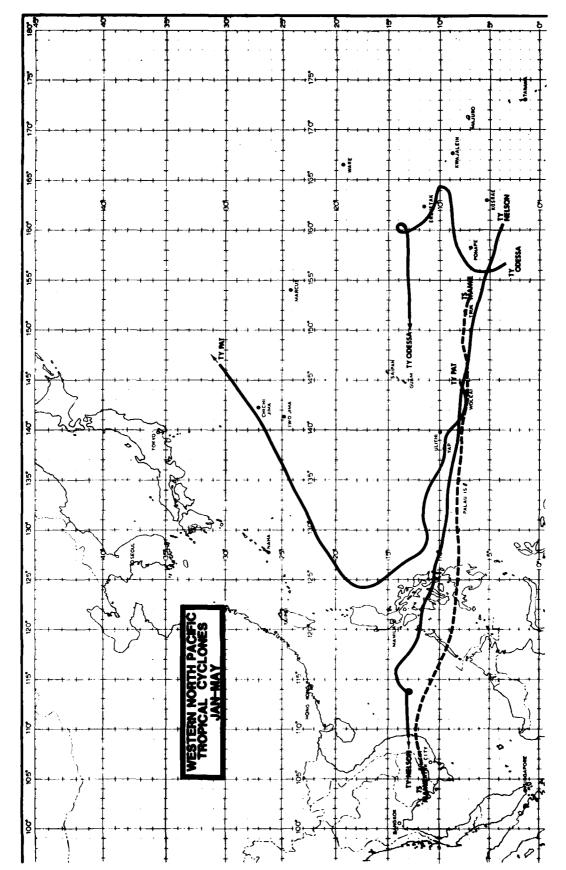
BLE	3-1.						WE	STERN NORT	H PACIFIC			
982	SIGNI	FICANT TF	ROPIC	AL (	YC	LON	ES					
TROP 1	CAL C	YCLONE	PERI	OD	ΟF	WAI	NING	CALENDAR DAYS OF WARNING	Number of Warnings Issued	MAXIMUM SURFACE WIND_(KT)	OBSERVED MSLP (MB)	BEST TRACK DISTANCE TRAVELED (N
01	TS M	LAMIE	16	MAR	_	24	MAR .	9	35	60	990	2733
02	TY N	IELSON	19	MAR	-	1	APR	14	53	105	934	3063
03	TY O	DESSA	29	MAR	_	4	APR	7	25	75	964	1528
04	TY F	PAT	17	MAY	-	23	MAY	7	24	105	947	1994
05	TY F	RUBY	21	JUN	-	27	JUN	7	25	75	970	2173
06	TS T	ress	29	JUN	-	2	JUL	4	14	35	999	585
07	TS S	SKIP	30	JUN	-	1	JUL	2	8	50	991	1197
08	TS V	/AL	3	JUL	-	4	JUL	2	7	55	987	867
09	TS V	NINONA	12	JUL	-	17	JUL	6	22	55	985	1486
10	TY A	ANDY	22	JUL	-	30	JUL	9	32	120	920	2072
11	STY E	BESS	22	JUL	-	2	AUG	12	43	140	901	2811
12	TY C	CECIL	5	AUG	-	14	AUG	10	39	125	914	1665
13	TY I	оот	9	AUG	-	15	AUG	7	27	80	960	2435
14	TY E	ELLIS	18	AUG	-	27	AUG	10	36	125	913	2640
15	TY I	FAYE	21	AUG	-	3	SEP	14	50	90	960	2454
16	TY C	GORDON	27	AUG	-	5	SEP	10	38	100	944	2014
17	TS I	HOPE	4	SEP	-	6	SEP	3	10	60	979	630
18	TY I	IRVING	5	SEP	-	16	SEP	12	44	90	952	1778
19	TY 3	JUDY	5	SEF	-	12	SEP	8	29	90	953	2133
20	TY I	KEN	16	SEF	-	25	SEP	10	37	110	936	1647
21	TS I	LOLA	16	SEF	-	19	SEP	4	12	50	993	1424
22	TD :	22	21	SEI		22	SEP	2	5	30	1001	282
23	STY I	MAC	1	OCT		9	OCT	9	32	140	895	2287
24	TY I	NANCY	11	OC1		18	OCT	8	29	115	926	2400
25	TD :	25	15	OCT		16	OCT	2	5	20	1002	228
26	TY (	OWEN	15	OC?	- 1	27	OCT**	1.2	40	105	9 3 9	3604
27	TY	PAMELA	24	NO	, -	9	DEC	16	60	100	940	4291
28	TY I	ROGER	6	DEC	: -	10	DEC	3	12	65	985	906
					_		ALS:	150*	793**			

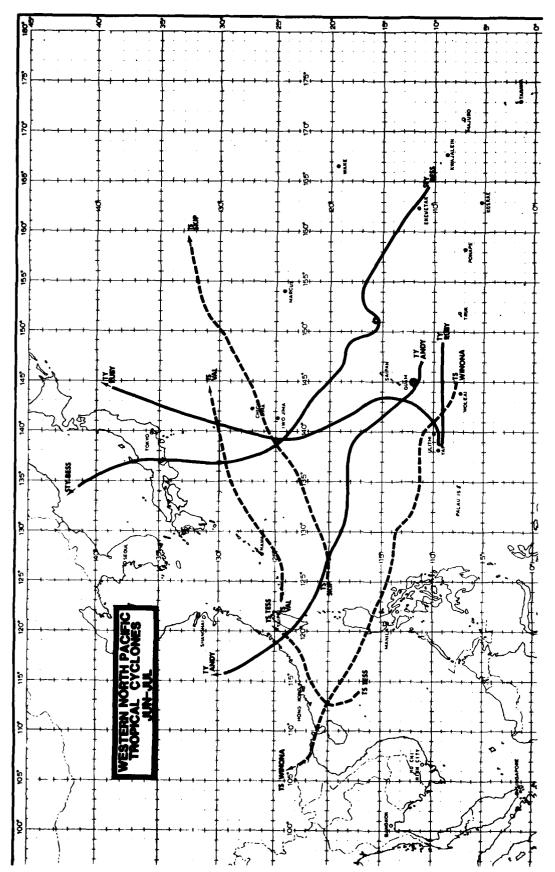
TABLE 3-2.																			
Western			19	82 SI	GNIFI	CANT	TROP	CAL (	CYCLO	NES									
NORTH PACIFIC	<u>JAN</u>	<u>FEB</u>	MAR	APR	MAY	JUN	JUL	AUG	SEP	<u>oct</u>	NOV	DEC	TOTAL	(1959-1 AVERAGE					
TROPICAL DEPRESSIONS	0	0	0	0	0	0	0	0	1	1	0	0	2	4.0	91				
TROPICAL STORMS	0	0	1	0	0	2	2	0	2	0	0	0	7	9.8	225				
TYPHOONS	0	0	2	0	1	1	2	5	3	3	1	1	19	17.8	409				
ALL TROPICAL CYCLONES	0	0	3	0	1	3	4	5	6	4	1	1	28	31.5	725				
1959-1981			-											PREVI	PREVIOUS				
AVERAGE	. 6	• 3	.7	1.0	1.4	2.0	5.0	6.3	5.9	4.4	2.7	1.4	31.5	23-Y	EAR				
CASES	13	8	15	22	32	45	115	144	136	101	62	32	725	HIST	ORY				
FORMATION ALERT	FORMATION ALERTS: 26 of 36 Formation Alert Events developed into significant tropical cyclones. Tropical Cyclone Formation Alerts were issued for all but two of the significant tropical cyclones that developed during 1982.																		
WARNINGS:		Num	ber o	f war	ning	days	:			150									
			Number of warning days with two tropical cyclones in region:												ı				
							with nes in			6				· · · · · · · · · · · · · · · · · · ·					

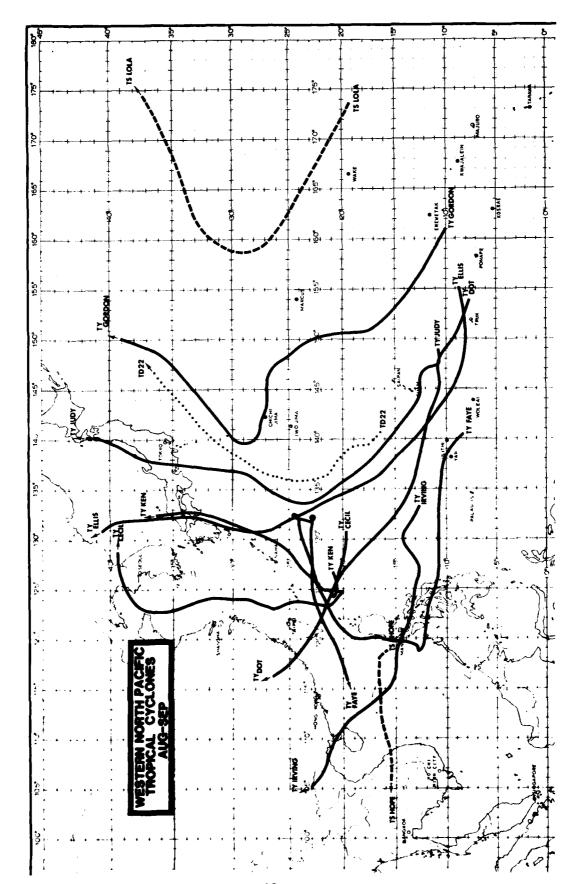
TABLE 3-3.		F	REQUE	NCY O	F TYP	HOONS	ву м	ONTH	AND Y	EAR		-	
YEAR	JAN	FEB	MAR	APR	MAY	JUN	<u>jur</u>	AUG	SEP	<u>oct</u>	NOV	DEC	TOTAL
(1945-1958) AVERAGE	. 4	.1	. 3	. 4	. 7	1.1	2.0	2.9	3.2	2.4	2.0	. 9	16.3
1959	0	0	0	1	0	0	1	5	3	3	2	2	17
1960	0	0	0	1	0	2	2	8	0	4	1	1	19
1961	0	Ô	1	0	2	1	3	3	5	3	1	1	20
1962	0	0	0	1	2	0	5	7	2	4	3	0	24
1963	0	0	0	1	1	2	3	3	3	4	0	2	19
1964	Ō	0	Ō	0	2	2	6	3	5	3	4	1	26
1965	1	0	0	1	2	2	4	3	5	2	1	0	21
1966	0	Ō	Ö	1	2	1	3	6	4	2	0	1	20
1967	Ö	Ō	1	1	0	1	3	4	4	3	3	0	20
1968	Ó	Ō	0	1	1	1	1	4	3	5	4	0	20
1969	ĩ	Ŏ	ō	1	0	Ö	2	3	2	3	1	0	13
1970	Ō	1	Ö	0	0	1	0	4	2	3	1	0	12
1971	0	0	0	3	1	2	6	3	5	3	1	0	24
1972	1	0	0	Ō	1	1	4	4	3	4	2	2	22
1973	0	Ó	0	0	0	0	4	2	2	4	0	0	12
1974	Ó	Ó	0	0	1	2	1	2	3	4	2	0	14
1975	1	ō	0	Ô	0	Ō	1	3	4	3	2	0	15
1976	1	0	0	1	2	2	2	1	4	1	1	0	15
1977	0	0	0	0	0	0	3	0	2	3	2	1	11
1978	Ō	Ō	Ō	1	0	Ō	3	2	4	3	2	0	15
1979	ī	ŏ	ì	ī	Ō	Ŏ	2	2	3	2	1	1	14
1980	ō	õ	ō	ō	2	ŏ	3	2	5	2	1	0	15
1981	ŏ	ŏ	ĭ	ŏ	ō	2	2	2	4	ī	2	2	16
1982	ō	Õ	2	ŏ	1	ī	2	5	3	3	ï	1	19
(1959-1982)	.3	.04	. 3	.6	.9	1.0	2.8	3.4	3.3	3.0	1.6	.7	17.8
average												• •	
CASES	6	1	6	15	20	23	66	81	80	72	38	15	423

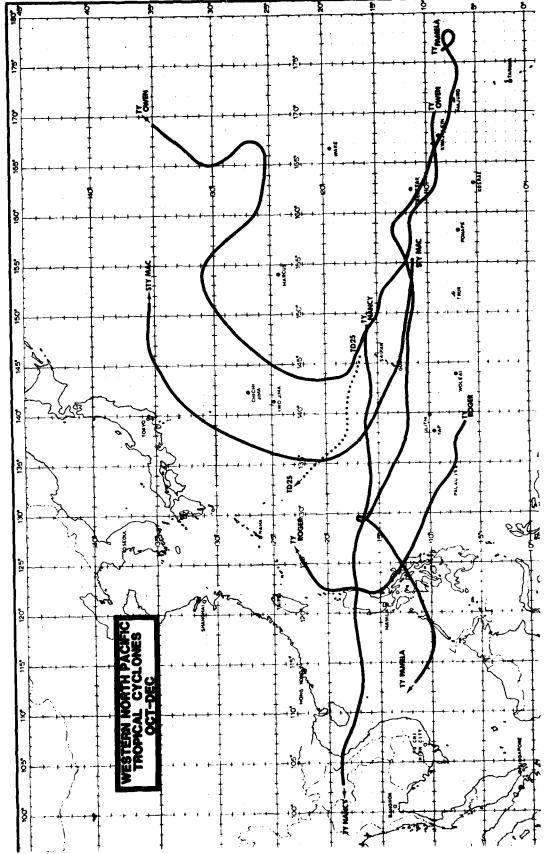
TABLE 3-4.													
	FREQUE	NCY O	F TRO	PICAL	STOR	MS AN	ID TY	PHOONS	BY M	ЮПТН	AND Y	EAR	
YEAR	<u>JAN</u>	FEB	MAR	APR	MAY	<u>JUN</u>	JUL	AUG	SEP	<u>oct</u>	NOV	DEC	TOTAL
(1945-1958)													
AVERAGE	.4	.1	. 4	. 5	.8	1.3	3.0	3.9	4.1	3.3	2.7	1.1	21.6
1959	0	1	1	1	0	0	3	6	6	4	2	2	26
1960	0	0	0	1	1	3	3	10	3	4	1	1	27
1961	1	1	1	1	3	2	-5	4	6	5	1	1	31
1962	0	1	0	1	2	0	6	7	3	5	3	2	30
1963	0	0	0	1	1	3	4	3	5	5	0	3	25
1964	0	0	0	0	2	2	7	9	7	6	6	1	40
1965	2	2	1	1	2	3	5	6	7	2	2	1	34
1966	0	0	0	1	2	1	5	8	7	3	2	1	30
1967	1	0	2	1	1	1	6	8	7	4	3	1	35
1968	0	0	0	1	1	1	3	8	3	6	4	0	27
1969	1	0	1	1	0	0	3	4	3	3	2	1	19
1970	0	1	0	0	0	2	2	6	4	5	4	0	24
1971	1	0	1	3	4	2	8	4	6	4	2	0	35
1972	1	0	0	0	1	3	6	5	4	5	2	3	30
1973	0	0	0	0	0	0	7	5	2	4	3	0	21
1974	1	0	1	1	1	4	4	5 5 4	5 5	4	4	2	32
1975	1	0	0	0	0	0	2	4	5	5	3	0	20
1976	1	1	0	2	2	2	4	4	5	1	1	2	25
1977	0	0	1	0	0	1	4	1	5	4	2	1	19
1978	1	0	0	1	0	3	4	7	5	4	3	0	28
1979	1	0	1	1	1	0	4	2	7	3	2	2	24
1980	0	0	0	1	4	1	4	2	6	4	1	1	24
1981	Ö	Ö	1	2	0	2	5	7	4	2	3	2	28
1982	Ō	0	3	0	1	3	4	5	5	2 3	1	1	26
(1959-1982)													
AVERAGE	. 5	. 3	.6	.9	1.2	1.6	4.5	5.4	5.0	4.0	2.4	1.2	27.5
CASES	12	7	14	21	29	39	108	130	120	95	57	28	660

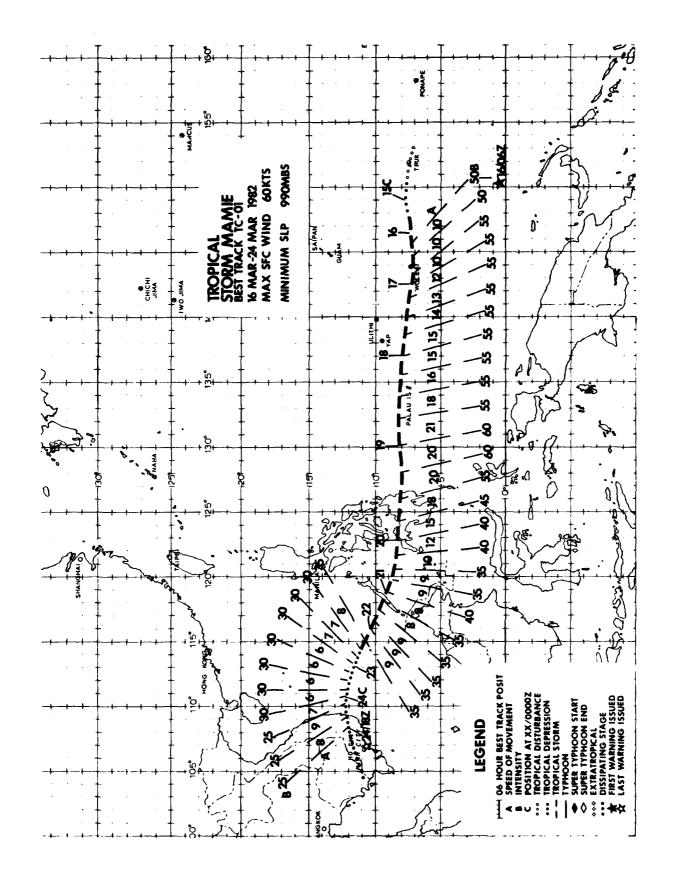
TABLE 3-5.											
	FORMATION ALERT SUMMARY										
	WESTERN NORTH PACIFIC										
<u>YEAR</u>	Number Of Alert Systems	ALERT SYSTEMS WHICH BECAME NUMBERED TROPICAL CYCLONES	TOTAL NUMBERED TROPICAL CYCLONES	DEVELOPMENT RATE							
1972	41	29	32	71%							
1973	26	22	23	85%							
1974	35	30	36	86%							
1975	34	25	25	74%							
1976	34	25	25	74%							
1977	26	20	21	77%							
1978	32	27	32	84%							
1979	27	23	28	85%							
1980	37	28	28	76%							
1981	29	28	29	97%							
1982	36	26	28	728							
(1972-1982) AVERAGE	32.5	25.7	27.9	798							











### TROPICAL STORM MAMIE (01)

Tropical Storm Mamie, the first tropical cyclone of the season, developed from an area of active convection 'hich was first sighted on 7 March, near 150E and just south of the equator (Figure 3-01-1). During the next five days, this convective area was observed migrating northward as the near-equatorial trough set up south of 05N. By 12 March, the convective organization was sufficient to warrant discussion in the Significant Tropical Weather Advisory (ABEH PGTW). On 14 March, the first satellite fix located the developing disturbance approximately 104 nm (193 km) east-southeast of Truk Atoll (WMO 91344). As the disturbance tracked westward and was followed on satellite imagery, the available synoptic data indi-

cated a relatively weak wind field with surface pressures near normal (1010 mb). However, because satellite imagery showed continued convective organization, a reconnaissance aircraft was sent on an investigative mission which proved to be very enlightening. Upon receipt of observed winds of 50 kt (26 m/sec) and evidence of a closed circulation from the reconnaissance data, the first warning on Tropical Storm Mamie was issued immediately (1606002). Mamie's intensities up to that point can only be extrapolated backwards; however, further intensification was very slow with the maximum intensity of 60 kt (31 m/sec) reached shortly before making landfall on Mindanao on 19 March.

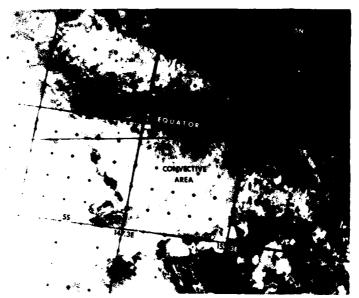


Figure 3-01-1. Satellite imagery shows an area of convection south of the equator which migrated northward and eventually became associated with the development of Tropical Storm Mamie, 070430Z March (NOAA 7 visual imagery).

From the first satellite fix to landfall on Mindanao, Mamie tracked westward along the southern periphery of a strong subtropical ridge (Pigure 3-01-2). During this period, had it not been for satellite surveillance, Mamie may well have gone undetected until initial casualty reports were received from Mindanao (approximately 40 persons dead and extensive property and crop damage). Aside from winds received from the reconnaissance aircraft missions,

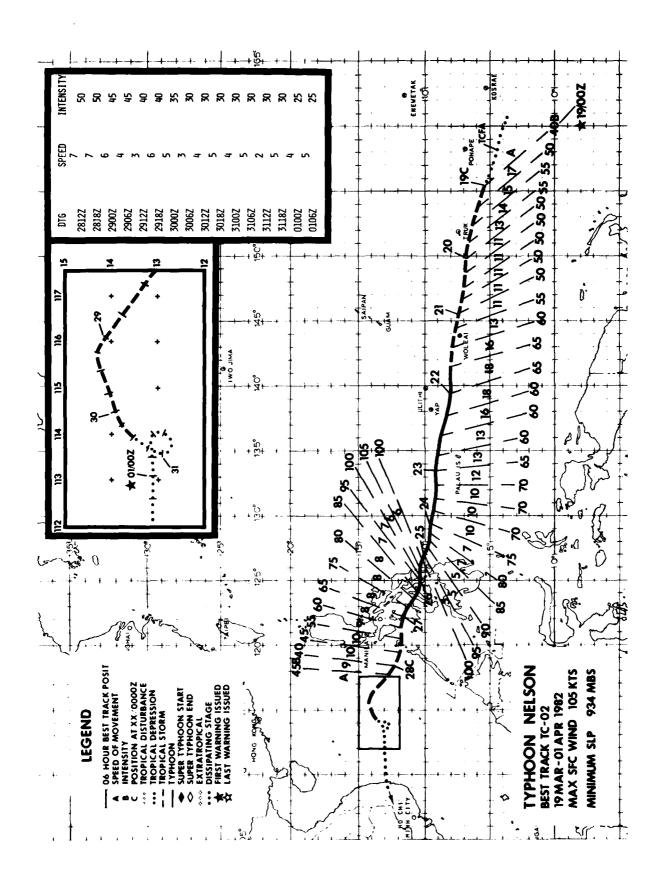
no other surface observations were received which indicated a well-organized circulation. Even upon landfall, Mamie was not detectable from the observations of local reporting stations. Fortunately, given Mamie's track and compact circulation (less than 90 nm (167 km)), both satellite and aircraft reconnaissance platforms were available and Mamie was tracked and monitored despite the paucity of reporting stations and ships in the Philippine Sea.



Figure 3-02-1. 500 mb streamLine analysis for 1500002 March superimposed on a mosaic from visual satelLite imagay. This figure depicts the steeking figure depicts the steeking figure depicts the steeking theorem of a strong subtrapical ridge north of Tropical Storm Manie. [1504361 and 1506181 March, NOAA 7 visual imagery].

On the second, and on subsequent reconnaissance aircraft missions, the Aerial Reconnaissance Weather Officers (ARWOS) observed an eyewall which was restricted to the lower levels. (Maximum observed height of the eyewall was near 10,000 ft (3048 m)). Due to Mamie's compactness and increasing vertical wind shear in the mid- and uppertropospheric levels, the eyewall did not fully develop and extend to heights that could be observed on satellite imagery. This failure to develop in the vertical contributed to Mamie not reaching typhoon strength.

After tracking across the northern portion of Mindanao, Mamie entered the Sulu Sea with winds of 40 kt (21 m/sec) and was unable to reintensify despite surface conditions which were generally favorable for reintensification. On 21 March, as Mamie reached the South China Sea, a weakness in the subtropical ridge allowed a more northwestward track which was maintained until approximately 230000Z, when the ridge strengthened and Mamie resumed a westward movement. At 241200Z, Mamie made final landfall near Nha Trang, Vietnam and then dissipated in the mountainous region to the west.



Typhoon Nelson was the second of three early season tropical cyclones in the western North Pacific which formed at very low latitudes southeast of Guam. Nelson, similar to Mamie (01), was a well-behaved tropical cyclone which developed and tracked westward, south of a strong midtropospheric ridge (centered near 15N 150E and extending west-northwest toward Taiwan).

In the initial stages of development, Nelson intensified rapidly from a weak tropical disturbance to a full-fledged tropical storm. In fact, the Tropical Cyclone Formation Alert, which was issued just 10 hours before the first warning, was preceded and followed by satellite fixes (180900Z and 181800Z) which described very little convective organization. However, at 190615Z, a reconnaissance aircraft reported flight level (1500 ft (457 m)) winds of 66 kt (34 m/sec), surface winds of 50 kt (26 m/sec), and an extrapolitied sea level pressure of 993 mb.

Nelson's rapid development was in response to a véry strong divergence field in the upper-troposphere located over the cyclone, where a 40 to 60 kt (21 to 31 m/sec) easterly jet branched to the northwest and southwest. However, while these strong easterlies remained near Nelson, further development was limited to minimal typhoon strength. During this entire period, Nelson moved rapidly westward at speeds reaching 18 kt (33 km/hr) on 22 April, after which a gradual slowing in forward speeds and further intensification followed. After maintaining intensities between 60 and 70 kt (31 to 36 m/sec) for 60 hours, a change in the upper air patterns allowed Nelson to deepen rapidly, reaching 100 kt (51 m/sec) within 24 hours.

At 2312002, while Nelson was moving away from the westernmost extent of the upper-tropospheric ridge (Fig.re 3-02-1), nearby westerlies aloft provided a strong outflow channel to the north and northeast.

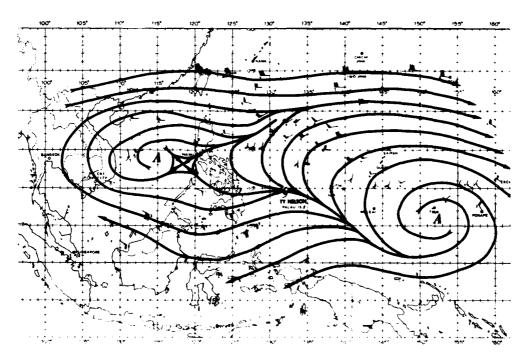


Figure 3-02-1. 200 mb analysis at 2312007 March. Note Typhoon Nelson's position just west of the westernmost portion of the ridge and the presence of a westerly current seven degrees north which will provide a good outflow channel.

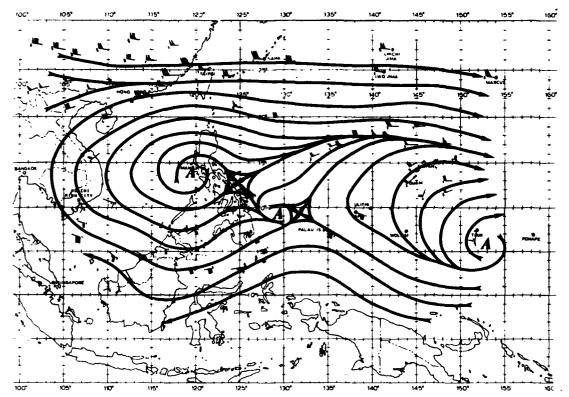


Figure 3-02-2. 200 mb analysis at 2400001 March. Within 12 hours an appreciable change in the upper-tropospheric levels has allowed the formation of an anticyclone aloft and the beginning of the good outflow channel into the westerlies.

As this occurred, an upper-level anticyclone was established (Figure 3-02-2) and intensified over Nelson; concurrently, Nelson responded and reached a maximum intensity of 105 kt (54 m/sec) at 2512002 (Figure 3-02-3).

On 27 March, a much weakened Tropical Storm Nelson entered the South China Sea after navigating through the south-central Philippines. On 28 March, Nelson briefly reintensified before weakening under the influence of vertical wind shear. Until 2912002, the presence of a 500 mb short wave trough north of Nelson provided a favorable opportunity for recurvature toward the northeast. However, Nelson was quickly sheared and the low-level center meandered westward and eventually dissipated four days later. The fifty-third and final warning was issued at 0100002 April for Tropical Depression 02 (Nelson), approximately 240 nm (444 km) east of Nha Trang, Vietnam, near to the location where Tropical Storm Mamie (01) had made landfall one week earlier.

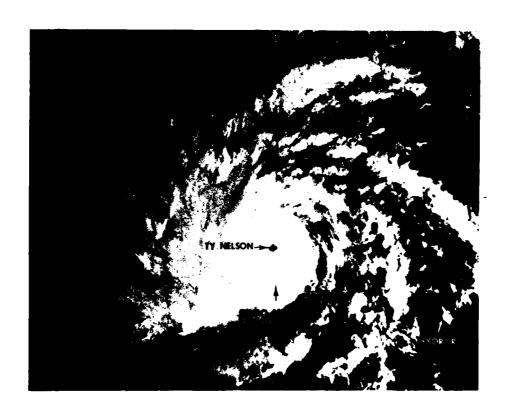
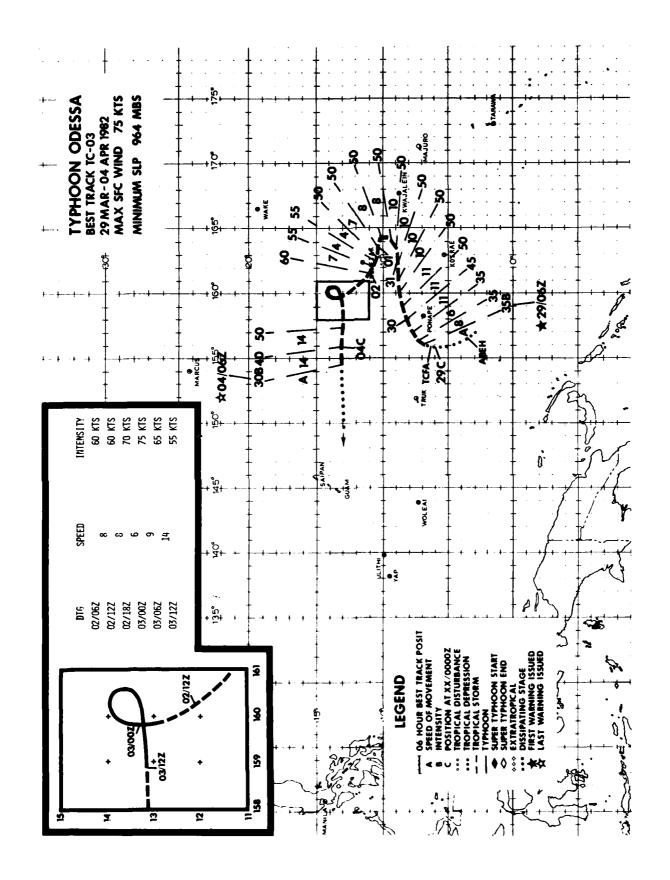


Figure 3-02-3. Typhoon Nelson near peak intensity, east of the Philippines. Note the anticyclonic flow aloft and the well-formed outflow channel to the north, 250601Z March. (NOAA 7 visual satellite imagery)



March is normally a relatively quiet month in the tropical western North Pacific, producing on the average less than one tropical cyclone per year. March 1982 was quite the contrary, with the genesis of three tropical cyclones taking place within a period of 13 days; 1967 was the most recent year with more than one tropical cyclone during March. Typhoon Nelson (02) and the subject of this report, Typhoon Odessa represent only the fifth and sixth typhoons to occur in March since the JTWC was established in 1959.

Just as March was a unique month in the level of tropical cyclone activity, Odessa was unique among the three tropical cyclones. As illustrated in Figure 3-03-1, tropical cyclones which develop near 160E tend to follow one of two climatological tracks: 60 percent move in a generally westward direction and 40 percent move in a generally northward direction. Although both Tropical Storm Mamie (01) and Typhoon Nelson (02) moved westward from this genesis area, Odessa's track defied climatology as it moved both eastward and westward across the area shown for northward-moving tropical cyclones.

Typhoon Odessa was initially detected as an area of loosely organized convection near 2N 159E on 26 March. In the following three days, a cloud system center emerged from these low-latitudes and moved north-westward. A Tropical Cyclone Formation Alert was issued at 290400Z upon receipt of reconnaissance aircraft data which indicated that a closed circulation had developed. As subsequent aircraft data and satellite imagery became available, it was evident that the circulation had rapidly organized and thus, at 290741Z, the initial warning was issued for Odessa with maximum surface winds of 35 kt (18 m/sec)

Much of the remaining discussion will concentrate on the meteorological factors which influenced Odessa's atypical track. To facilitate this discussion, Odessa's best track has been divided into four segments (Figure 3-03-2) representing the different track directions of the tropical cyclone. Each of these segments can be explained quite well in post-analysis when large-scale changes in the mid-latitudes at distances 600 to 1200 nm (1111 km to 2222 km) from Odessa are considered.

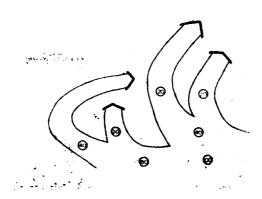


Figure 3-03-1. March Typhoon Climatology Tracks |1WW Special Study 105-8 March 1970|

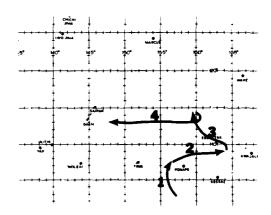


Figure 3-03-2. Typhoon Odessa's best track illustrating the four segments of Odessa's track as discussed in the text.

Odessa's initial movement to the northwest was in response to a weakening of the subtropical ridge northeast of Guam and the rapid cyclogenesis which was occurring southeast of Japan. The first three forecasts described a short-term northwestward movement followed by a more pronounced westward track. However, the continued deterioration of the subtropical ridge, north of Odessa, essentially removed any easterly steering current capable of driving Odessa westward. During the same period, a major high pressure system moved southeastward from Japan and strengthened the low-level northeasterly wind regime west of Odessa. Conventional surface data, at 3000002, show this ridging extended deep into the tropics and created an effective block to any continued northwestward advance by Odessa (Figure 3-03-3). At mid-tropospheric

levels, rawinsonde data from Truk (WMO 91334), Ponare (WMO 91348) and Kwajalein (WMO 91366) indicated that the base of a mid-latitude trough extended well into the tropics and south of Odessa. Although the axis of this trough was located well northeast of Odessa, between 160E and 165E (500 mb), its influence on Odessa's movement became obvious in the days that followed.

On 30 and 31 March, as Odessa tracked eastward at 10 to 11 kt (19 to 20 km/hr), the mid-latitude trough advanced more rapidly eastward and was located near 170E at 310000Z. Odessa, now 400 nm (741 km) west of the trough axis, began to slow and eventually turn toward the north. As Odessa approached 10N, it turned west-northwestward in response to a weak subtropical ridge filling in behind the mid-latitude trough

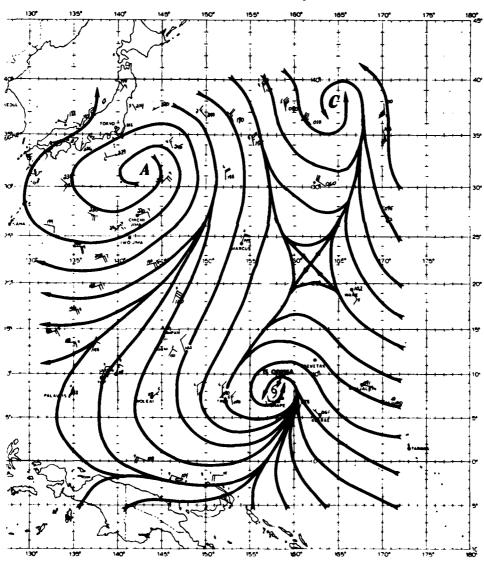


Figure 3-03-3. The 3000002 March 1982 surface/gradient level wind data and streamline analysis. Wind speeds are in knots.

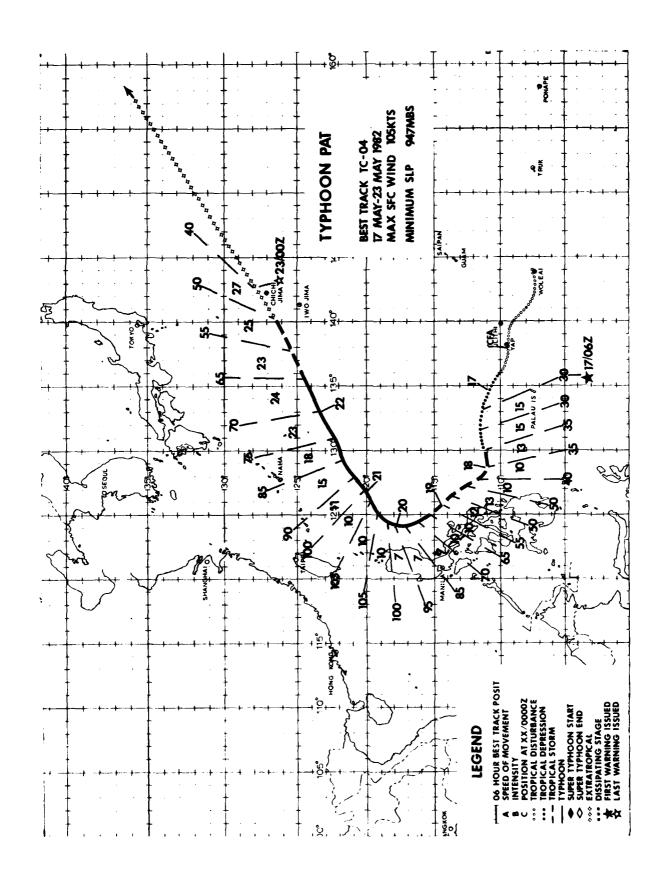
(which had stalled near 175E). To this point, Odessa had maintained an intensity near 50 kt (26 m/sec) as westerlies restricted the development of the cyclone's circulation. With the subtropical ridge in place, Odessa was able to develop a closed circulation in the mid-tropospheric levels and a noticeable intensification trend began which culminated with a peak intensity of 75 kt (39 m/sec) at 0300002 (Figure 3-03-4 shows Odessa just prior to reaching typhoon strength).

Just as Odessa reached maximum intensity, the last major directional change

commenced. On 3 April, Odessa was approaching a break in the subtropical ridge, along 158E. Forecasts described a track northward around the ridge axis and then northeastward toward Wake Island. However, strong midand upper-level southerly winds moved over Odessa and a rapid shearing of the major convective features to the northeast followed. At 0308002, a reconnaissance aircraft located Odessa's low-level circulation center 90 nm (167 km) southwest of the closest convective activity. During the 24 hours that followed, Odessa weakened rapidly and was no longer detectable from satellite imagery after 0406002.



Figure 3-03-4. Tropical Storm Odessa, approximately 18 hours prior to reaching maximum intensity. At this time, Odessa was approximately 90 nm (167 km) west of Enewetak Atoll with maximum winds of 60 kt (31 m/sec). Note the cirrus streamers to the south, these originated from TC 17-82 (Bernic) in the Southern Hemisphere. Later, near 0300007, Bernic's expansive development would increase the southerly winds moving toward Odessa and aid in the shearing process which led to Odessa's dissipation. 020425. April (NOAA 7 visual imagery).



The transition from the winter to the summer monsoon regime over the tropical western North Pacific can vary greatly from year to year. During this transition time (March through May), tropical cyclone activity can be very strong (six in 1980) or moderate (three in 1981). In May, 1982, there were several disturbances that developed in the near-equatorial trough and then dissipated without producing a significant tropical cyclone. During the third week of May, Typhoon Pat developed and became the only disturbance to reach warning status in the region between early April (Typhoon Odessa (03)) and late June (Typhoon Ruby (05)).

The disturbance that eventually produced Typhoon Pat was first detected as a mid-level circulation southwest of Guam. The 140000Z May 500 mb streamline analysis depicted a cyclonic circulation center near 8N 143E. Coincident with the analysis, satellite imagery indicated an area of centralized convection associated with the circulation. A Tropical Cyclon Formation Alert (TCFA) was issued at 140305Z when evidence of a strong upper-level circulation center was noticed on satellite

imagery. Aircraft reconnaissance at 1406002 reported no evidence of a surface circulation but did observe an area of strong low-level convergence near the convective disturbance.

It wasn't until the disturbance began moving out of the near-equatorial trough that a low-level circulation could be located by reconnaissance aircraft. On 17 May, another aircraft investigation located a closed circulation at 1500 ft (472 m) but surface winds were too light to determine a surface circulation center. The first warning on Pat, as Tropical Depression 04, was issued at 170600Z when sustained increased convective organization was observed on satellite imagery.

The forecast movement for the first six warnings projected Pat to move westward with passage over the Philippines, south of Luzon. This scenario was based on the existence of a mid-level (500 mb) ridge centered over the western portion of the South China Sea which was forecast to build eastward thus blocking northward movement of Typhoon Pat. During the ensuing 24-hour period, little change was evident in the mid-level ridge north and northwest of Pat (Figure 3-04-1). The

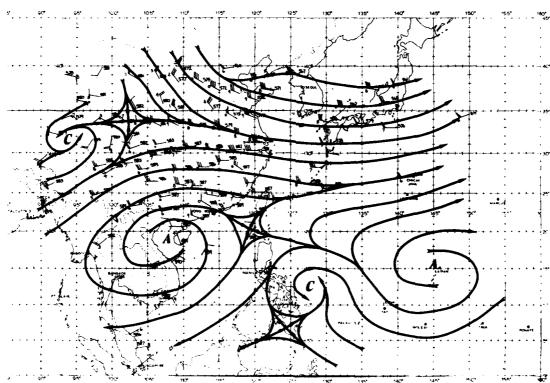


Figure 3-04-1. 500 mb streamline analysis at 1812007 May which shows Pat just south of an apparent weakness in the subtropical ridge. There had been no appreciable height fall changes over a 24-hour period when Pat suddenly changed from a westward-moving to northward-moving tropical cyclone.

expected building of the ridge had not materialized; yet until 18 May, Pat persisted on its westward track. Then abruptly at 180600Z, Pat turned northward and paralleled the eastern portion of the Philippines for two days. Aircraft reconnaissance data at 180940Z provided the first indication of a possible track change, which was later confirmed by satellite fixes from Detachment 1, 1WW, Nimitz Hill, Guam and radar fixes from Cataduanes Island (WMO 98447). At 190000Z, upon evaluation of the fix data and a reevaluation of the westward track forecast scenario, JTWC changed the forecast track northward and toward eventual recurvature. From that point forward, Pat presented no further track forecasting problems.

Shortly after turning northward, Pat began to rapidly intensify, aided by a 200 mb wind maximum that had moved north of Pat and had enhanced outflow channels to the northeast. At 2112002, Typhoon Pat reached its maximum intensity of 105 kt (54 m/sec) (Figure 3-04-2). This rapid intensification was not fully anticipated as Pat was forecast to only attain minimal typhoon strength. When aircraft reconnaissance data at 1922332 reported 95 kt (49 m/sec) surface winds, this new information was factored into the

next forecast which then called for Pat to attain maximum intensity within the ensuing 12 to 18 hours. Fortunately, Pat's increased intensity did not bring any destructive winds to the Philippines, previously hit by Tropical Storm Mamie (01) and Typhoon Nelson (02), despite approaches as close as 90 nm (167 km) to Cataduanes Island and eastern Luzon.

As Typhoon Pat approached 20N, a track toward the northeast became increasingly favorable. In recurvature, Pat began to accelerate in response to increasing midand upper level westerly steering currents. A new method for forecasting the acceleration of northward-moving tropical cyclones, developed by JTWC personnel during the past year, was used to predict the point of initial acceleration as well as the rate of acceleration; Typhoon Acceleration Prediction Technique (TAPT) (Weir, 1982), utilizes 200 mb analysis data to determine possible future acceleration. First used on the 1912007 analysis data, TAPT accurately predicted acceleration to begin near 19N and gave excellent guidance on the speed of movement to 24N, where Pat slowed its forward speed and weakened from the effects of vertical wind shear on the system's organization.

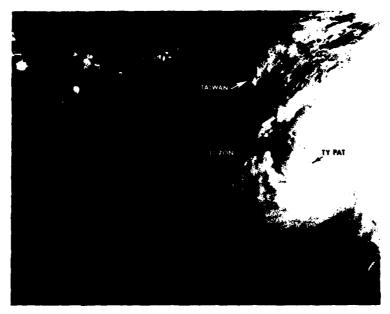
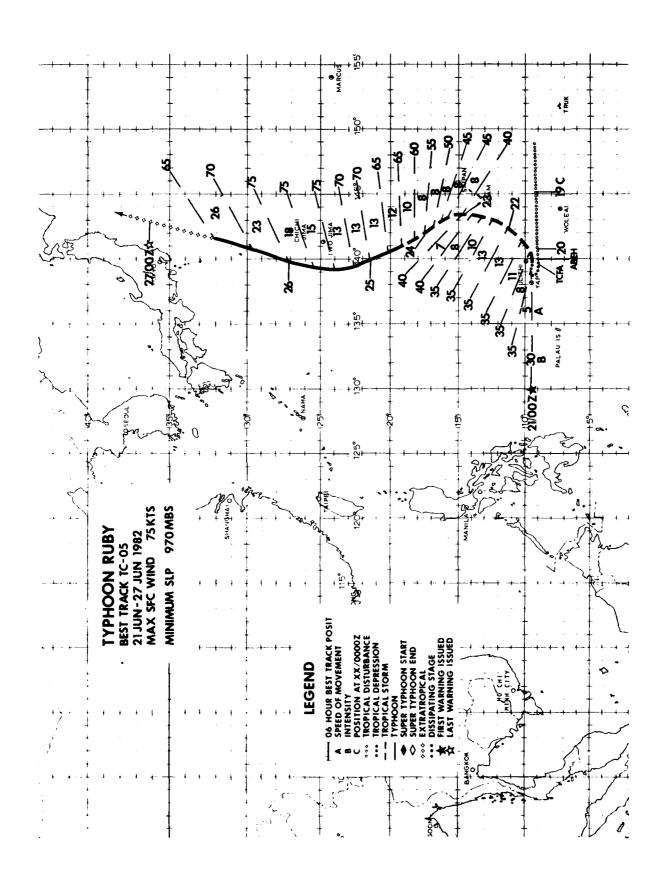


Figure 3-04-2. Typhoon Pat near maximum intensity of 105 kt (54 m/sec), 150 nm (278 km) east of Luzon, 2006412 May (NOAA 7 visual imagery).

On 22 May, as Typhoon Pat approached 24N, a weak frontal system (associated with an extratropical low east of Japan) was moving toward Pat and the first indications of Pat's eventual transition to an extratropical low were observed. Since 2116002, there had been a marked decrease in Pat's deep-layer convection; additionally, aircraft reconnaissance data at 220955Z indicated that the central sea level pressure had risen to 988 mb. Although observed winds were still near typhoon strength, the maximum winds were observed at distances much further from the center than in previous missions. These

expanding wind radii are frequently associated with tropical cyclones undergoing extratropical transition as the cyclone's energy source changes from latent heat release to a more baroclinic process. By 2212002, synoptic data gave evidence of the incursion of cool, dry air into Pat's center and satellite imagery showed the system merging into a weak frontal boundary. Transition to an extratropical low was completed by 2300002 and this low gradually dissipated during the subsequent 24 hours as it was drawn into a stronger extratropical system, east of Japan.



Typhoon Ruby developed from a convective disturbance which was initially detected southeast of Guam on 18 June. During the first ten days of Ruby's development, its track and eventual extratropical transition were dramatically affected by several events which can be traced to fairly rapid changes in the upper-troposphere. These events will be discussed individually as they occurred during Ruby's lifespan; however, collectively, they illustrate the need for a bettet understanding of the upper-troposphere and its effects on subsequent tropical cyclone development and movement.

Satellite imagery, on 18 June, located a weak convective disturbance 320 nm (593 km) southeast of Guam. During the next 24 hours, this disturbance was observed tracking westward to near 145E where it weakened significantly while an upper-level anticyclone, previously supporting the convection, receded to a position east of 150E. On 20 June, a cloud cluster developed near 9N 141E and continued moving westward, south of Ulithi Atoll (MMO 91203). A Tropical Cyclone Formation Alert was issued upon receipt of Ulithi's 2006002 surface observation which reported a six-hour pressure fall

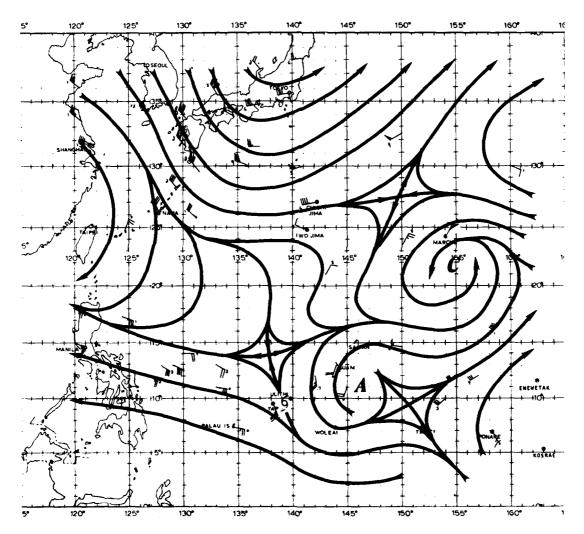


Figure 3-05-1. 2100007 June 1982, 200 mb streamline analysis. Ruby, positioned within a divergent southerly flow, was maintaining a central convective feature. To the north, a broad northerly flow was beginning to influence the near-storm environment. Wind speeds are in knots.

of 5 mb to 1004 mb, and a windshift from 030 degrees at 20 kt (10 m/sec) to 100 degrees at 25 kt (13 m/sec).

During the next 42 hours, satellite imagery and synoptic data indicated very little westward movement, with the system moving erratically between Yap and Ulithi. At 202339%, the first aircraft reconnaissance mission into the system located a well-defined, very compact, 995 mb circulation center 45 nm (83 km) west-southwest of Ulithi. Based on these data, the first warning was issued for Tropical Storm Ruby at 210000; with a forecast track toward the west-northwest. This forecast track was based on a very close agreement in most objective forecast aids. In fact, only the 700 mb and 850 mb steering aids, which indicated south-eastward low-level steering, did not support this initial forecast movement.

The apparent conflict between low-level and mid-level steering was seen as a reason for ruby's erratic movement; but at that point, the long-term potential for a west-northwest-ward track looked good. At 2108302, an aircraft fix located Ruby 35 nm (65 km) south of Ulithi; this fix was in good agreement with Ulithi's 2106002 observation. Unfortunately, the 2106002 observation would be the last received from Ulithi for 24 hours. During the next 18 hours, fix positions from infrared satellite imagery showed Ruby moving northward, then northwestward, passing over Ulithi. Without sufficient synoptic data to the contrary, the next few warnings followed these satellite positions and maintained the forecast track toward the west-northwest.

However, on this first day in warning status, the upper-level wind regime near Ruby was changing. As depicted in Figure 3-05-1,

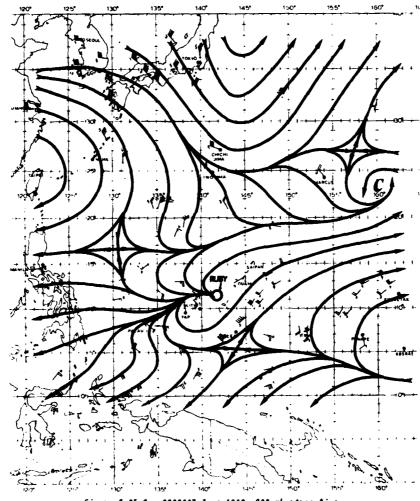


Figure 3.05-2. 2200007 June 1982, 200 mb streamline analysis. Considerable change has occurred in a 24-hour period. The northerly winds have penetrated to 10N, where the base of an upper-level trough formed. Coincident with this trough, a maximum cloud zone developed over the area south of Ruby's position and near-gale force winds were observed over a broad area at the surface and gradient levels near the upper-level trough/maximum cloud zone. Wind speeds are in knots.

the 200 mb winds at 210000Z were strongly divergent over Ruby but a broad mid-latitude trough, south of Japan, was introducing a significant northerly flow into the region. 220000Z, the 200 mb winds (see Figure 3-05-2) had changed and an upper-level trough had set up south of 10N, and south of Ruby. while this process was underway, the objective forecast aids - especially the tropical cyclone models - were predicting a return to a westward track while analyses data were indicating a strengthening of the monsoon flow, located southeast and southwest of Ruby. When the first visual satellite imagery became available on 22 July, a low-level circulation center was seen embedded in a maximum cloud zone which had developed over the monsoon flow. This circulation, presumed to be Ruby, was located near 11N 142E, or more than 200 nm (370 km) from the 210000Z warning position. The 220000Z warning was immediately amended and a forecast track to the northeast, toward Guam, was issued. Interestingly, this amended warning had an exact 24-hour forecast position and only a 57 nm (106 km) error at 48-hours; but more importantly, a similar set of forecast errors could have been produced as early as 210600Z if the development of an upper-level trough and associated surge in the southwest monsoon

could have been predicted from the 2100002 upper-wind flow analysis. This northeastward movement has become a familiar pattern in years past when developing tropical cyclones become involved with an intensifying southwest monsoon. For recent examples, refer to past ATCRs describing Tropical Depression 16/Typhoon Orchid (1980), Tropical Storm Thelma/Typhoon Vernon (1980), Tropical Depression 11/Tropical Storm Phyllis (1981), and Typhoon Gay (1981).

As Fuby moved northeastward toward Guam, its intensity remained near 35 kt (18 m/sec). During this period, much of Ruby's circulation pattern was involved with the monsoonal flow and the strongest winds were observed within the maximum cloud zone associated with this flow. Not until 23 June, when Ruby turned northward and became a separate entity from this maximum cloud zone, did its surface pressures fall and intensity increase.

Although the best track might suggest a rather steady increase in both Ruby's intensity and speed of movement from 23 through 25 June, these days were marked by often conflicting fix data. For example, the 240445Z visual satellite imagery (refer to Figure 3-05-3) indicated an exposed low-level circulation center near 19N 142E, while a



Figure 3-05-3. Visual satellite imagery suggested a low-level circulation center located in the northern periphery of the cloud system. This apparent low-level center was located well-north of a aircraft position received more than 3 hours tater. 2404452 June 1982 (NOAA 1 visual satellite imagery).

reconnaissance aircraft surface/700 mb fix, at 2408092, found a center nearly 60 nm (111 km) to the south. On 25 June, the 2506302 and 2509112 700 mb aircraft fixes were positioned in a way to suggest either erratic movement or multiple circulation centers. These phenomena have been observed in other tropical cyclones which have emerged from an active monsoon flow. Typhoon Orchid (1980) had a sufficient amount of satellite, aircraft and radar fixes to suggest a high speed looping pattern over a 30-hour period. Ruby's intensity during this period was equally hard to determine. Intensity estimates derived from visual satellite imagery (Dvorak, 1973) and minimum sea level pressures (Atkinson and Holliday, 1977) were normally separated by 15 to 25 kt (8 to 13 m/sec), with the pressure consistently lower than expected during this period. In postanalysis, both the track and the intensity trend have been smoothed by a careful reevaluation of the data during this period.

As Ruby moved north-northwestward, the potential for recurvature, significant acceleration and extratropical transition became increasingly important. series of evaluations from the 2400002, 2412002 and 2500002 200 mb charts, 24N was consistently identified as the best latitude for initial acceleration into the midlatitude westerlies (Typhoon Acceleration Prediction Technique (Weir, 1982)). A persistent and strong west-southwesterly 200 mb flow over Japan gave an indication for the potential of recurvature toward the northeast and, based on the mean latitudes of recent mid-latitude low pressure systems and ocean sea surface temperature fronts, 35N was deemed to be a favorable latitude for extratropical transition. Figure 3-05-4 depicts the 2512002 200 mb flow with Typhoon Ruby near 24N. Within 18 hours, Ruby had assumed a north-northeastward track and accelerated to 23 kt (43 km/hr). The 260000Z 200 mb analysis (Figure 3-05-5)

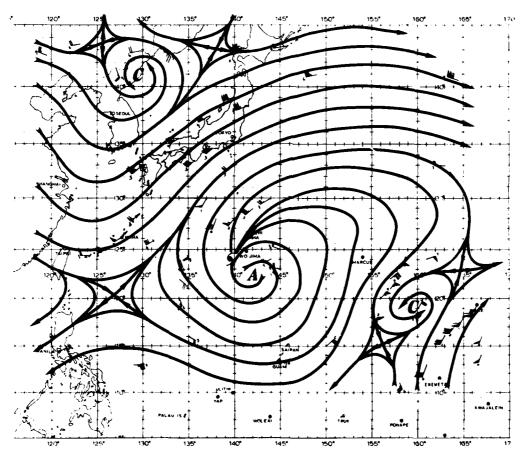


Figure 3-05-4. 2512007 June 1982, 200 mb streamline analysis. Typhoon Ruby was becoming involved with the upper-level mid-latitude westerlies. Wind speeds are in knots.

showed a dramatic change in the upper-wind pattern over Japan; 200 mb winds had become south-southeasterly and thus, signalled the potential for a more northward track. However, visual satellite fixes indicated a continuing tendency toward the northeast and the northeast forecast track was maintained. The 260602Z reconnaissance aircraft fix located Ruby's low-level circulation center 70 nm (130 km) west of the 260600Z warning position and these data, along with the 200 mb winds, dictated an amended warning toward the north-northeast and passing just east of northern Honshu.

A similar shift in the 200 mb flow also occurred with Typhoon Thad (August, 1981)  $\,$ 

and as Ruby approached the mid-latitude westerlies, the potential for such a shift was being closely monitored. Unlike Thad, Ruby quickly transitioned to an extratropical low and this movement and upper-wind shift may have been associated with that process more than any large-scale changes in the upper-troposphere.

The final tropical cyclone warning for Ruby was issued at 270000Z, after the 262149Z aircraft fix data indicated a cold core low was present at 700 mb. As an extratropical low, Ruby continued to move toward the north and rapidly occluded, becoming nearly stationary east of Hokkaido for several days thereafter.

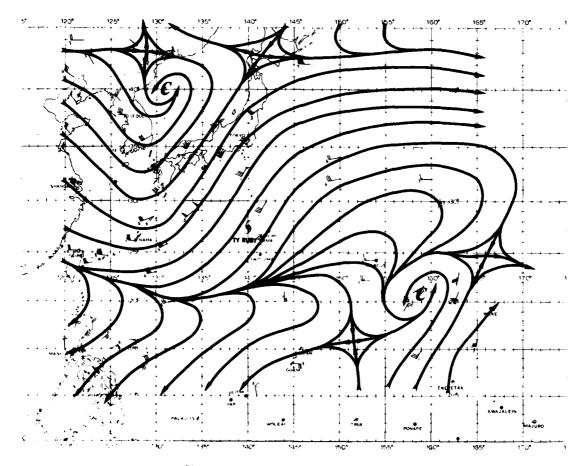
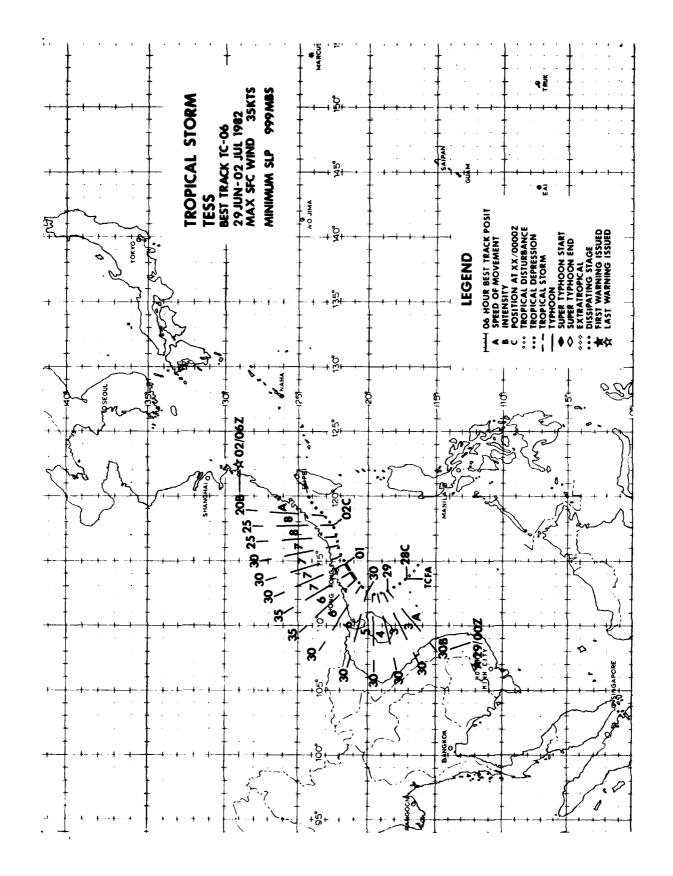


Figure 3-05-5. 2600007 June 1982, streamline analysis. Typhoon Ruby was well-embedded in the mid-latitude flow. Note the significant change in the 200 mb wind pattern over Japan in just 12 hours. This change, along with Ruby's rapid extratropical transition produced an extended north-northeas ward movement and not the northeas tward track predicted earlier from the 200 mb flow depicted in Figure 3-05-4. Wind speeds are in knots.



## TROPICAL STORM TESS (06)

The Tropical Storm Tess had its origins and much of its life cycle linked to a strong southwest monsoonal flow which was established over the South China Sea in late June. While low surface pressures and gale force winds generally prevailed over a majority of the region, a disturbance could not be detected until 27 June, when synoptic reports indicated the development of a weak low-level circulation. At the point of initial detection, the nearest area of significant convection was located more than 200 nm (370 km) to the northwest of the circulation. A Tropical Cyclone Formation Alert was issued at 272330z when it had become apparent that a zone of lower surface pressures (<1002 mb) was aligning itself in close proximity to the disturbance.

During the subsequent 24-hour period, there was an increase in convective activity within the formation alert area and satellite imagery suggested an increase in convective organization. Although still lacking evidence of vertical alignment, the trends toward lower surface pressures and increased convection

prompted the issuance of the initial warning for Tropical Depression 06 at 2900002.

From 28 to 30 June, Tropical Depression 36 tracked northward without any further evidence of convective organization. On 30 June, the depression turned east-northeastward and paralleled the coast of China. During this period, the southwest monsoon had abated somewhat and several weak circulations (eddies) became evident on satellite imagery (Figure 3-06-1). However, as the system passed south of Hong Kong, synoptic reports indicated that near-gale and gale force winds were present close to Tropical Depression 06. Thus, on the 0100002 July warning, Tropical Depression 06 was upgraded to Tropical Storm Tess. Post-analysis of this period indicates that Tess probably only attained tropical storm strength for a relatively short period (3012002 to 3018002).

On 1 and 2 July, surface synoptic data indicated a marked decrease in wind velocities in the area and thereafter, the remants of Tess gradually dissipated as it approached the Formosa Strait.

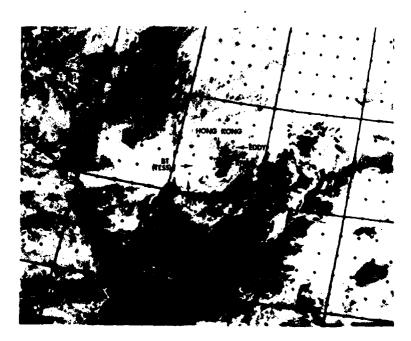
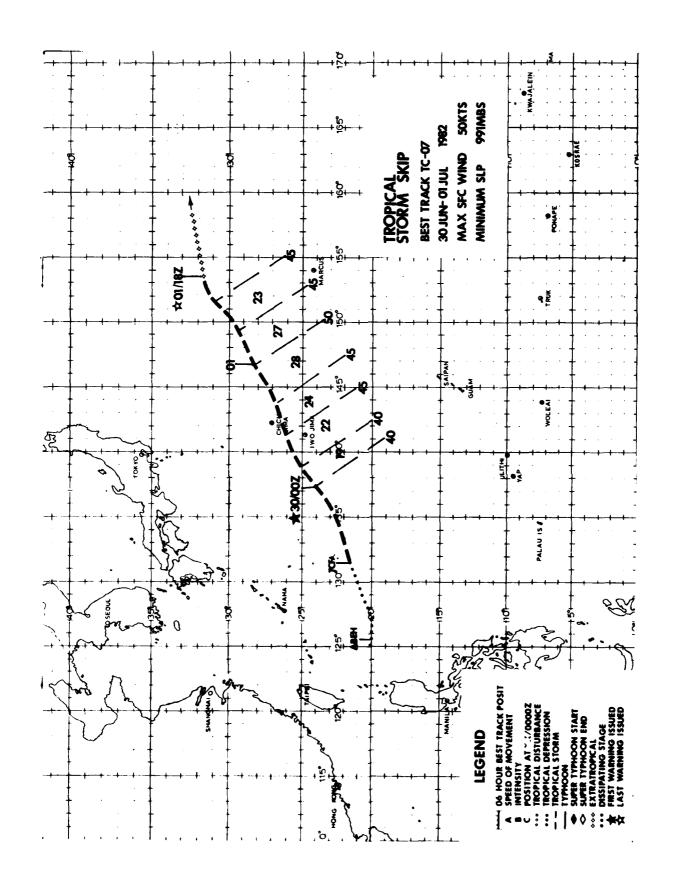
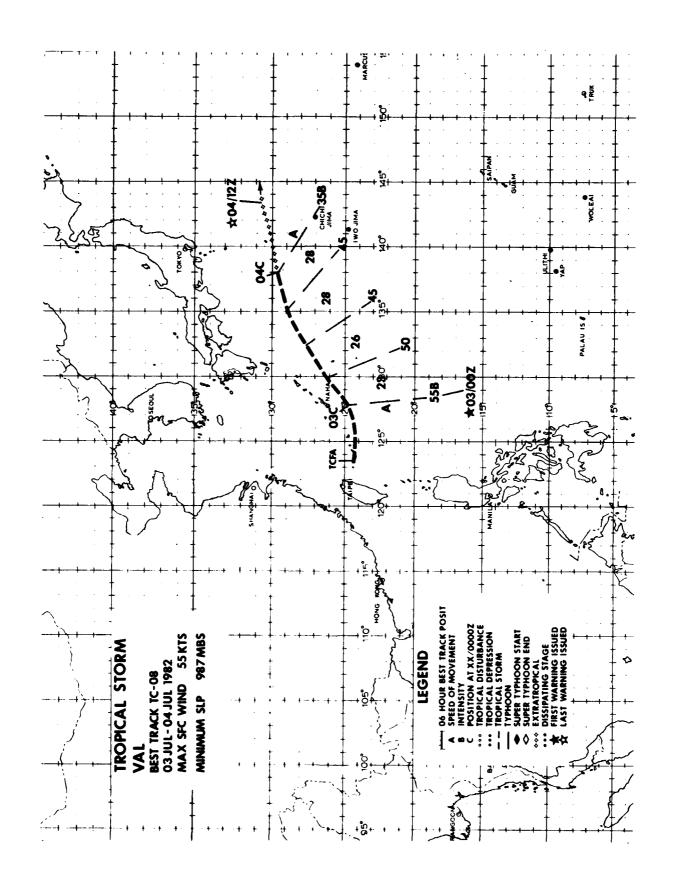


Figure 3-06-1. Satellite imagery hows several low-level eddies far removed from the central convective mass. Fix positions supplied from Detachment 5, 1WW, Clark AB, RP (RPMK) and from Detachment 1, 1WW, Nimitz Hill, Guam (PGTW) differ considerably in determining which eddy is the developing Tropical Storm Tess. The final best track position at fix time is shown as BT. 3006562 June (NOAA 7 visual imagery)





## TROPICAL STORMS SKIP (7) AND VAL (8)

Each tropical cyclone season sees a few circulations develop near the mid-latitudes which appear to have both tropical and extratropical characteristics. These "hybrid" or "subtropical" cyclones have long been known to the tropical forecaster. In particular, an article by Herbert and Poteat (1975) describes several distinguishing characteristics that allow differentiation between tropical and subtropical systems based upon satellite imagery (Table 3-07-1). The week between 23 June and 5 July saw The week between 23 June and Dury surt two such circulations, Tropical Storms Skip two such circulations, Tropical Storms During and Val, develop southeast of Taiwan. their existence each of these relatively small and compact systems were observed to have several characteristics associated with non-tropical cyclones, e.g. very little deep-layer convection near the surface center, displacement of convective features poleward and eastward of the system center, and each remained entirely enveloped within a larger cloud system associated with the mid-latitude westerlies. Conversely, both aircraft and satellite reconnaissance data indicated some typical tropical characteristics, i.e. a sharp pressure gradient near the center, surface winds in excess of 45 kt (23 m/sec), warm central temperatures, and a small but uniquely tropical upper-level anticyclonic outflow pattern.

The origin of the first circulation, Tropical Storm Skip, was more tropical in nature. The disturbance was first detected near 20N 124E on 26 June when surface

synoptic data indicated the presence of circulation that was subsequently apparent as an exposed low-level circulation on satellite imagery. Synoptically, a sharp trough existed between this area and Typhoon Ruby (05), which was in its initial phases of extratropical transition near 30N 130E. Although satellite imagery indicated that frontogenesis had begun, it is unclear from the available data just how far south along the trough the front could be identified. To the west, an active monsoon trough, which was soon to spawn Tropical Storm Tess (06) in the South China Sea, had also begun to push into the area. During the next three days, winds in excess of 15 to 20 kt (8 to 10 m/sec) could be detected in the monsoon flow south of the circulation; however, very little organized convection could be detected near the vortex. In the upper-troposphere, westerlies penetrated as far south as 25N (at 500 mb) and 20N (at 200 mb) as the result of deep troughing behind the now extratropical Ruby. By 29 June the 200 mb flow began to ridge strongly along the trough boundary and 60 to 70 kt (31 to 36 m/sec) westerly winds to the north were soon accompanied by 65 kt (33 m/sec) northeasterly winds south of the trough. This resulted in an extensive cloud band more than 500 nm (926 km) wide along this entire region. A Tropical Cyclone Formation Alert (TCFA) was issued at 290500z when a small upper-level anticyclone appeared to be developing in the vicinity of the low-level circulation (Figure

TABLE 3-07-1. SUBTROPICAL AND TROPICAL CYCLONES	
SUBTROPICAL	TROPICAL
Poleward & eastward from center	Equatorward & eastward from center
Width 15° latitude or more	Width usually less than 10° latitude
Convective cloud system remains connected to other synoptic systems (Some cold lows excepted)	Cloud system becomes isolated
al cloud structure	
- amorphous convective	cloud mass
cloud pattern with limi	ted convection near cente
•	SUBTROPICAL  Poleward & eastward from center  Width 15° latitude or more  Convective cloud system remains connected to other synoptic systems (Some cold lows excepted)  al cloud structure  - amorphous convective

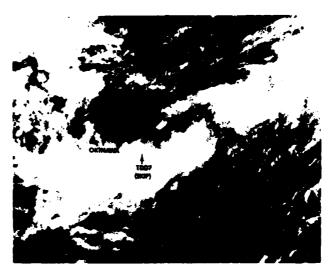


Figure 3-07-1. A developing low-level circulation can be detected within the confines of a broad large-scale cloud pattern. Weak upper-level outflow can be detected at 2905267 June (NOAA 7 visual imagery).

An aircraft investigative mission on 30 June located a 991 mb center with surface winds of 45 kt (23 m/sec), prompting the first warning to be issued at 300000Z. During the next 36 hours, Skip moved quickly northeastward along the frontal trough, averaging over 24 kt (44 km/hr), however its convection remained weak and generally restricted to within 120 nm (222 km) of its northern and eastern sides (Figure 3-07-2). Throughout Skip's lifetime, the Aerial

Reconnaissance Weather Officers (ARWOs) consistently reported very little convection near the center, rather large light and variable wind centers, and an abundance of stratocumulus entrainment. By 0116002 July, all convection had dissipated from the vicinity of Skip's center and the upperlevel anticyclone was no longer visible, indicating that the storm had completed its extratropical transition.

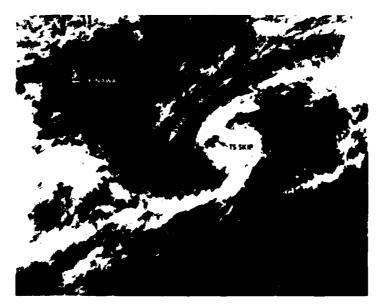


Figure 3-07-2. Tropical Storm Skip's exposed lowlevel circulation can be seen at 3005147 June to the south and west of its major convective area. Note the extent of stratocumulus to the north of this system. (NOAA 7 visual imagery).

As Skip was moving rapidly toward the northeast, a new circulation could be identified from 1 July synoptic data, just east of Taiwan. At this time, the frontal trough ran westward from Skip into the vicinity of northern Taiwan. Upper-level vicinity of northern Taiwan. Upper-level westerlies prevailed throughout the region although sharp ridging south of the 200 mb jet still maintained the large band of clouds. Isolated convection was present throughout this cloud mass, although none could be identified with the low-level circulation as it remained quasistationary. However, aircraft reconnaissance at 020115Z did identify a 995 mb center with winds up to 35 kt (18 m/sec) in the flow south of the circulation, thus a TCFA was issued. Convection finally began to develop near the circulation's center by 0212002 and, when the next aircraft mission found that the circulation had moved eastward and deepened to 987 mb, the first warning was issued at 030000Z. As was the case for Tropical Storm Skip, Val moved quickly northeastward along the trough, averaging over 26 kt (46 km/hr). Also like Skip, convection remained weakly organized and restricted to within 100 to 200 nm (185 to 370 km) of the system's center (mostly on the northern and eastern sides). As can be seen in Figure 3-07-3, Val still displayed its own individual outflow pattern despite being embedded within the larger cloud mass. By 040000Z, Val had lost all of its convection and could no longer be identified on satellite imagery as it completely merged into the frontal zone.

Both Tropical Storms Skip and Val contained many of the characteristics of subtropical cyclones identified in Table 3-07-1. Although monsoonal flow probably helped initiate Skip's low-level vortex, its further development and propagation can more likely be attributed to its position in relation to the eastern side of the upper trough. This is especially true of Val which formed farther north. Convection for both storms remained weak and unorganized and, partially due to strong westerly vertical shear, the low-level centers were often exposed with convection remaining poleward and eastward. Figures 3-07-2 and 3-07-3 show that each system did eventually become partially isolated from the dominance of the midatitude westerlies and displayed their own anticyclonic outflow pattern.

Re-analysis of synoptic and satellite data revealed that Skip and Val were not the only circulations to develop during this unique period. At 3000002, Skip (located near 24N 137E) could be seen flanked by circulations (or frontal waves) at 34N 153E, 31N 143E and 20N 125E. Similar conditions occurred for Tropical Storm Val as well. On the synoptic-scale each was only a small part of an extensive mass of clouds along the eastern boundary of a very active mid-latitude upper-level trough.

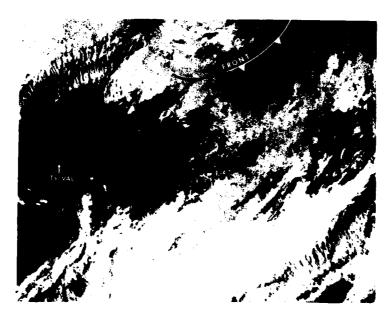
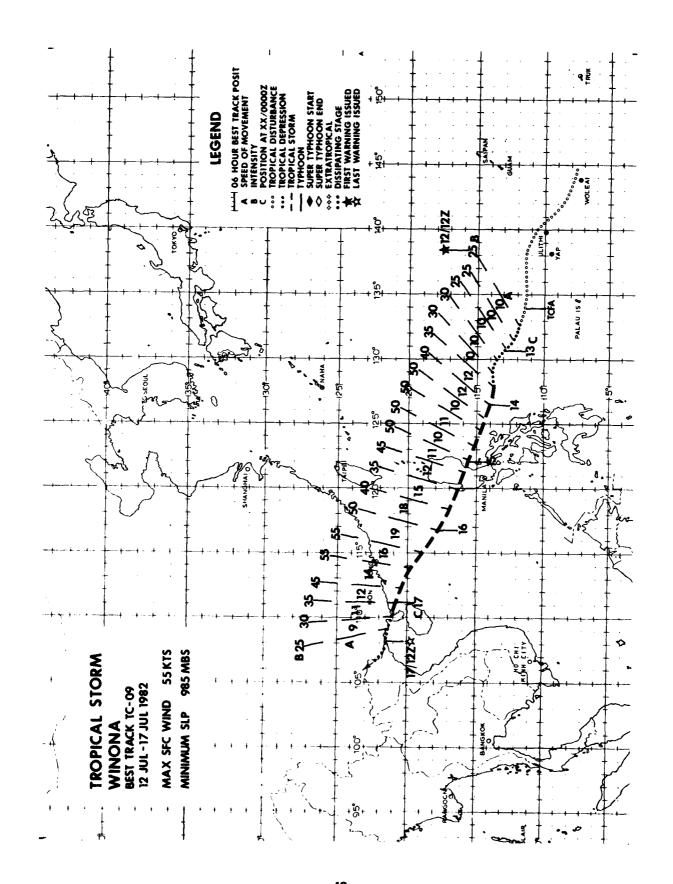


Figure 3-07-3. Tropical Storm Val's unorganized convection and outflow pattern can be seen with respect to larger frontal cloud mass pattern at 031723Z July. (NOAA 7 infrared imagery).



## TROPICAL STORM WINONA (09)

Tropical Storm Winona exemplifies tropical cyclone development without corresponding upper-level support. The presence of strong upper-level winds is often an inhibiting factor for significant tropical cyclone development. Based on JTWC's 200 mb synoptic data and streamline analyses, a strong subtropical ridge centered over central China was reinforcing strong upper-level winds over the Philippine Sea and South China Sea (See Figure 3-09-1). This situation persisted throughout Winona's warning period. The presence of 35 to 45 kt (17 to 23 m/sec) northeasterly winds in the upper-troposphere over Winona prevented the development of a strong anticyclonic outflow pattern and was a major factor in restricting further development to typhoon strength.

Winona's entire intensification process was slow. Between 10 and 12 July, three Tropical Cyclone Formation Alerts (TCFA) were issued as satellite imagery, synoptic and reconnaissance aircraft data revealed a persistent, but weak, disturbance moving westward through a primary tropical cyclone genesis region between Guam and the Republic of the Philippines. Reconnaissance aircraft investigative missions on the 10th and 11th found a weakly organized system with minimum sea level pressures of 1008 mb. At 121200Z, synoptic data gave the first indication that the disturbance was intensifying as gradient-level winds reported by Yap (WMO 91413) increased to 25 kt (13 m/sec). Simultaneously, the 200 mb streamline analysis indicated the development of a weak anti-

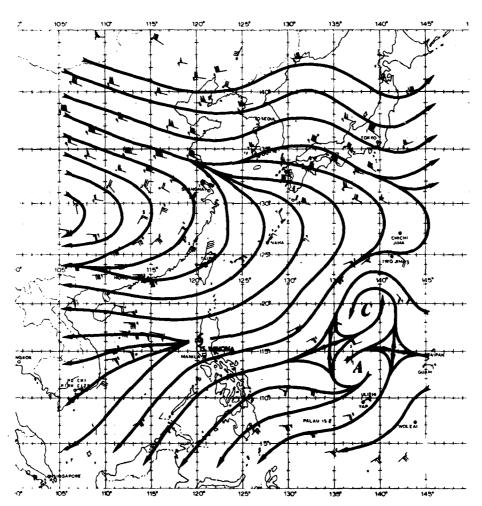


Figure 3-09-1. 200 mb streamline analysis at 151200 July. Strong upper-level northeasterly winds prevent the development of outflow channels to the north.



Figure 3-09-2. Tropical Storm Winona at 55 kt [28 m/sec] intensity, 400 nm (741 km) northwest of central Luzon. Even at maximum intensity, Winona's upper- and lower-level centers are not aligned due to the presence of strong upper-tropospheric winds. 1607077 (NOAA 7 visual imagery).

cyclone over the disturbance. This information, combined with increasing convection and organization (apparent on satellite imagery), prompted the issuance of the initial warning for Tropical Depression 09 at 1214002. Subsequent aircraft reconnaissance at 1300362 confirmed JTWC's suspicions of intensification when it was reported that the minimum sea level pressure had dropped to 1000 mb.

From the initial warning, JTWC forecasts predicted that Winona would move into a region of strong upper-level winds which would inhibit its development. Thus, a maximum intensity of 50 kt (26 m/sec) was forecast prior to Winona's expected landfall upon central Luzon. Winona's intensity and movement were well-forecast during this period as it

proceeded west-northwestward along the southern periphery of the subtropical ridge, centered along 25N.

By 1406002, Winona reached the forecast 50 kt (26 m/sec) intensity which it maintained until landfall on Luzon at 1505002. As Winona crossed central Luzon, it passed 35 nm (65 km) north of Clark AB, where maximum sustained winds recorded were 23 kt (12 m/sec) with peak gusts to 30 kt (15 m/sec). Reported damage to the surrounding region was estimated at \$275,000 with 272 families left homeless as a result of severe flooding.

Winona entered the South China Sea as a minimal tropical storm, but upon reaching open waters, its convection increased and Winona reintensified to a peak intensity of 55 kt

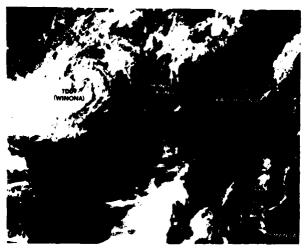


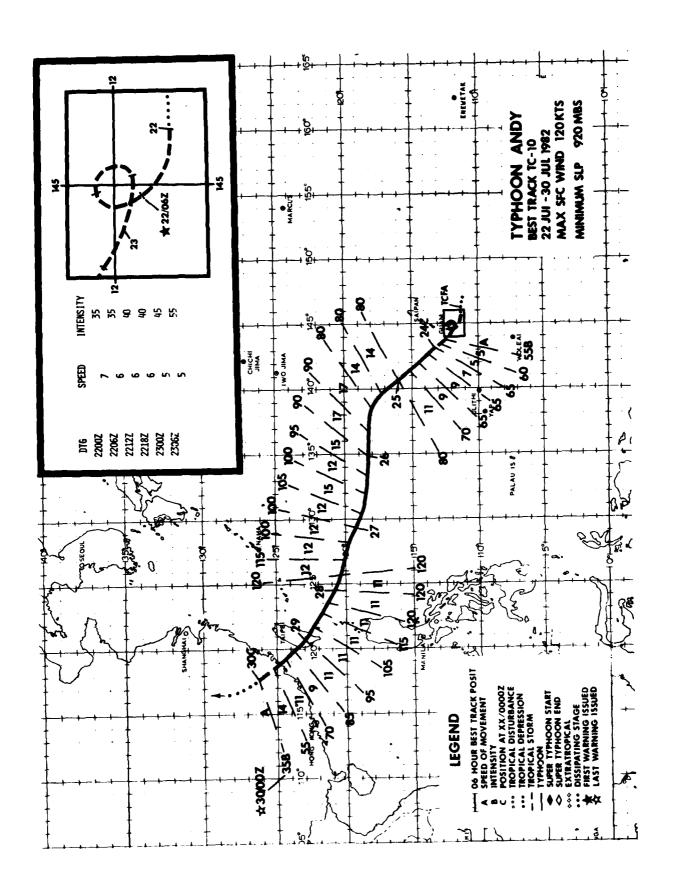
Figure 3-09-3. Winona after being downgraded to a tropical depression 210 nm (389 km) west-southwest of Hong Kong. Notice the persistent strong upper-level shear. 1706552 July (NOAA 7 visual imagery).

(28 m/sec) at 160600Z (Figure 3-09-2). This intensification occurred even though 40 kt (21 m/sec) 200 mb winds persisted over the area. However, based on limited 500 and 700 mb data, it appears that the strong winds did not extend into the mid-tropospheric levels. This situation allowed Winona's convection to develop well into the mid-tropospheric levels while the strong upper-level winds provided a sufficient outflow channel to the southwest.

Winona was forecast to move northward along the western periphery of the subtropical ridge upon entering the South China Sea. However, a 500 mb synoptic track completed by the 54th Weather Reconnaissance Squadron at 1512007 showed that a second ridge had developed east of Taiwan, resulting in a steering flow over the South China Sea

toward the west-northwest. The 1518002 and subsequent forecasts reflected this new information and projected Winona on a west-northwestward track, with landfall expected southwest of Hong Kong.

After reaching maximum intensity on 16 July, Winona weakened as wind shear in the mid- and upper-layers increased. Winona became an exposed low-level system as its convective center was sheared to the southwest early on 17 July. By 170500Z, Winona was downgraded to a tropical depression as it passed 40 nm (74 km) north of Hai-Nan Island (See Figure 3-09-3). Further dissipation as a significant tropical cyclone occurred as it moved toward the China-Vietnam coastline on 18 July.



## TYPHOON ANDY (10)

Andy formed on the northern edge of a zone of maximum cloudiness associated with the monsoon trough south of Guam. Prior to 22 July, the low-level westerlies were well established along 10N and extended eastward to the dateline. Satellite imagery on 20 July showed this maximum cloud zone had begun to segment. Within 24 hours the cloudiness consolidated into three distinct masses centered near 132E, 148E and 168E. Each cloud mass was poorly defined but had rudimentary banding features. The cloud system centers near 148E and 168E drifted westward, intensified, and became Typhoon Andy and Super Typhoon Bess (11) respectively. The cloud mass near 132E drifted westward and was disrupted by the combined effects of the rugged terrain over the Philippines and vertical wind shear from a tropical upper-tropospheric trough (TUTT).

A Tropical Cyclone Formation Alert (TCFA) was issued for the area south of Guam

at 2119002 due to significant pressure falls (to below 1004 mb), increased convection, and convective organization. Aircraft reconnaissance at 2202292 located a small, tight circulation center with a minimum sea level pressure of 995 mb. These data, along with observed winds of 35 to 40 kt (18 to 21 m/sec) prompted the issuance of the first warning. Although intensification was evident from 20 to 24 July on satellite imagery, the cloud pattern remained poorly defined and the circulation center was difficult to position—except for a brief period on 23 July, when the low-level center was visible on the satellite imagery. Aircraft reconnaissance was an invaluable asset during this period; no other reconnaissance platform was capable of following the low-level wind center, particularly since there was considerable interest on Guam as the fix data received implied an anticyclonic loop 35 nm (65 km) in diameter just 90 nm (167 km) south of the island.

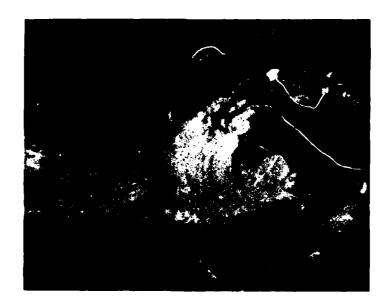


Figure 3-10-1. At 240530Z July Andy, shortly after reaching typhoon strength, is shown 125 mm (232 km) west of Guam (see arrow). During this time the strong south-westerly fetch south of Typhoon Andy brought phenomenal surf to Guam. (NOAA 7 visual imagery)

While Andy was undergoing the loop south of Guam, several meteorological factors were influencing the synoptic situation. Rawinsonde observations from Chichi Jima (WMO 47971) at 221200Z and 230000Z revealed 500 mb height falls of 10 to 20 meters. These falls indicated a weakening of the subtropical ridge north of Andy as well as a lessening of the steering current, factors probably accounting for Andy's lack of forward movement. In addition, reconnaissance aircraft consistently reported Andy's 700 mb center 10 to 20 nm (19 to 37 km) south of the surface center. This tilt, half of the diameter of the loop, suggests that Andy's

actual movement during this period might have been virtually nil, and may have been more related to the fix accuracies and the internal dynamics of the developing tropical cyclone. However, for best track purposes, this period is described well by the loop.

After completing the loop, Andy accelerated to the northwest and intensified. In Andy's wake, Guam experienced phenomenal surf on exposed southern and western beaches as a strong southwesterly fetch was brought to bear on the island on 24 July (See Figure 3-10-1). Andy's northwestward track turned abruptly toward the west as the cyclone

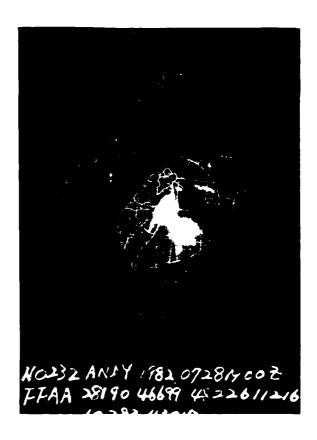
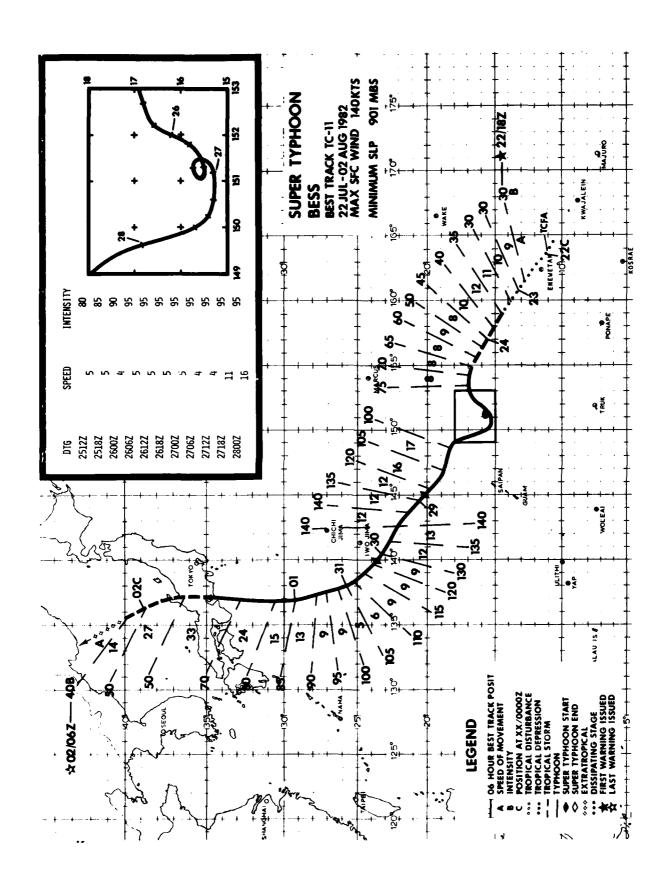


Figure 3-10-2. Typhoon Andy as seen by radar from Hua Lien (WMO 46699) at 2819002 July (Photograph courtesy of Central Weather Bureau; Taipei, Taiwan)

reached 18N on 25 July. This track change occurred while reported 500 mb heights rose at Chichi Jima, to the northeast of Andy. From this point onward, Andy remained equatorward of and parallelled the subtropical ridge axis.

While Andy was tracking westward, upperlevel outflow channels to the east (south of the TUTT axis) and to the southwest (return flow from the monsoon over southeast Asia) provided a favorable environment for intensification. At 271800z, Andy reached a maximum intensity of 120 kt (62 m/sec). Until making landfall upon the southern portion of Taiwan on 29 July (See Figure 3-10-2), Andy's intensity remained over 100 kt (51 m/sec). Taiwan experienced torrential rains from the typhoon's passage; especially hard hit was the eastern coastal area, where considerable damage from flooding was reported. Weakened from Taiwan's rugged terrain, Andy continued westward, across the Formosa Strait, and dissipated in the mountainous area of southeastern China on 30 July.



Bess formed at the eastern end of a maximum cloud zone associated with the monsoon trough anchored south of Guam. By 21 July: this area of cloudiness had separated into three masses near 132E, 148E, and DEE. The two easternmost cloud masses continued to develop and became Typhoon Andy (10) and Super Typhoon Bess. The third area dissipated over the Philippine Islands.

A Tropical Cyclone Formation Alert was issued for an area near 11N 165E at 2119002. Observations from Kwajalein (WMO 91336) and Ailinglaplap (WMO 91367) showed that sea level pressures had continued to fall in the region, and satellite imagery indicated increased convection and organization in the cloud system.

The first warning, with maximum winds of 30 kt (15 m/sec), was issued at 221800Z when the curvature of loosely organized cloud bands into the central cloud mass increased. Initial forecasts for Bess indicated a track toward the northwest, in response to an east-southeasterly flow at low- and mid-levels. Reconnaissance aircraft missions during the period 222200Z to 232200Z indicated that the surface and 700 mb centers were not well-aligned vertically. Once this feature was eliminated, Bess began to intensify and by 241800Z, it was upgraded to typhoon strength based upon satellite imagery which indicated a 30 nm (56 km) eye had developed.

Bess maintained its northwestward track for the first 48 hours in warning status. However, by 241800Z a noticeable decrease in the speed of movement was observed as Bess began to move toward the west-northwest. This change in motion was thought to be the result of westward building of the subtropical ridge to the north. Consequently, the forecast track was changed to a more westward heading. Contrary to JTWC expectations, Bess took a turn toward the southwest at 251200Z. Subsequent analysis of satellite imagery indicates that a short wave trough had just passed to the north of the circulation. The enhanced northwesterly flow behind this

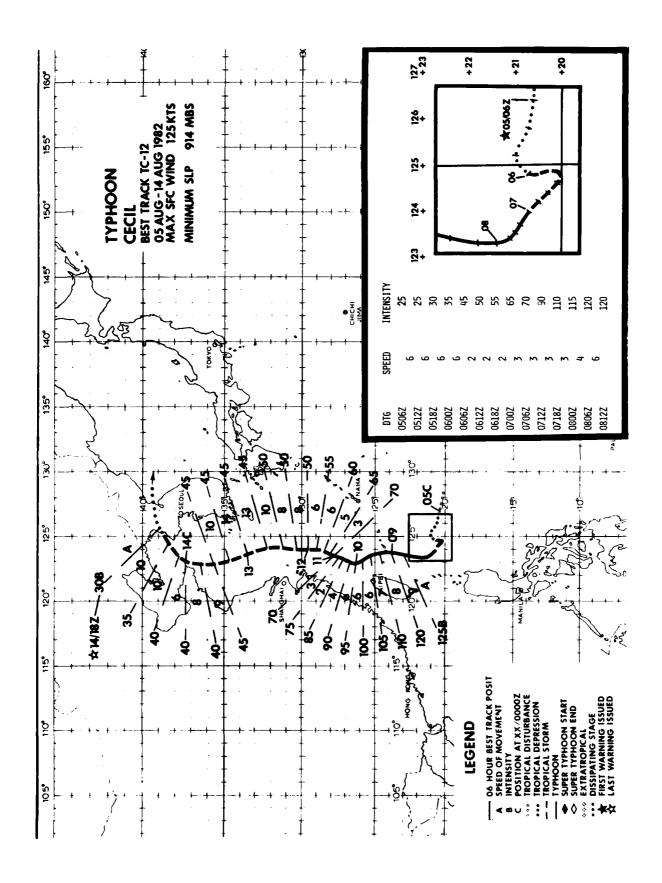
trough forced Bess toward the southwest. During this period, Bess slowed to 5 kt (9 km/hr) and completed a 20 nm (37 km) diameter cyclonic loop, while its intensity remained at 95 kt (49 m/sec). Further intensification did not occur and Bess remained on its southwestward track until another short wave trough moved eastward from Japan on 27 July. In response to this trough, Bess took a noticeable turn north-northwestward until 2806002 when Bess began moving toward the northwest along the southwestern extension of the subtropical ridge. While moving northwestward, a rapid intensification period began, culminating in the attainment of super typhoon strength and a peak intensity of 140 kt (72 m/sec) at 2906002.

As Bess approached 25N, a decrease in forward movement was observed: numerical forecast fields and the JTWC 500 mb analysis of 30 June indicated a weakness forming the subtropical ridge over the southern islands of Japan which would allow Bess to take a more northward track. As Bess entered the south-southeasterly flow associated with the western periphery of the subtropical ridge, interaction with the midlatitude westerlies was expected to occur within 36 hours and Bess was forecast to recurve along the southern coast of Japan. Bess, however, maintained a northward track. The Typhoon Acceleration Prediction Technique TAPT (Weir, 1982) was employed, and correctly forecast significant acceleration commencing near 28N. From this latitude, Bess did begin to accelerate toward the north and eventually merged with a low pressure center in the Sea of Japan on 02 August.

Bess passed over the Araumi Peninsula on central Honshu where extensive damage and human suffering were reported. The greatest damage was caused by torrential rainfall which set off 1,557 landslides and flooded over 27,000 homes, leaving 25,000 persons homeless, and 59 dead. More than 25 ships ran aground or were lost, over 100 bridges were washed out, and nearly 300 acres (741 hectares) of farmland were flooded.



Figure 3-11-1. Super Typhoon Bess at maximum intensity. 2904302 August (NOAA 7 visual imagery).



The tropical disturbance which later became Typhoon Cecil was first distinguishable as a low-level circulation about 250 nm (463 km) north of Truk (WNO 91334) on 31 July. This disturbance persisted as a closed circulation on the surface streamline analyses and as an area of enhanced convective activity on satellite imagery that travelled westward along the monsoon trough for the next four days. Although mentioned in four consecutive Significant Tropical Weather Advisories (ABEH PGTW), a Tropical Cyclone Formation Alert (TCFA) was not issued on the system

during this period because a strong easterly flow at upper-levels was expected to inhibit development of the disturbance. Figure 3-12-1 is typical of the upper-level (200 mb) flow during this period. On 4 August, increased convective activity was apparent from satellite imagery, ship reports in the area indicated that central pressures had dropped to 1000-1003 mb and weakening of the upper-level easterlies was indicated by the 200 mb analysis data. When it became evident that the disturbance had indeed intensified, and that further intensification was likely, a TCFA was issued at 041400z.

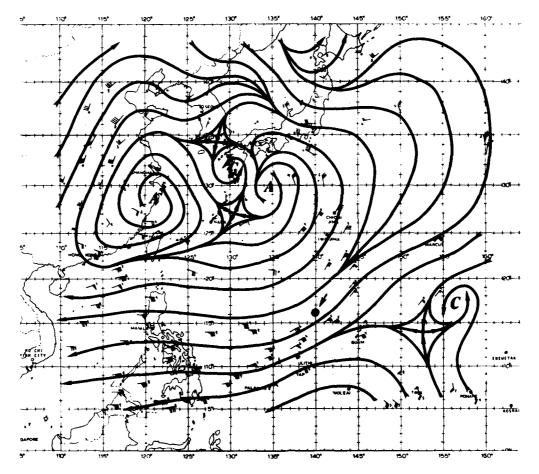


Figure 3-12-1. 0300007 August 200 mb streamline analysis. The location of the surface circulation is indicated by the dark circle.



Figure 3-12-2. 0818382 August (NOAA 7 infrared imagery).

The first warning on Tropical Depression 12 was issued at 0506002 after an aircraft reconnaissance mission observed sustained winds of 25 kt (13 m/sec) associated with the circulation. Tropical Depression 12 continued to track westward under the influence of easterly steering currents along the southern periphery of the subtropical ridge. Upgraded to tropical storm status on 6 August, Cecil turned southward, slowed to 3 kt (6 km/hr), and then turned northwestward. From 6 to 8 August, Cecil intensified from 35 kt (18 m/sec) to 115 kt (59 m/sec), reaching a peak intensity of 125 kt (64 m/sec) at 0818002 while located 120 nm (222 km) east of Taiwan (figures 3-12-2 and 3-12-3).

As Cecil approached Taiwan from the southeast, its track turned sharply northward until reaching 25N when Cecil once again assumed a more northwestward track. Although Cecil never approached closer than 80 nm (148 km) to Taiwan, heavy rains associated with its peripheral circulation touched off landslides which killed at least 19 people in Wu-Koo County, near Taipei.

On 10 August, Cecil turned toward the north-northeast and the combined effects of colder ocean temperatures, vertical wind shear, and cooler surrounding air began to take their toll. Within three days after reaching maximum intensity, Cecil was downgraded to a tropical storm.

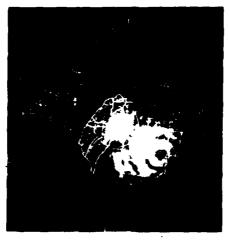


Figure 3-12-3. Typhoon Cecil as seen by radar from Hua Lien (WMO 46699) at 0819007 August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).

As a tropical storm, Cecil continued to move northward in response to steering from an extension of the subtropical ridge which had built northward into the Sea of Japan. The situation at 500 mb is illustrated by the 1012002 August 500 mb streamline analysis (Figure 3-12-4) which is typical of the mid-level synoptic pattern during Cecil's northward movement.

By 14 August, Cecil, located near 38N 124E, was beyond the northward influence of the subtropical ridge and entering an area of westerly flow. Cecil moved eastward in

response to its new environment and made landfall on Korea with 35 kt (18 m/sec) winds. Although, at this time, Cecil was a weak storm in terms of wind intensity, there was a great deal of precipitation associated with the circulation. Heaviest rains, 21.2 inches (55 cm), were recorded in Sanchong, resulting in severe flooding which left 35 dead, 28 missing, and 42 injured in addition to an estimated 30 million dollars in property damage. Cecil's circulation was unable to reorganize after crossing the Korean peninsula and dissipated in the Sea of Japan on 15 August.

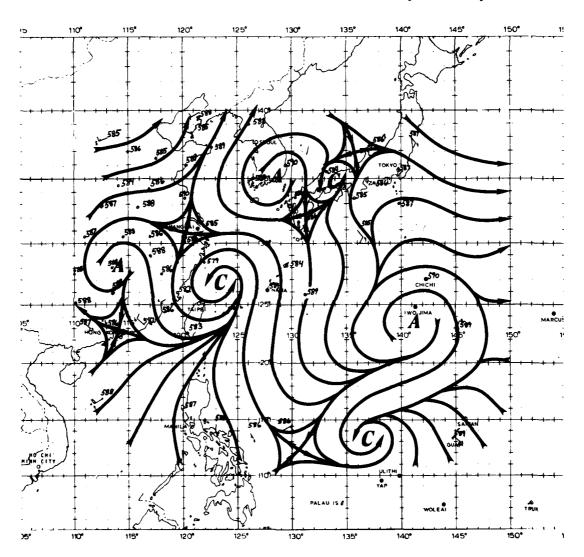
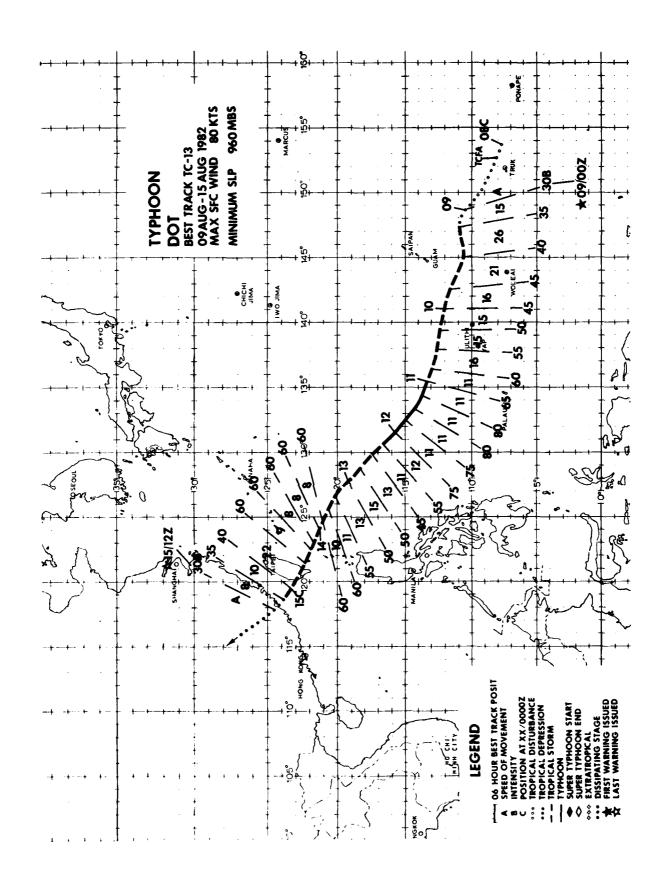


Figure 3-12-4. 1012002 August 500 mb streamline analysis.



The origins of Typhoon Dot can be traced back to a weak surface circulation located near Kwajelein (WMO 91366) on the 5th of August. Surface winds associated with this circulation were 5 to 10 kt (3 to 5 m/sec) and the minimum surface pressure was 1008 mb. Over the next two days, as the circulation drifted northwestward, it remained fairly weak with loosely organized convection and light winds. On 8 August, a reconnaissance aircraft mission into the area showed that the circulation had maximum sustained winds of 20 kt (10 m/sec) but that the surface circulation was still very broad with relatively unorganized convection. However, satellite imagery and 200 mb data indicated that an upper-level anticyclone was present in the area, although not vertically aligned with the surface center. A Tropical Cyclone Formation Alert (TCFA) was issued at 0805002 based upon the persistence of the system and the presence of upper-level conditions that could lead to intensification of the disturbance. The initial warning on Tropical Depression 13 was issued at 0900002 when satellite imagery indicated that the cloud pattern associated with the developing depression was becoming more organized along with increased convective activity.

A reconnaissance aircraft mission at 090118Z observed surface winds of 35 kt (18 m/sec) and an extrapolated minimum sea

level pressure of 1003 mb. Based on these data, Tropical Depression 13 was upgraded to Tropical Storm Dot at 0906002. During this period, the subtropical ridge was well established to the north of the system; thus Dot was forecast to track westward and to continue to intensify. Dot lived up to these expectations, moving westward and reaching typhoon strength on 11 August. However, after reaching a maximum intensity of 80 kt (41 m/sec), Dot began to weaken as upper-level outflow channels became restricted due to interaction with Typhoon Cecil (12) located to the northwest. This interaction located to the northwest. is easily seen on satellite imagery (Figure 3-13-1 shows the early stages of this interaction); at this time, Cecil was located northeast of Taiwan with maximum winds of northeast of Taiwan with maximum winds of 90 kt (46 m/sec) and Tropical Storm Dot, with maximum sustained winds of 50 kt (26 m/sec), was rapidly intensifying and would achieve maximum sustained winds of 80 kt (41 m/sec) on the following day. Although there was some interference in the upper-level outflow between the two cyclones, Dot's outflow channels to the northeast and southwest were well established. Figure 3-13-2 shows the relationship between the two cyclones two and one-half days later. Although the satellite pass was not optimally located, features of interest are readily observable, i.e., Dot's outflow channels to the north were completely cut off by the strong northeasterly winds associated with Cecil's outflow. The 200 mb analysis for



Figure 3-13-1. Satellite imagery shows Typhoon Cecil at the upper left and Tropical Storm Dot at the lower right. 1005292 August (NOAA 7 infrared imagery).

Figure 3-13-2. Satellite imagery shows Tropical Storm Cecil at the upper left and Tropical Storm Dot at the lower left. 1217502 August (NOAA 7 infrared imagery).

this period (Figure 3-13-3) shows that flow was unidirectional over Dot, with no indication of an anticyclone at that level.

As the distance between Cecil and Dot increased over the next few days, Dot regained intensity, reaching maximum sustained winds of 60 kt (31 m/sec) on the 13th. Figure 3-13-4 shows the relationship between Dot's intensity and the separation between the two cyclones. The data indicate a correlation between separation and Dot's intensity once the separation distance fell below 1000 nm (1852 km).



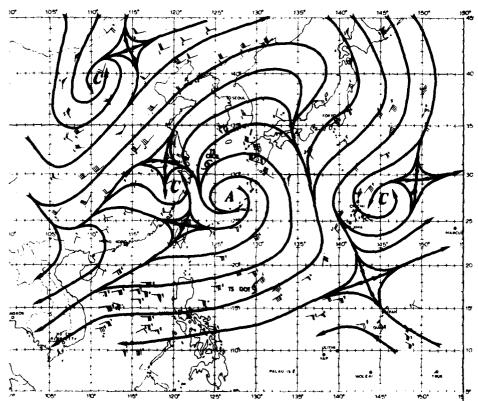


Figure 3-13-3. 1212002 200 mb analysis with surface position of Tropical Storms Cecil and Dot superimposed.

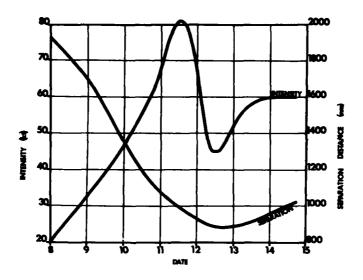


Figure 3-13-4. Variation in intensity as a function of time and separation between Dot and Cecil.

As Dot continued westward along the southern periphery of the subtropical ridge, several forecasts were issued indicating Dot would follow Cecil and turn toward the north prior to reaching Taiwan. However, the subtropical ridge was reestablished in the region to the north of Taiwan after Cecil's passage; subsiding air between the two tropical cyclones probably contributed to the ridging in this area, thereby causing Dot to continue its movement westward toward Taiwan. Although Dot's passage over

Taiwan was rapid, the rugged topography of the island had a devastating effect on Dot's low-level circulation. Figure 3-13-5 shows Dot as a well-organized tropical storm with maximum sustained winds of 60 kt (31 m/sec) prior to landfall. Figure 3-13-6 shows Dot 12 hours later in the Formosa Strait, barely distinguishable as a tropical storm. Dot never recovered from the effects of this crossing and dissipated less than a day later over the mountainous regions of eastern China.



Figure 3-13-5. Tropical Storm Dot was approaching Taiwan from the southeast, as seen by radar from Hua Lien (MMO 46699) at 1414002 August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).

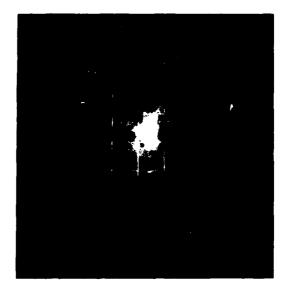
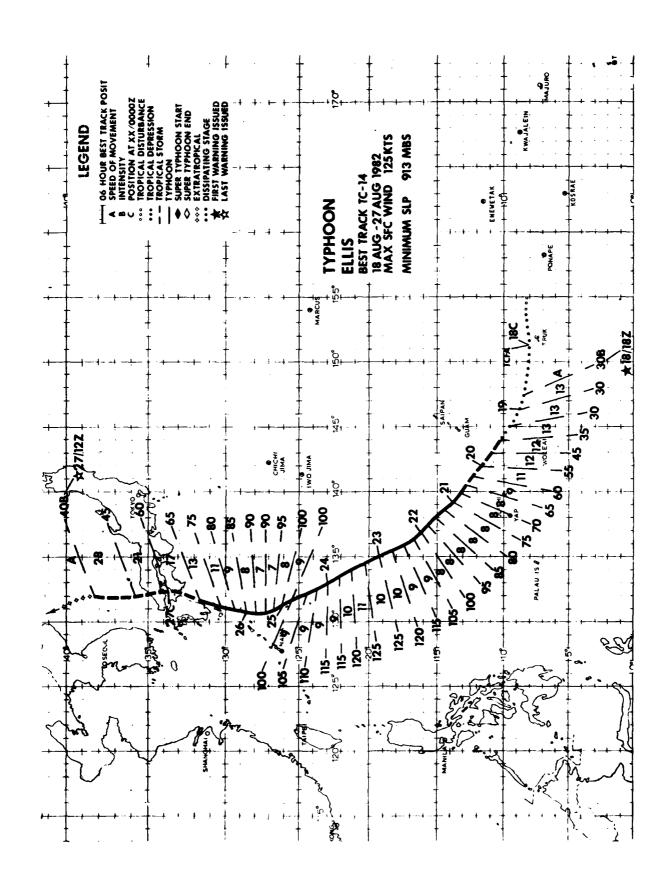


Figure 3-13-6. Tropical Storm Dot, located in the Formosa Strait after crossing southern Taiwan, as seen by radar from Kao-hsiung (MMO 46744) at 1502002 August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).



## TYPHOON ELLIS (14)

Typhoon Ellis developed from a disturbance that was first detected within the monsoon trough south of Ponape on 15 August. From initial detection to the issuance of a Tropical Cyclone Formation Alert (TCFA) on 18 August, the disturbance slowly acquired convective organization. Once organized, development was quite rapid, with Ellis reaching a peak intensity of 125 kt (64 m/sec) on 23 August.

The TCFA was issued at 1801002 when satellite imagery identified a cloud mass near 8N 151E that had acquired an upper-level outflow channel to the southwest. At 1804022, the initial reconnaissance aircraft mission located a 20 kt (10 m/sec) circulation center 85 nm (157 km) northwest of Truk Atoll. During the next 24 hours, satellite imagery provided fix positions on the convective center that showed movement toward the west-northwest at speeds approaching 16 kt (30 km/hr).

Based on continued convective organization, the first warning was issued

for Tropical Depression 14 at 1818002. At 1911082, data from the second reconnaissance aircraft mission indicated maximum winds of 35 kt (18 m/sec) were present and, at 1912002, Tropical Depression 14 was upgraded to Tropical Storm Ellis. On the 19th Ellis began tracking more northwestward in response to weaker steering currents south of 15N. From the first warning until the seventh warning (2006002) the forecast scensrio anticipated an initial jog to the northwest then, as Ellis began interacting with the subtropical ridge, it would return to a more westward heading. However, a deep mid-latitude trough (near 40N 115E at 2000002) began to weaken the subtropical ridge southwest of Japan and the anticipated westward movement never materialized. By 2012002, the effects of this mid-latitude trough on the strength of the subtropical ridge became evident and the forecast track was shifted toward the northwest.

On 20 August, satellite imagery (Figure 3-14-1) indicated the development of a banding-type eye. Ellis was upgraded to typhoon strength at 210000Z when both

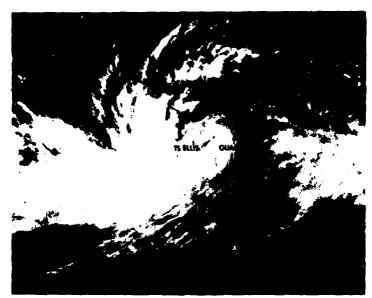


Figure 3-14-1. As an intense tropical storm, Ellis was exhibiting a strong southwest upper-level outflow pattern during a period when a banding-type eye was forming. 2005102 August (NOAA 7 visual imagery).



Figure 3-14-2. Typhoon Ellis, with strong upper-level outflow to the east and the southwest, was nearing a peak intensity of 125 kt (64 m/sec) at 2217302 August (NOAA 1 infrared imagery).

aircraft and satellite data supported an intensity greater than minimum typhoon strength (64 kt (33 m/sec)). In the following days, Ellis continued to develop rapidly, passing 100 kt (51 m/sec) intensity on 22 August and peaking at 125 kt (64 m/sec) on 23 August. Figure 3-14-2 shows Ellis just seven hours prior to reaching its maximum intensity.

By 230000Z, significant height falls were evident in the mid-tropospheric levels along the Ryukyu Islands, northwest of Ellis. The mid-latitude trough which had previously influenced Ellis's northwestward track was moving into the Yellow Sea. A day earlier, Ellis had shifted to

a north-northwestward track as the subtropical ridge continued to weaken south of Japan. Interestingly, the 14 warnings issued from 221800Z to 2600000Z consistently identified Ellis track within 30 nm (56 km) of the eventual best track up to 29N. During this period, both the analyses and numerical forecast fields maintained a very good relationship between the mid-latitude trough near Korea and the subtropical ridge, east of Japan.

As Ellis moved east of Okinawa on 25 August (Figure 3-14-3) its movement shifted toward the north. As early as 240000Z, JTWC forecasts began to anticipate this movement



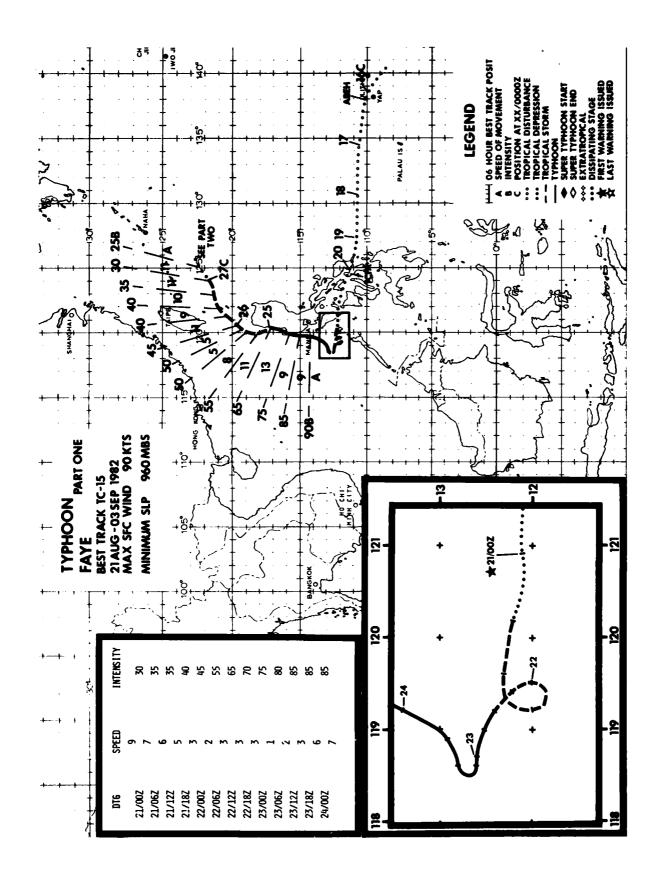
Figure 3-14-3. Typhoon Ellis, located 140 mm (259 km) east of Okinawa, was approaching the mid-latitude westerlies and subsequent acceleration toward the north. 2505512 August (NOAA 7 visual imagery).

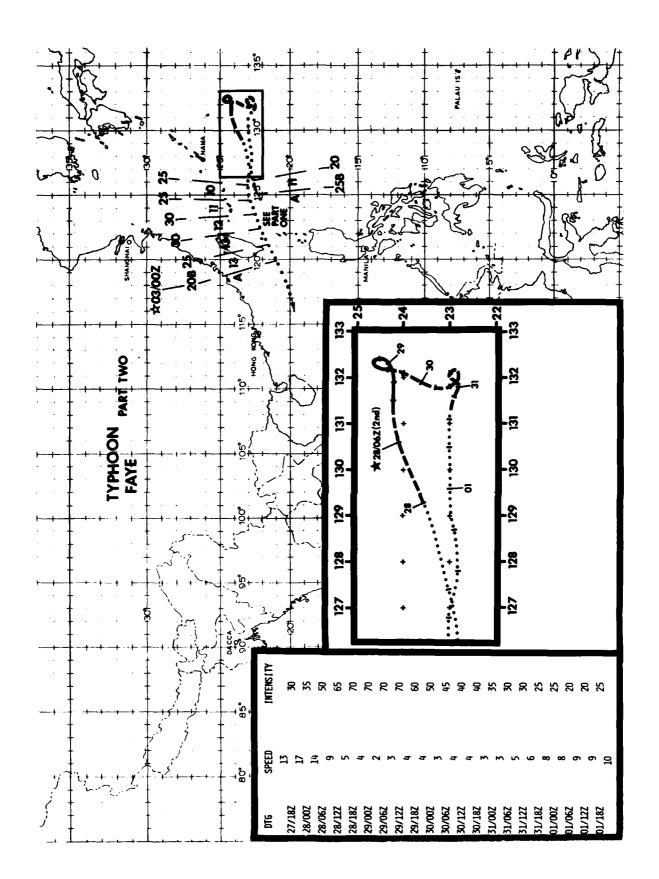
as well as significant acceleration as Ellis approached 28N, based on guidance from the Typhoon Acceleration Prediction Technique (TAPT) (Weir, 1982). Unfortunately Ellis slowed to 7 kt (13 km/hr) while approaching 28N and the early acceleration forecasts became premature in the timing of the initial acceleration. However, as Ellis crossed 28N, the predicted acceleration occurred and the speeds attained were very close to those predicted by TAPT.

Once the acceleration was underway, Ellis commenced a more rapid weakening trend as the combined effects of increasing vertical wind shear and interaction with the topography of Kyushu, Skikoku and western Honshu reduced Ellis to an estimated 45 kt

(23 m/sec) intensity as it entered the Sea of Japan.

Ellis moved toward the north-northeast on 26 August and passed along Kyushu's eastern coastline and then just west of Hiroshima on 27 August. This jog to the north-northeast was costly for the region, as torrential rains (as much as 28 inches (71 cm) in 24 hours), flooding, landslides, and high winds brought much of southwestern Japan to a virtual standstill. Having left much of its fury behind, Ellis entered the of Japan on 27 August and rapidly transled into an extratropical low pressure symbol which would later move northwestward, passing 120 nm (222 km) west of Vladivostok, USSR.





Typhoon Faye (15) proved to be one of the more difficult tropical cyclones to forecast during the 1982 season (Figure 3-15-1). With forecast errors of 142, 384, and 629 nm (263, 711, and 1182 km) for 24, 48, and 72 hours, respectively, the forecast history for Typhoon Faye is a good example of what can happen when there is confusion in understanding the effect that the large-scale flow field and other larger tropical cyclones can have on a very small but intense cyclone. In this report the life history of Typhoon Faye is depicted in table form with seven segments (Table 3-15-1).

For each segment, key events along with the basic forecast philosophy and prognostic reasoning are described. A brief post-analysis description is then presented in order to compare the actual events of the tropical cyclone and the synoptic situation. In this presentation it will be evident how a basically sound and logical forecast can go astray when all the "facts" are not completely understood. Furthermore, an attempt has been made in this table to describe for the reader the basic forecast/thought process at the JTWC. Figures 3-15-2 to 3-15-7 depict several events along Typhoon Faye's track.

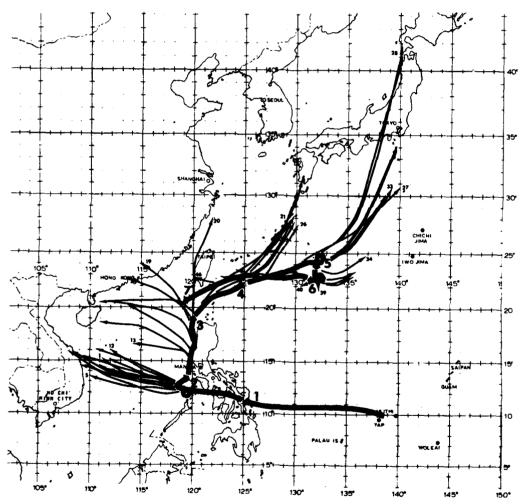


Figure 3-15-1. ITM Mindshield-wiper Chart. This chart depicts the forecast track for each warning issued for Faye. I deally, in a well-handled forecast situation, there is not a "windshield-wiper" (back and forth) effect but a superposition of one forecast track upon another. Forecast segments will be described in Table 3-15-1.

TABLE 3-15-1

Segment	Time Period (Warnings) *Events	Prognostic Reasoning	Post-analysis Discussion
-	16/00Z - 20/00Z Aug (none)  *Weak disturbance moves westward in the Philippine Sea toward the southern Philip- pines *Monitoring distur- bance for indication of convective develop- ment	Although an exposed low-level circulation could be identified on satellite imagery as well as on synoptic data, little development was expected due to the proximity of the Philippines and the dominance of the flow pattern around Typhoon Ellis (14) near Guam.	Little difference from prog reasoning. An upper-level anticyclone did develop over the area when an upper trough moved between the system and Ellis; however, convection remained unorganized due to orographic influences from the Philippines.
2	20/00Z - 24/00Z Aug (#1 - #12)  *System organizes in the South China Sea *Tropical Cyclone Formation Alert at 200203Z *ist warning at 210000Z in South China Sea *Upgrading to tropical storm status at 210600Z *Upgrading to typhoon status at 221200Z	Movement: Subtropical ridge in the vicinity of Hong Kong was forecast by the FNOC models to persist and strengthen during the forecast period. This would cause the system to slowly increase its forward speed toward the west-northwest. All objective aids predicted a west to northwest movement.  Intensification: Dominance of both the upper- and lower-level flow by Ellis in the Philippine Sea, as well as slight northerly shear from the 200 mb ridge over China, was expected to prevent much intensification.	Movement: The dominance of Ellis, as well as the slow encroachment of a frontal zone from central China, prevented much building of the ridge over Hong Kong resulting in weak steering flow near Faye - especially in the lower layers. Faye showed little trend in movement until a frontal/shear zone reached southeastern China on 23-24 Aug (height falls were seen at 500 and 700 mb throughout region).  Intensification: Although the adverse vertical shear had an effect on the cyclone, it resulted in a small, restricted system rather than a weak one. A small TUIT cell which was analyzed near Hai-nan Island on 22 Aug appeared to aid Faye's upper-level outflow toward the northeast.
3	24/00Z - 25/18Z Aug (#13 - #19)  *System continues northward *System reaches greatest strength (90 kt (46 m/sec)) at 240600Z  *System reaches Luzon at 241800Z with significant damage to Wallace Air Station at 242200Z with gusts up to 100 kt (51 m/sec) *Downgrading to tropical storm status at 250000Z	Movement: A persistent northward movement was expected during the initial 24 hours with a more climatological northwestward track in the outlook period. Although the daily analysis indicated that the subtropical ridge over China was moving north and weakening, FNOC prog series continued to call for a gradual strengthening of the ridge with time. Further support of this prognosis was seen in the expected quick movement of Ellis toward the north. Since Ellis was dominating the subtropical regions between 20-30N, its acceleration to the north and out of the subtropics, would allow for the eventual reintensification of the ridge. Finally, a forecast of westward movement continued to be predicted because of two primary reasons: the hesitation to break from the forecast philosophy maintained through the first 19 forecasts and the almost total lack of climatological tracks eastward of the South China Sea.  Intensification: Little change from the forecast reasoning in Segment 2. Although northeasterly vertical shear from Ellis continued to dominate, it was now generally thought that Faye would remain strong in spite of the adverse synoptic environment. Only after Faye made landfall on Luzon was a gradual weakening trend predicted.	Movement: Inspite of predictions to the contrary by the FNOC prog series, the ridge over southern China continued to retreat northward and weaken as strong troughing dominated the region between Ellis and Faye. This resulted in an almost due northward movement of Faye. Toward the end of this period, low- to mid-level westerly flow began to strengthen in the Luzon Strait while Ellis slowed its forward speed to 7 kt (13 km/hr) just east of Okinawa. Intensification: Faye continued to intensify until its circulation pattern began to interact with the mountainous terrain of western Luzon. Once landfall was made at 241800Z, a steady deterioration was observed as Faye had trouble maintaining good vertical alignment. The cause of this poor alignment appeared to come equally from the orographic effects of Luzon and the strong vertical shear north of Luzon initiated by Ellis's outflow pattern.

Segment	Time Period (Marnings) *Events	Prognostic Reasoning	Post-analysis Discussion
4	25/18Z - 27/06Z Aug (#20 - #26) *System begins to move northeastward at 251800Z *Initial final warning at 270600Z		Movement: Initial northeast movement was well predicted; however, toward the end of the period the low-level flow began to split in the vicinity of Faye with a portion of the flow moving northward into the trough and the other portion moving east-southeastward toward the newly developed Tropical Storm Gordon (16). Faye began to follow this more east-ward track near the end of the period. Intensification: Upper-level shear from the remains of Ellis continued to hamper Faye's efforts to reintensify. This adverse environmental effect reduced Faye to an exposed low-level circulation with only a few isolated convective cells.
5	27/06Z - 29/18Z Aug (#27 - #33)  *System continues on a east-northeastward track *System reintensifies to tropical storm status at 280000Z *JTWC resumes warning status at 280600Z *System intensifies to typhoon strength at 280900Z *System weakens to tropical storm strength at 291500Z	Movement: After Ellis moved north of Japan, the long wave trough was positioned over western Japan and the Sea of Japan. Since FNOC Progs predicted little change in pattern, a forecast track toward the northeast appeared the most logical. This was also supported by the CYCLOPS steering aids and the dynamic models. The JTWC TAPT technique - which keys on the 200 mb flow - predicted rapid acceleration toward the northeast north of 25N was likely. The direction of movement was predicted along the 500 mb flow. Intensification: Wind intensities were forecast based on persistence in the near term and gradual weakening with increasing latitude in the outlook period.	Movement: Although the upper trough remained over Japan as predicted, Faye perhaps due to its small size, failed to entrain into this flow or move north of 25N. Instead it appeared to be trapped within the low-level trough between Faye and Gordon and after 281800Z it became quasi-stationary. This resulted in very large forecast errors for this period.  Intensification: Once Faye moved out of the strong shearing environment, rapid intensification occurred. Faye went from a weak tropical depression to a typhoon in 27 hours. This reintensification was not well predicted nor was its extremely small size (smaller than that observed in the South China Sea). Aircraft at this time measured maximum surface winds of 70 kt (36 m/sec) out to only 10 nm (19 km) from the center and 30 kt (15 m/sec) winds out to 60 nm (111 km).



Figure 3-15-2. (Segment 1) Faye, as a tropical depression, crossing the southern Philippines. Although wind speeds were generally less than 25 kt (13 m/sec), widespread damage to property and agriculture was reported by Philippine newspapers due to blooding. 2006522 August (NOAA 7 visual imagery).

Segment	Time Period (Warnings) *Events	Prognostic Reasoning	Post-analysis Discussion
6	29/18Z - 31/06Z Aug (#34 - #39) *System shows little trend in movement and continues to weaken	Movement: Since it was apparent that Faye was not responding to the mid-latitude trough to the north, it was forecast to move eastward with the low-level flow directed toward Typhoon Gordon (16). Initially, movement was expected to be slow since the analysis fields indicated weak steering flow within the trough between Faye and Gordon. Once Gordon moved north, stronger westerlies were expected to accelerate Faye's low-level circulation eastward. Intensification: Dissipation was expected within 24 to 48 hours due to the proximity of Faye to Gordon's strong upper-level outflow pattern.	Movement: During this period, Gordon failed to maintain a steady northward motion. Instead, Gordon slowed its forward speed to 5 kt (9 km/hr). This, in turn, resulted in extremely weak steering flow at all levels around Faye. Toward the end of the period, a ridging pattern began developing over western Japan resulting in a slight increase in northerly and then northeasterly flow. Faye began to move slowly southwestward in response to this flow.  Intensification: Although Faye continued to weaken as predicted, the cause was not from Gordon's upper-level wind pattern but from the movement of an upper trough from China to a position over Faye. This resulted in Faye being stripped of its convection, leaving an exposed low-level circulation.
7	31/06Z Aug - 03/06Z Sep (#40 - #50)  *System weakens to a tropical depression at 310600Z *System drifts westward for three days as an exposed low-level circulation *Final warning issued by JTMC for Faye at 030000Z *System dissipates in the South China Sea at 030600Z	Movement: With the ridge well established north of the system and over western Japan, a predicted westward movement appeared to be best.  Intensification: Aircraft reconaissance indicated that Faye's central pressure had risen to 999 mb and so each warning during this period predicted dissipation within 24 hours.	Movement: Forecast track was fairly accurate although Faye's increase in forward speed to 13 kt (24 km/hr) was not anticipated.  Intensification: Although its wind intensities were only 20-30 kt (10-15 m/sec), Faye managed to survive as a low-level circulation much longer than predicted. Final dissipation did not occur until Faye's exposed low-level circulation became entrained into the monsoon circulation that was to become Typhoon Hope (17) in the South China Sea.

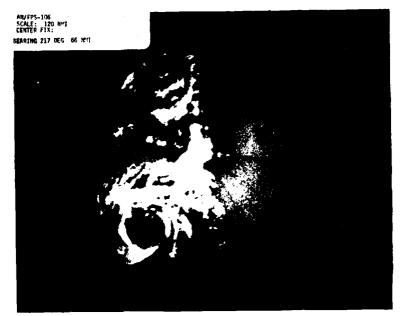


Figure 3-15-3. (Segment 3) The "eye" of Typhoon Faye as seen by radar 66 nm (122 km) southwest of Subic Bay at 2403582 August. (Photograph courtesy of NOCF, Cubi Pt, Republic of the Philippines)

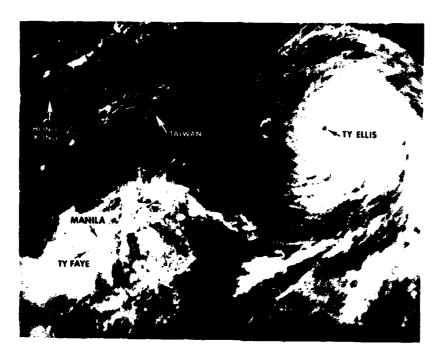


Figure 3-15-4. (Segment 3) Typhoon Faye at full strength, 90 kt (46 m/sec), just south of Luzon. The much larger Typhoon Ellis, 110 kt (57 m/sec), can be seen 925 nm (1713 km) northeast of Faye. 240603Z August (NOAA 7 visual imagery)



Figure 3-15-5. (Segment 4) Tropical Storm Faye just south of Taiwan weakening rapidly at 2605392 August as it moves under the strong upper-level outflow of Typhoon Ellis. (NOAA 7 visual imagery)



Figure 3-15-6. (Segment 6) Tropical Storm Faye, 50 kt (26 m/sec), once again being dwarfed by another tropical cyclone (Typhoon Gordon, 100 kt (51 m/sec)) at 3004517 August (NOAA 7 visual imagery)

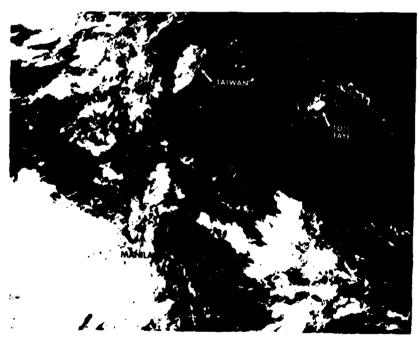
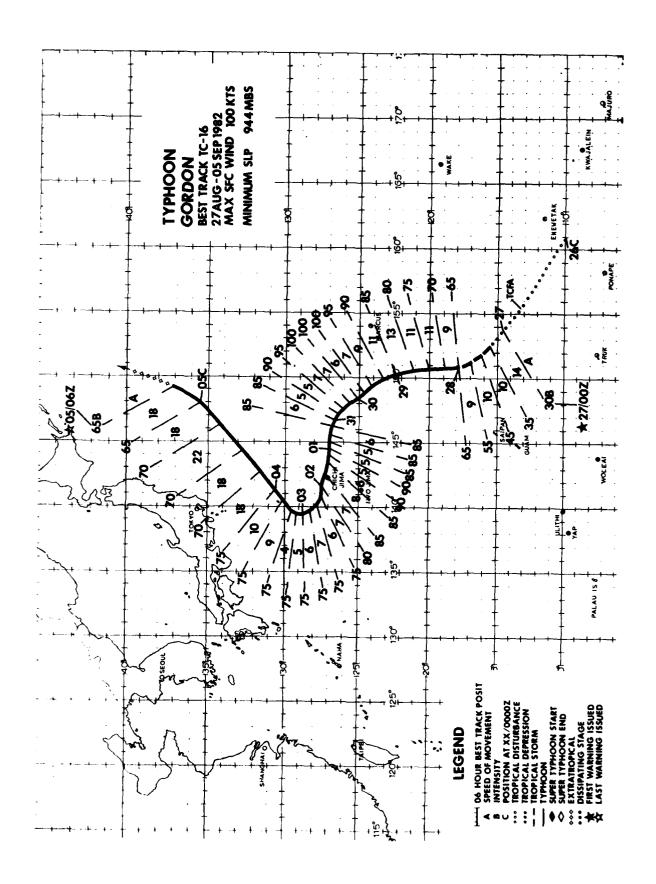


Figure 3-15-7. (Segment 7) An exposed low-level circulation can be seen just east of Taiwan as the remains of Typhoon Faye at 0106087 September. This weak circulation persisted for over three days. (NOAA 7 visual imagery)



Typhoon Gordon developed rapidly from a disturbance which was initially detected while it was embedded in an elongated monsoon trough along 8N between 145E and 175E. Within 48 hours of its initial detection, Gordon reached typhoon strength and eventually proved to be one of the most difficult typhoons of the season for JTWC forecasters.

On 25 August, a surface circulation was detected near 8N 163E associated with an area of strong, yet unorganized convection. During the ensuing 24 hours little increase in convective organization was noted on satellite imagery; however, an uppertropospheric pattern existed nearby that was conducive for further development. Analysis data indicated that outflow channels were readily available via an upper-level anticyclone centered near 10N 167E, further enhanced by a tropical upper-tropospheric trough (TUTT) north of Guam.

Rapid development did not occur until the upper-level anticyclone moved over the surface circulation. A TUTT cell located northwest of the disturbance enabled outflow channels to remain open to all quadrants and resulted in a significant increase in convection on 26 August. A Tropical Cyclone Formation Alert (TCFA) was issued at 261500Z during this burst in convective activity and organization. Synoptic data from Truk Atoll (WMO 91334) and Ponape (WMO 91348) at 261200Z also indicated intensification was occurring as gradient level winds increased to near 30 kt (15 m/sec) at both reporting stations.

A reconnaissance aircraft investigative mission at 262347Z was able to fix a circulation center near 14.5N 154E with associated surface winds of 30 kt (15 m/sec) and a 1001 mb sea level pressure. These data preceded the issuance of the first warning for Tropical Depression 16 at 270100Z. One day later, at 272335Z, reconnaissance aircraft data showed Gordon's central sea level pressure had dropped to

977 mb and surface winds of 65 kt (33 m/sec) were observed in the north semicircle. During this period of intensification, Gordon was upgraded to tropical storm status at 270600Z and typhoon status at 280000Z based on reported aircraft data and steadily increasing cloud system organization. At 291800Z, four days after initial detection, Gordon's rapid intensification ended at 100 kt (51 m/sec) (See Figure 3-16-1).

The forecasts issued by JTWC during Gordon's developing stages anticipated a northwestward movement toward a weakness in the subtropical ridge located near These forecasts anticipated recurvature to occur as Gordon moved north of the ridge axis along 23N and came under the influence of an advancing mid-latitude trough. In response to this synoptic situation, Gordon's forward speed slowed as it approached the ridge axis on 28 August; however, the midlatitude trough continued its eastward movement and by 29 August, its effects on Gordon's movement were no longer evident. Following the passage of this trough, the subtropical ridge was re-established north of Gordon and in response. Gordon resumed a northwestward track along the ridge's southwestern periphery. Forecasts issued on 29 and 30 August reflected
Gordon's continued northwestward movement followed by a northward movement and acceleration toward Japan.

By 31 August, a different forecast scenario was gaining strength. At 310000Z, 500 mb and 700 mb height rises were observed over southern Honshu and north of Gordon, indicating the approaching short wave trough was weakening or moving more northeastward than previously forecast. During this period, Gordon, with 90 kt (46 m/sec) surface winds, was advecting large amounts of warm, moist air from the tropics and thereby strengthening the ridge to the northeast. This strengthening of the ridge, combined with changes in the short wave trough, forced Gordon toward



Figure 3-16-1. Typhoon Gordon near maximum intensity of 100 kt (51 m/sec) 640 nm (1185 km) nontheast of Guam. Typhoon Faye is also seen in this picture south of Okinawa. 2905027 August (NOAA 7 visual imagery).

a more westward track which was maintained until late on 2 September.

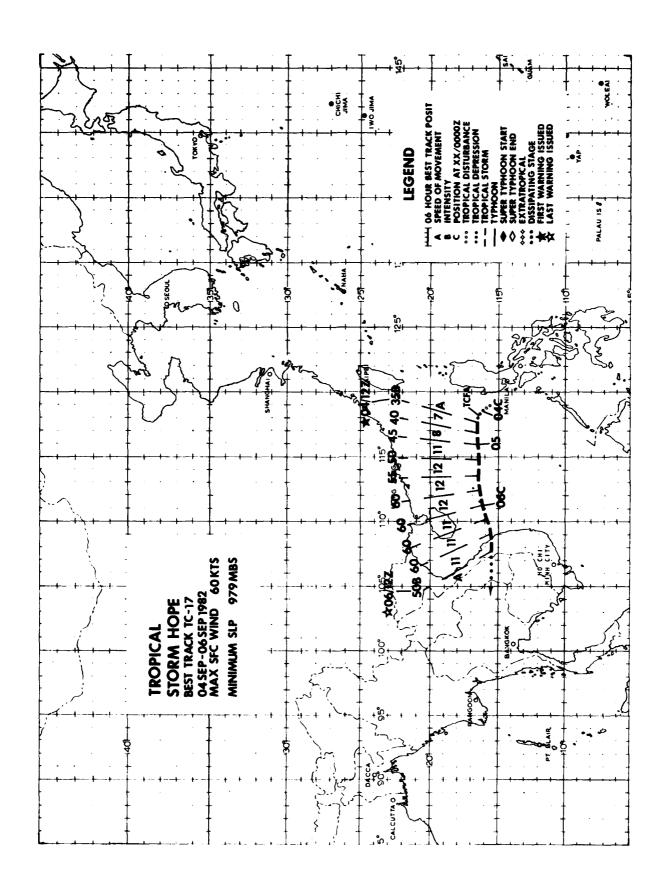
In response to numerical forecast fields which showed a low- to mid-level ridge near Korea building eastward over Japan, JTMC forecasts on 2 September began forecasting a continued westward movement along the southern periphery of the two ridges. By 030000Z, a conflicting forecast scenario began to develop. It was observed that 500 mb and 700 mb heights were falling over southern Honshu, indicating that the short wave trough, located over Hokkaido, was deepening once again. However, the numerical forecast fields provided by Fleet Numerical Oceanography Command (FNOC), Monterey, CA, did not reflect this tendency and continued to build the ridge behind the short wave trough and to the north of Gordon's track. At this time, two opposing forecasts were considered possible: one reflecting the westward track below the

ridge; the other, indicating a sharp recurvature and acceleration toward the northeast in response to the deepening trough. JTWC chose to maintain the westward prediction as the FNOC forecast fields appeared to be a meteorologically sound solution to the synoptic situation. Concurrently, an intensive meteorological watch was instituted whereby conventional analysis data and satellite imagery were closely monitored for indication of any changes which would mandate a change from the westward-moving forecast scenario.

On 3 September, Gordon slowed to 4 kt (7 km/hr) from 7 kt (13 km/hr) and took an increasingly more northward course. This movement, combined with the continued 500 mb and 700 mb height falls over Honshu prompted JTWC to abandon the westward forecast at 0312002, and adopt a forecast toward sharp recurvature and acceleration to the northeast.

Subsequent to the change in the JTWC forecast toward recurvature, the FNOC forecast fields, produced from the 0312002 data base, changed significantly and supported the recurvature scenario. Had the numerical forecast series indicated this trend earlier and not persisted in building the low- to mid-level ridge eastward from Korea, the recurvature track would have been adopted much earlier or perhaps not even abandoned on 2 September. This forecast situation emphasizes the difficulty in issuing credible forecasts when there exists a conflict between the observed short-term changes in the analysis data and the numerically forecast changes beyond the analysis period. There are no easy answers in there situations and unfortunately, in similar future forecast situations, JTWC and its customers may well have to deal with alternating guidance from both analysis and forecast fields.

On 3 and 4 September, Gordon did sharply recurve to the east-northeast as it became embedded in the mid-latitude westerlies along the southeastern periphery of the short wave trough. A fairly rapid accleration to 22 kt (41 km/hr) was observed prior to extratropical transition near 37N at 050600Z. As Gordon recurved, it passed 260 nm (482 km) southeast of Tokyo. The U.S. Naval Oceanography Command Facility at Yokosuka, Japan, reported maximum sustained winds of 32 kt (16 m/sec) with a maximum gust of 44 kt (23 m/sec) during the period, 3 to 4 September. Fortunately, despite some difficult forecast situations, Gordon did not strike any major land mass and there was no significant damage to military or civilian interests in Japan.



## TROPICAL STORM HOPE (17)

Tropical Storm Hope developed from a monsoon depression which formed on 3 September along the northern edge of a strong southwest monsoon flow (25 to 30 kt (13 to 15 m/sec)) that was present over the southern portion of the South China Sea. During the formative stages of this rapidly deepening monsoon depression, shipboard synoptic observations provided essential data which enabled the JTWC to closely monitor the system's development.

At 040345Z, a Tropical Cyclone Formation Alert was issued for an area west of central Luzon when shipboard observations revealed surface pressures had dropped to at least 1002 mb near the depression's center. The 041200Z synoptic data, indicating improved organization in the low-level wind flow, prompted the first warning which was issued at 041500Z. In support of the first two warnings, satellite fix positions - based on a poorly-defined cloud signature - and surface observations did not correlate very well on the system's center. Thus, when a resources permitting aircraft reconnaissance mission at 042357Z located Hope well southwest of the previous warning position, with

maximum winds of 45 kt (23 m/sec) and a 994 mb central sea level pressure, the tropical cyclone was relocated and upgraded to tropical storm status on the 0500002 warning.

During the first 30 hours in warning status, Hope intensified to a peak of 60 kt (31 m/sec) which was maintained until landfall. On 6 September, Hope slammed into the coast of Vietnam, 25 nm (46 km) south of Da Nang, and subsequently dissipated over the mountainous terrain of Vietnam and Laos. Accompanying Hope's demise over Southeast Asia, widespread flooding was reported in Vietnam and northeastern Thailand, resulting in several thousand people fleeing their homes and extensive damage to the season's rice crop.

From the first warning, JTWC forecasts continued to anticipate that Hope would slow its forward movement, or move towards the west-northwest and slow. Hope, however, accelerated towards the west-southwest, paralleling the subtropical ridge axis to the north, and the expected forecast movement was never realized.

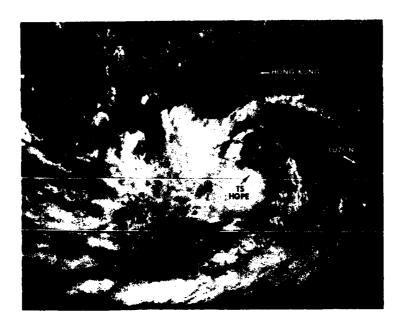
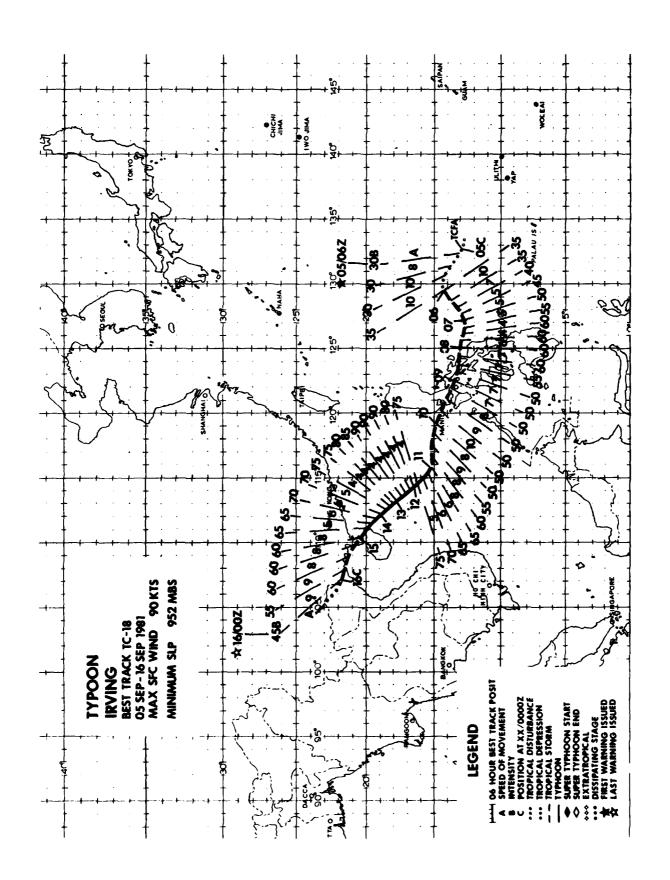


Figure 3-17-1. Tropical Storm Hope near 50 kt (26 m/sec) intensity in the central South China Sea. 0507002 September (NOAA 7 visual imagery).



## TYPHOON IRVING (18)

Typhoon Irving developed within an area of unorganized convection associated with an active monsoon trough anchored south of Guam in early September. Surface pressures throughout the region between 125E to 165E and 8N to 13N were below 1004 mb, and the southwest monsoon flow averaged 20 kt (10 m/sec) over much of the region. By 040300Z, a low-level circulation was evident on visual satellite imagery `ar 11N 130E, although nearby convection had decreased during the preceding 12 hours. During this period, another tropical cyclone was developing in the monsoon trough near 12N 147E (Typhoon Judy (19)). The passage of Typhoon Gordon (16) east of Japan reestablished a low-level easterly flow to the north of both of the developing systems; thus increasing the potential for further development.

As the circulation near 130E (Irving) developed, an increase in cloud organization was seen on satellite imagery which led to the issuance of a Tropical Cyclone Formation Alert at 050000Z. An immediate, abbreviated warning bulletin for Tropical Depression 18

was issued by JTWC at 0508552, when reconnaissance aircraft closed off a surface circulation with observed winds near 30 kt (15 m/sec). Based on continued convective organization, Tropical Depression 18 was upgraded to Tropical Storm Irving at 0518002.

Early in its development, Irving was characterized as an exposed low-level circulation center to the east of the most active convection region of the disturbance. Visual satellite imagery and aircraft reconnaissance data enabled JTWC to follow the surface center, rather than the upperlevel (convective) center, as Irving moved across the Philippine Sea.

Prom 6 to 8 September Irving remained equatorward of a strengthening subtropical ridge and maintained a westward track across the Philippine Sea. Irving made landfall at 0809002, on the southern tip of Luzon (Figure 3-18-1). Maximum winds at landfall were 60 kt (31 m/sec). Thereafter, Irving assumed a more northwestward path (of least resistance) through the Sibuyan Sea

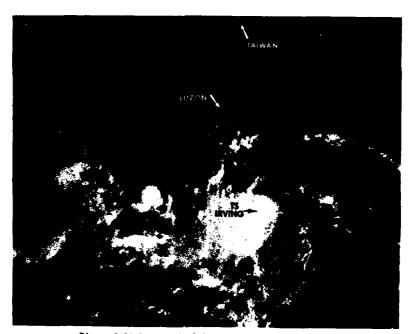


Figure 3-18-1. Tropical Storm Irving near landfall south of Luzon. 0816162 September (NOAA 7 visual imagery)

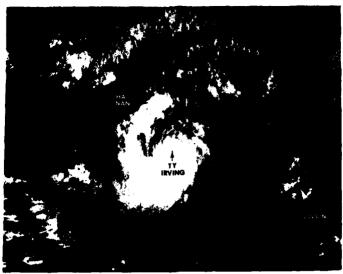


Figure 3-18-2. Typhoon Irving near maximum intensity in the South China Sea. 1307062 September (NOAA 7 visual imagery)

and remained over a marine pathway between the islands of the central Philippines. During this period, Irving maintained much of its intensity although some convective organization was lost. Irving entered the open waters of the South China Sea, 27 nm (50 km) southwest of Cubi Point Naval Air Station at 091700Z. NAS Cubi reported sustained winds of 46 kt (24 m/sec) with a peak gust of 64 kt (33 m/sec) during Irving's transit of the region.

As Irving moved into the South China Sea, a return to a more westward track and gradual intensification were forecast, with the subtropical ridge anticipated to maintain itself north of Irving's track throughout most of the period. A more northwestward track became probable based upon analyses of 500 and 700 mb heights at 110000Z that indicated height falls at both levels were occurring over China. Irving, sensing this developing weakness in the subtropical ridge, maintained



Figure 3-18-3. Typhoon Irving approaching mainland China. 1506437 September (NOAA 7 visual imagery)

a slow, northwestward movement until 1412002, when a slight acceleration began. Aircraft reconnaissance at 1206302 reported a maximum observed surface wind of 90 kt (46 m/sec), well above the 50 to 65 kt (26 to 33 m/sec) range previously forecast. Figure 3-18-2 shows Irving near peak intensity. The aircraft data also indicated that Irving had a very tight circulation, with the radius of 50 kt (26 m/sec) winds within 60 nm (111 km) of the center during this period of maximum intensity. Radar observations, as well as synoptic reports from the Paracel Islands

(WMO 59981 and 59985) were very useful in accurately determining Irving's position and intensity during the period 12-13 September when reconnaissance aircraft fix missions could no longer be flown.

On 15 September, as the system began to interact with Hai-nan Island and the coast of China, Irving was downgraded to tropical storm strength (Figure 3-18-3). Irving made landfall 110 nm (204 km) northeast of Hanoi at 151800Z, and thereafter rapidly dissipated over the mountainous area of Vietnam.

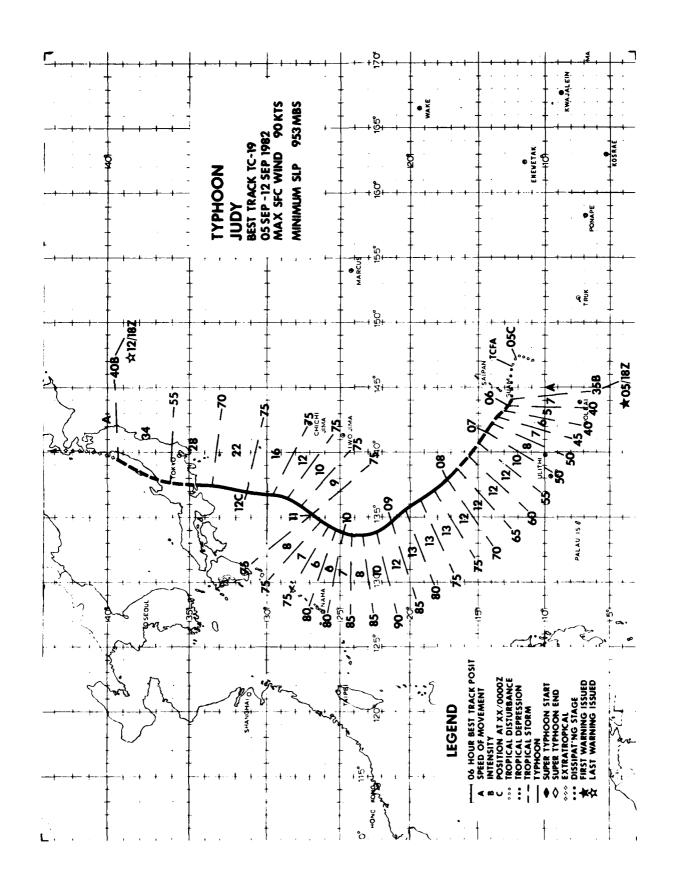




Figure 3-19-1. 0505202 September (NOAA 7 visual imagery).

Typhoon Judy, along with Typhoon Irving (18) developed within a very active monsoon trough that dominated the low-latitudes of the western North Pacific during the first week of September. At 041200Z, synoptic data indicated low-level winds were beginning to organize around the disturbances which later became Judy and Irving. This apparent organization prompted the reissuance of the Significant Tropical Weather Advisory (ABEH PGTW) at 041600Z which discussed each of these systems for the first time. The relatively continuous maximum cloud zone that spawned these two typhoons is shown in Figure 3-19-1, at about the time that a Tropical Cyclone Formation Alert was issued for Judy and the initial warning was issued for Tropical Depression 18 (Irving).

During the ensuing 24-hour period, Judy rapidly organized while Irving slowly intensified. It was during this period that satellite imagery showed the maximum cloud zone segmenting around the



Figure 3-19-3. 0906132 September (NOAA 1 visual imagery).

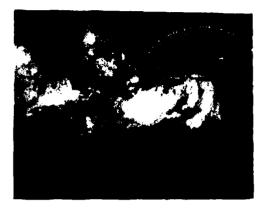


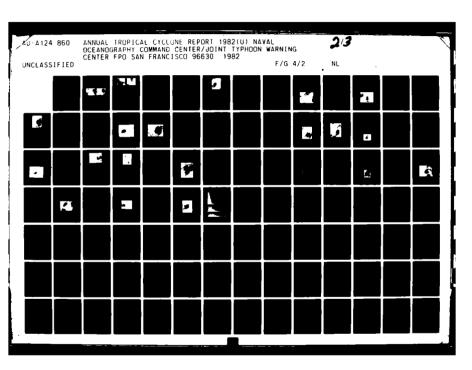
Figure 3-19-2. 0605087 September (NOAA 7 visual imagery).

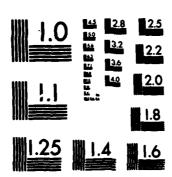
two systems (Figure 3-19-2). The first warning for Tropical Depression 19 was issued at 051600Z when satellite imagery indicated a progressive development of cloud features around the system. The first reconnaissance aircraft mission for Judy was conducted at 052239Z and reported 45 kt (23 m/sec) surface winds and a 994 mb minimum sea level pressure. Based on these data, Tropical Depression 19 was upgraded to Tropical Storm Judy on the 060000Z warning.

Initial forecasts for Judy anticipated a movement toward the west-northwest as the numerical forecast series built the subtropical ridge from 150E toward 130E along 25N. However, the subtropical ridge did not build from east to west but built northward along 150E instead. This change in ridge orientation, along with the eastward progression of a short wave trough over Asia, permitted Judy to track northwestward toward eventual recurvature east of Okinawa.



Figure 3-19-4. 0918582 September (NOAA 7 infrared imagery).





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From 6 to 9 September, Judy developed at a fairly steady rate (15 to 20 kt (8 to 10 m/sec) per day) and reached a peak intensity of 90 kt (46 m/sec) on 9 September. This period of intensification was aided by a tropical upper-tropospheric trough (TUTT) that was located to the north and northwest of Judy through most of this period.

On 8 and 9 September, 200 mb data and satellite imageries suggested that Judy's upper-level circulation was moving into a region previously occupied by the TUTT. As depicted in Figure 3-19-3, the TUTT axis was contorted northward around the periphery of the advancing Judy. By 0918582 (Figure 3-19-4), satellite imagery revealed that the west quadrant was virtually devoid of deep-layer convection and Judy's center had expanded to more than 90 nm (167 km) in diameter. During this period, Judy exhibited a reversal in sea level pressure tendency and subsequent



Figure 3-19-5. 100601Z September (NOAA 7 visual imagery)

On 10 September, Judy was moving slowly (6 to 7 kt (11 to 13 km/hr)) toward the north-northeast; satellite imagery (Figure 3-19-5) shows the cloud signature returning to a more circular appearance. Presumably, the interaction with the TUTT had ceased and the mid- and upper-levels were returning to a more typical environment for a mature typhoon.

Judy accelerated toward Japan on the 11th; this movement had been expected as early as 9 September (near 24N) but was delayed until the influence of low-level reintensification was not observed. Based on the interpretation of available data, it appears that at the mid- and upper-tropospheric levels, Judy may have ingested the remnants of the TUTT; and this entrainment of cooler air at these levels may have accounted for the changes in Judy's intensity trend and the resultant satellite signature that were observed on 9 September.

Prior to 0818003, JTMC forecast tracks predicted that Judy would progress slowly toward the north in the 48- to 72-hour period with a close approach to Okinawa expected. However, with the issuance of warning number 13 at 0818002, a significant change toward the north and recurvature toward eastern Honshu was forecast. This change in the forecast was prompted by the 081200Z 500 mb and 200 mb analyses data which showed a deeper penetration of a mid-latitude trough, south of Korea, than was previously anticipated.

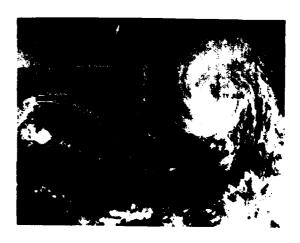


Figure 3-19-6. 1105492 September (NOAA 7 visual imagery)

steering became favorable for a sustained northward movement. A low-level anti-cyclone, centered near 45N 120E, had been exerting a relatively strong north to northeast flow over the Sea of Japan southward to 27N. On 11 September, this anticyclone began to weaken and its influence on the region north of Judy abated. In response, Judy accelerated from 8 kt (15 km/hr) at 1100002 to well over 25 kt (46 km/hr) before it struck Japan 38 hours later. Figure 3-19-6 shows Judy as this acceleration began.

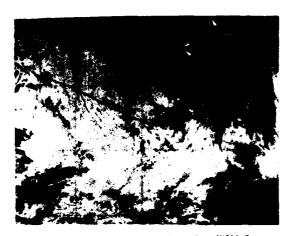


Figure 3-19-7. 111834Z September (NOAA 7 infrared imagery)

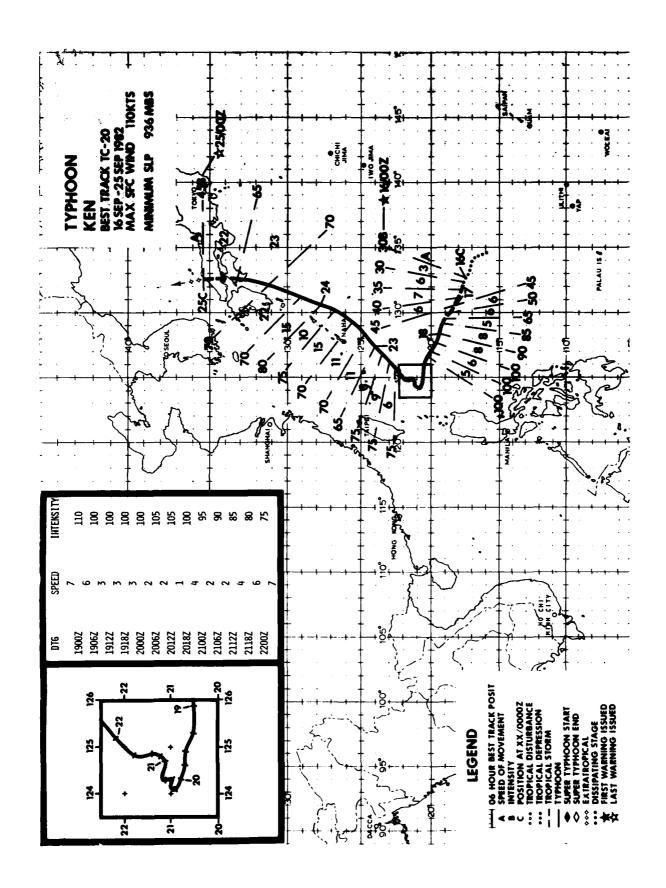
As Judy approached 30N, strong upperlevel winds from the south-southwest began exerting considerable pressure on Judy. As seen in Figure 3-19-7, convective activity was eroding on the southwestern periphery of Judy's center. This process preceded and accompanied Judy through its extratropical transition (Figure 3-19-8).

At 120800z, Judy made landfall upon Omaezaki Point in Shizuoka Prefecture,



Figure 3-19-8. 1218102 September (NOAA 7 infrared imagery).

southeast of Nagoya. Judy moved rapidly over the mountainous region of central Honshu and entered the eastern portion of the Sea of Japan where extratropical transition followed. In its wake, Judy left at least 25 dead and the accompanying torrential rains and floods damaged more than 61,000 houses, washed out sections of 956 highways and swept away 46 bridges in an area stretching from Osaka in the south, to Hokkaido in the north.



Typhoon Ken formed in mid-September in the western portion of an elongated monsoon trough in the Philippine Sea. Satellite imagery on 14 and 15 September showed a persistent convective disturbance near 17N 134E with evidence of upper— and lower-level circulation centers. A reconnaissance aircraft mission early on 16 September closed off a surface circulation near 18N 133E, with 10 to 35 kt (5 to 18 m/sec) winds and a minimum sea level pressure of 1003 mb. Based on this information, JTWC elected to forgo the issuance of a Tropical Cyclone Formation Alert and, at 1603002, the initial warning was issued on Ken as Tropical Depression 20.

Ken was upgraded to tropical storm status on the 1612002 warning after aircraft reconnaissance reported a 999 mb central pressure and sustained winds of 35 kt (18 m/sec). Initial warnings for Ken anticipated movement toward the west, passing near the northern tip of Luzon within 72 hours. The forecasts were based on the apparent strength of the mid-level steering flow along the southern periphery of the subtropical ridge which was centered between Taiwan and Okinawa. Thirty-three hours after the initial warning was issued, Ken was upgraded to typhoon status when aircraft reconnaissance data showed a when alreraft reconnaissance data showed a central pressure of 976 mb, equivalent to an intensity of 65 kt (33 m/sec) (Atkinson and Holliday, 1977). Ken underwent a rapid intensification during the following 24 to 36 hours, with its intensity surpassing 100 kt (51 m/sec) on 18 September. Up to this point in its development Ken was characterized a compact system; for example, aircraft data at 180600Z indicated a 938 mb central pressure in a 10 nm (19 km) diameter eye with a maximum surface wind of 100 kt (51 m/sec) located within a band of maximum winds only 15 nm (28 km) from the center.

Ken moved much slower than anticipated, and toward the west-northwest, for the first four days in warning status. During this period, a gradual but significant change in the subtropical ridge was taking place; by 19 September the ridge had retrograded south-westward and strengthened over southern China and the northern portion of the South China Sea. JTWC forecasts during this period expected this slow movement to be short-lived based on a forecast strengthening of the ridge north of Ken and a corresponding weakening of the ridge over the South China Sea which would allow Ken to resume its movement westward. This forecast scenario never materialized and, aided by analysis and prognostic fields from the 1912002 data base which provided indications that westward movement was not likely to occur, JTWC forecast tracks turned toward the north commencing with the 2000002 warning. Some of the indicators which prompted JTWC to change the forecast track were: the numerical forecast fields were starting to show a persistent break in the ridge north of Ken vice a strengthening of the ridge; the dynamic tropical cyclone models (OTCM, NTCM) began to consistently forecast a northward movement; and analysis data began to show significant height falls at the 700 mb level were starting to occur north of the ridge over southern Japan.

Despite all the signs predicting a northward movement, Ken eventually became quasi-stationary on 20 September (Figure 3-20-1 shows Ken at its westernmost position) and the character of the associated circulation pattern began to change dramatically; aircraft reconnaissance missions found the center expanding, with the strongest wind bands moving away from the center. The diameter and character of the eye (when observed) was also changing from mission to mission. A possible explanation of what



Figure 3-20-1. Typhoon Ken, at its westernmost position and just beginning a period of very little movement. Note the strong banding toward Ken's center. Within the next two days, much of this center would erode, leaving a nearly cloud-free area 60 nm [111 km] in diameter. 2005427 September (NOAA 7 visual imagery provided by Det 4, 10W Clark AB RP).

caused Ken to undergo such drastic changes could be the interaction with mid-latitude westerlies advecting much cooler air into Ken's center, thus accounting for formation of the large cloud-free center. The 2012002 500 mb analysis (Figure 3-20-2) shows the winds from the west moving into Ken's circulation about the time that these changes began. However, this does not explain why Ken's eye dissipated and then reformed within the otherwise cloud-free center, unless the westerlies were diverted from the center for short periods of time, allowing warm, moist air to reenter the center and assist in the reformation of the eye.

Ken's eye was last observed at 212011Z during a double-fix aircraft mission. On the first penetration, the mission Aerial Reconnaissance Weather Officer (ARWO) indicated the eye was 7 nm (13 km) in diameter but on the second penetration, at 212327Z, the ARWO reported "... the eye was so large we couldn't even pick it up on our radar ..."1. Further, the band of maximum winds were observed some 60 to 95 nm (111 to 176 km) from Ken's center.

On 21 September, satellite imagery and upper air analysis data indicated the trough north of the subtropical ridge had begun to

Candis L. Weatherford, Capt, USAF, mission ARWO.

deepen. In response, Ken began to move erratically toward the northeast and by 2118002 was on a steady course toward Okinawa. The possibility of significant acceleration was examined as continued interaction with the mid-latitude westerlies seemed likely. A recently developed JTWC forecast aid, TAPT (Weir, 1982), indicated Ken might undergo acceleration near 25N. Indeed, as Ken approached 26N, its forward speed began to increase and acceleration continued until landfall on the island of Shikoku, Japan. During this acceleration period Ken passed 78 nm (143 km) southeast of Okinawa; maximum winds recorded at Kadena AB were 35 kt (18 m/sec) at 2309552 and a peak gust of 58 kt (30 m/sec) at 2311352. Ken also brought a significant, and much needed, rainfall to Okinawa; 11.09 inches (28.2 cm) were recorded at Kadena on 23 September.

Once past Okinawa, Ken began to gradually weaken under strong mid- and upper-level

westerlies. Aircraft reconnaissance missions continued to find the belt of maximum surface winds moving farther away from the center with every fix. Satellite imagery showed a steady decline in convection as Ken continued to move toward Japan. Ken made landfall upon Shikoku at 2417002, crossed the inland sea, and then moved through western Honshu into the Sea of Japan where it became extratropical at 2500002.

Ken was the fourth typhoon of the season to hit the main islands of Japan; it brought torrential rains and high winds, which triggered mudslides that flooded or wrecked thousands of homes and paralyzed both air and ground transportation. Reports from the region indicated that a peak gust of 114 kt (59 m/sec) was recorded on Shikoku during Ken's passage along with 8.7 inches (22.1 cm) of rain over one six-hour period.

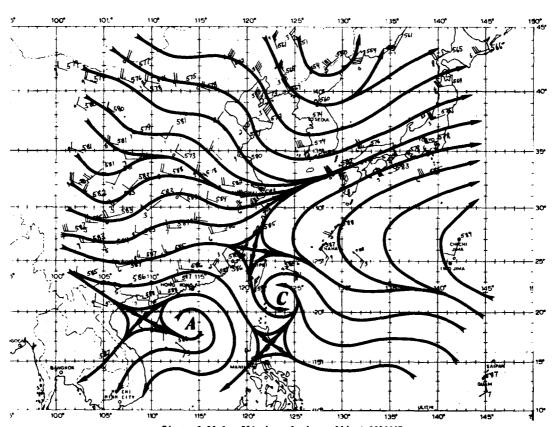
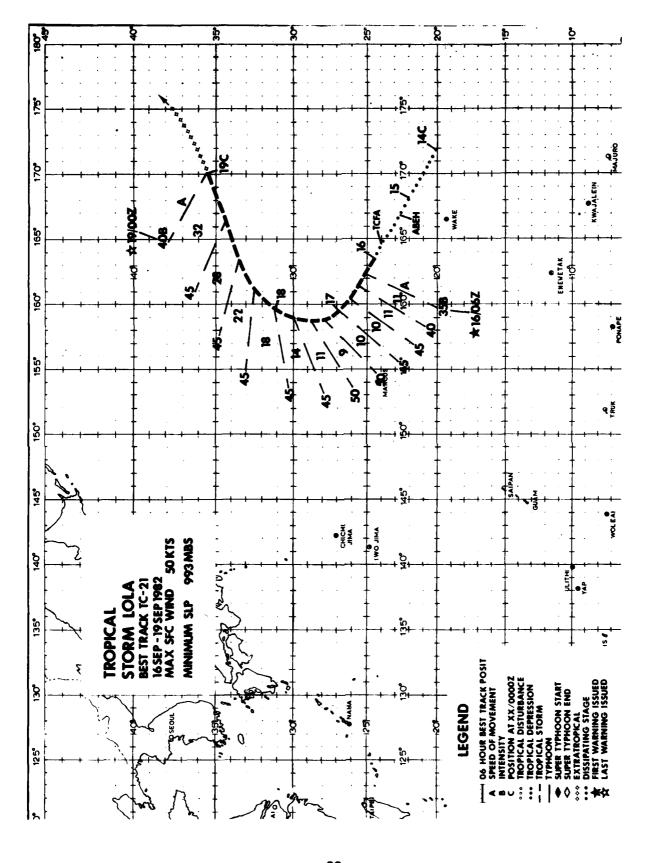


Figure 3-20-2. 500 mb analysis, valid at 2012002. The strength of the subtropical ridge over China had diminished during the previous 12-hour period. This process allowed mid-latitude westerlies to move further southward and become involved with Ken's circulation pattern. The break in the east-west extension of the ridge, north of Ken, can also be seen. Wind speeds are in knots.



## TROPICAL STORM LOLA (21)

Tropical Storm Lola was the third tropical cyclone of the season to form in the subtropical latitudes of the western North Pacific Ocean. Typical of tropical cyclones that form north of 20N in the mid- and late summer, Lola's formation was aided by its proximity to a tropical upper tropospheric trough (TUTT) cell (Sadler, 1976) and remained a small, compact tropical cyclone during its lifetime. Due to Lola's remote location, no successful reconnaissance aircraft missions were flown and all fix positions and intensity estimates were based on analyses from satellite imagery.

Lola was first detected on satellite imagery as a weakly organized band of convection near the dateline on 13 September. By 140000Z, this convection had moved westward to within 600 nm (1111 km) of a well-defined TUTT cell that was located in the vicinity of Wake Island (WMO 91245). During the ensuing 24 hours, the upper-tropospheric divergence fields appeared to increase in the area and a small anticyclone was soon detected on satellite imagery over the disturbance. During the same period, a low-level shear line from a cold front moved to within 200 nm (370 km), north of the convective disturbance. This shear line appeared to aid the development of the low-level

circulation center, as cumulus lines could be detected spiraling into the system's center from the north as early as 150000Z.

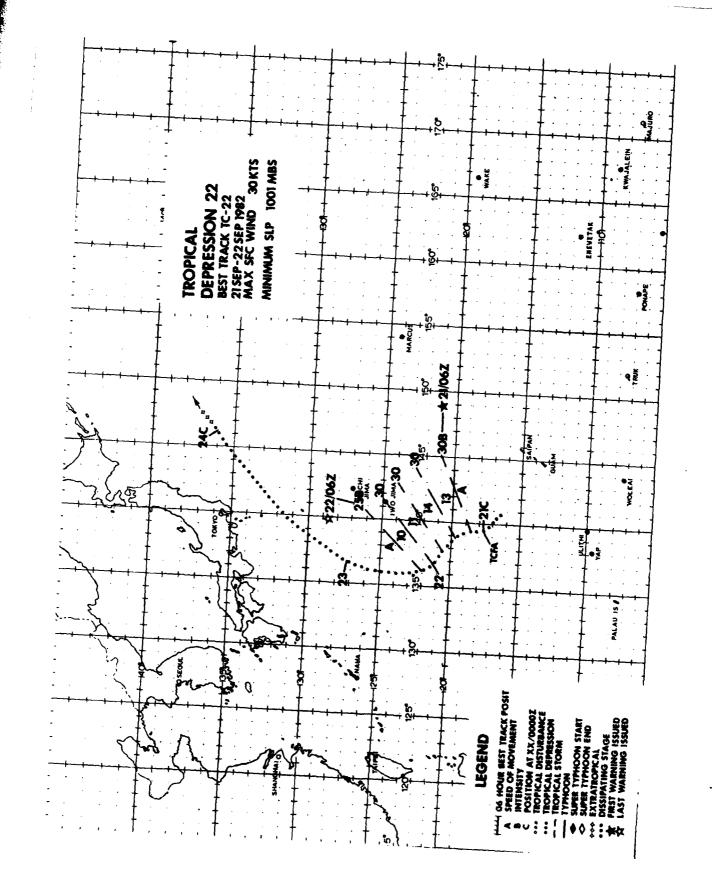
Convection remained weak and variable over the next 18 hours; however, at 151829Z a Tropical Cyclone Formation Alert was issued when upper-level outflow increased around the system. During the next 12 hours, convective organization increased and at 160600Z, the first warning was issued for Tropical Storm Lola when the intensity estimate from analysis of visual satellite imagery indicated the likelihood of 35 kt (18 m/sec) surface winds near Lola's center.

Lola's eventual recurvature around a mid-tropospheric anticyclone was well forecast due, in part, to good agreement from the very first forecast with the CYCLOPS steering aids and the One-Way Interactive Tropical Cyclone Model (OTCM).

As Lola approached 30N on 17 September, acceleration toward the northeast began in advance of a newly formed cold front which was moving toward Lola from the northwest. Extratropical transition was completed by 190000Z when Lola became totally entrained into the frontal system.



Figure 3-21-1. Tropical Storm Lola at the point of recurvature as a cold front approaches from the northwest. 1704362 September (NOAA 7 visual imagery).



## TROPICAL DEPRESSION (22)

Tropical Depression 22 began its brief existence as a significant tropical cyclone in the wake of Typhoon Ken (20). An exposed low-level circulation, with convection displaced well west-southwest of the circulation center, was a persistent feature of this system throughout its lifetime as it was apparently dominated by Typhoon Ken's upper-level outflow.

The first aircraft investigative mission flown on 20 September closed a surface circulation with 15 kt (8 m/sec) winds and a central sea level pressure of 1002 mb. The mission Aerial Reconnaissance Weather Officer reported no mid- or upper-level cloud features associated with the low-level center. A second investigative flight on 21 September reported winds had increased to 20 kt (10 m/sec) near the circulation center, while winds of 30 kt (15 m/sec) were evident 70 nm (130 km) south of the center. Convection was displaced 90 nm (167 km) west-southwest of the low-level center but was increasing in intensity. This information prompted the issuance of a Tropical Cyclone Formation Alert (TCFA) at 210123Z.

Subsequent synoptic data carried a growing number of reports of 30 kt (15 m/sec) winds in the alert area, plus visual satellite imagery at 210300Z depicted a strengthening of the low-level circulation. Based on these factors, the first warning was issued

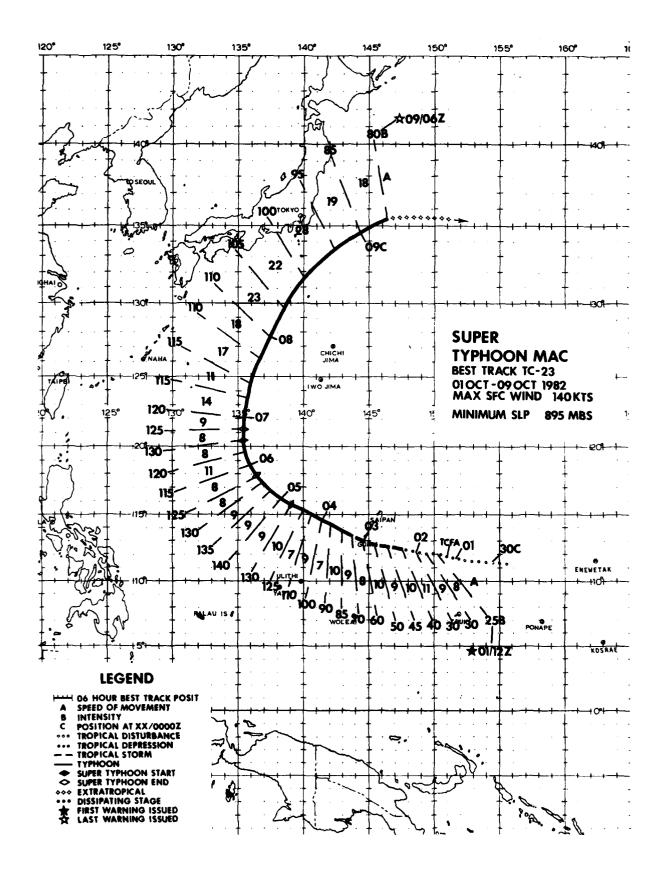
on Tropical Depression 22 at 2106002 calling for movement toward the northwest. At this time Typhoon Ken was 900 nm (1667 km) to the west-northwest but minimal interaction was expected. However, Ken's outflow pattern was expected to inhibit rapid development of Tropical Depression 22. Therefore intensification to only 55 kt (28 m/sec) was forecast by the end of 72 hours. (See Figure 3-22-1).

During the ensuing 24-hour period aircraft and satellite data showed no indication of vertical development. Synoptic data at 2200002 indicated that surface winds had weakened to 20 kt (10 m/sec) and surface pressures had not changed from the previous 1002 mb level. Because Tropical Depression 22 was continuing to move more rapidly toward the north-northeast, little opportunity for further development was expected. Additionally, satellite imagery continued to show a weakening of the low-level circulation, thus warnings were suspended at 2207002.

After dissipating as a significant tropical cyclone, a weak convective disturbance persisted and began accelerating northeastward. This disturbance did maintain enough integrity to induce the development of a small extratropical system upon merging with a frontal zone southeast of Japan on 24 September.



Figure 3-22-1. Tropical Depression 22 at 30 kt 115 m/sec) intensity as an exposed low-level circulation. Convection is displaced to the west-southwest. Typhoon Ken can be seen 900 nm (1667 km) to the northwest. 2105292 September (NOAA 7 visual imagery).



Super Typhoon Mac was reawned to the east of Ponape (WMO 91348) n an area which had been under close scr liny by the Joint Typhoon Warning Center for several days. A persistent surface circulation, with an associated upper-level anticyclone, was closely monitored beginning on 28 September. No signs of significant development were evident until satellite imagery on 1 October revealed that the convective pattern was more conducive to intensification and the upper-level outflow signature was supportive of sustained further growth of the disturbance. Based upon this evidence, a Tropical Cyclone Formation Alert was issued at 010635z. Further intensification was rapid; the first warning on Tropical Depression 23 was issued at 011200z after nearby shipboard observations indicated that the surface pressure was as low as 1003 mb and that surface winds had risen to 25 kt (13 m/sec).

Because of Tropical Depression 23's location (near 12N 150E), it became apparent that the system presented a significant threat to the island of Guam. During its formative stages, Mac had moved somewhat erratically but had tracked generally west-northwestward under the influence of steering currents associated with the southern periphery of the subtropical ridge. Initially, numerical forecast fields indicated there would be no change in this steering flow over the next three days and Mac was predicted to continue on a west-northwest course. During this period, rapid intensification was expected due to favorable upper- and lower-level conditions: the relatively small upper-level anticyclone over the system was in close proximity to strong upper-level outflow channels; and at the surface, there was a massive area of inflow from the west with virtually no competition from other circulation centers in the area (Figure 3-23-1).

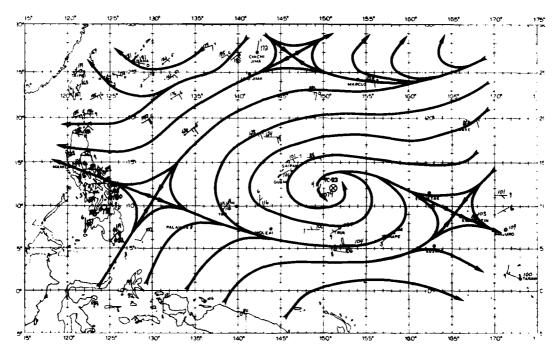


Figure 3-23-1. 0112007 October surface analysis. Wind speeds are in knots.

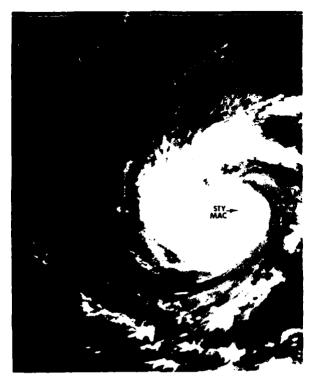


Figure 3-23-2. Super Typhoon Mac is shown 11 hours after maximum intensity, 050640Z October (NOAA 7 visual imagery).

Initial forecasts proved accurate as Mac passed 10 nm (19 km) southwest of Guam at 030000Z. Although maximum sustained winds within Mac were estimated to be 60 kt (31 m/sec) at closest point of approach to Guam, the highest sustained winds recorded at Nimitz Hill (24 nm (44 km) from Mac's center) were just 30 kt (15 m/sec). Guam experienced little structural or equipment damage because of the fortunate combination of adequate advance warning and preparation, and the compact wind radii associated with Mac. However, crop damage was extensive in the southern part of the island due to the heavy rains and relatively high winds experienced there; the Government of Guam Department of Agriculture estimated damages at 1.5 million dollars.

Mac continued to intensify rapidly after passing Guam. In two days, from the 3rd to the 5th, Mac more than doubled its intensity from 60 kt (31 m/sec) to 140 kt (72 m/sec) (Figure 3-23-2). Figure 3-23-3 shows the trends of various meteorological parameters over Mac's lifetime. The 700 mb data and minimum sea level pressure (MSLP) were derived from reconnaissance aircraft data. Items of particular note include: the dewpoint depression of 28°C, one of the largest ever recorded in a tropical cyclone; the redevelopment to super typhoon strength, only the sixth recorded instance since 1958; the correspondence of the MSLP trends and intensity peaks; and the relatively smooth intensity trend as presented by Dvorak analyses.

During its period of rapid intensification, Mac began to assume a more northwestward track in response to a developing weakness in the subtropical ridge near the Ryukyu Islands. On 5 and 6 October, after having attained super typhoon strength, Mac turned sharply north-northeastward and accelerated. Beginning with forecasts issued on 4 October, which keyed on the break in the subtropical ridge, JTWC anticipated this movement quite well. Because of a deep westerly flow which extended well to the south of the main islands of Japan, Mac never posed a threat to Japan even though it

appeared to be right on course toward Tokyo until 8 October.

Once embedded in the mid-latitude westerly flow, Mac accelerated to a maximum forward speed of 28 kt (52 km/hr) but lost little of its intensity. Two days after its recurvature, Mac's intensity had dropped only 30 kt (15 m/sec), i.e. from 125 to 95 kt (64 to 49 m/sec); although Mac remained intense, it rapidly lost its tropical characteristics and transitioned into an extratropical system on 9 October.

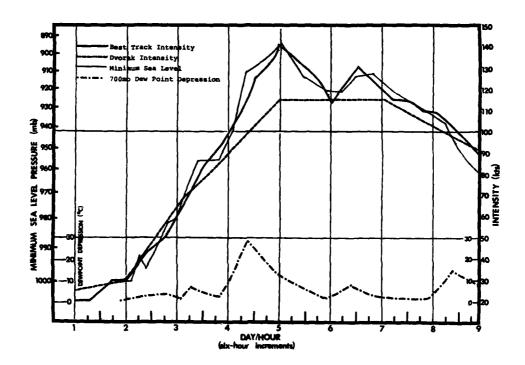
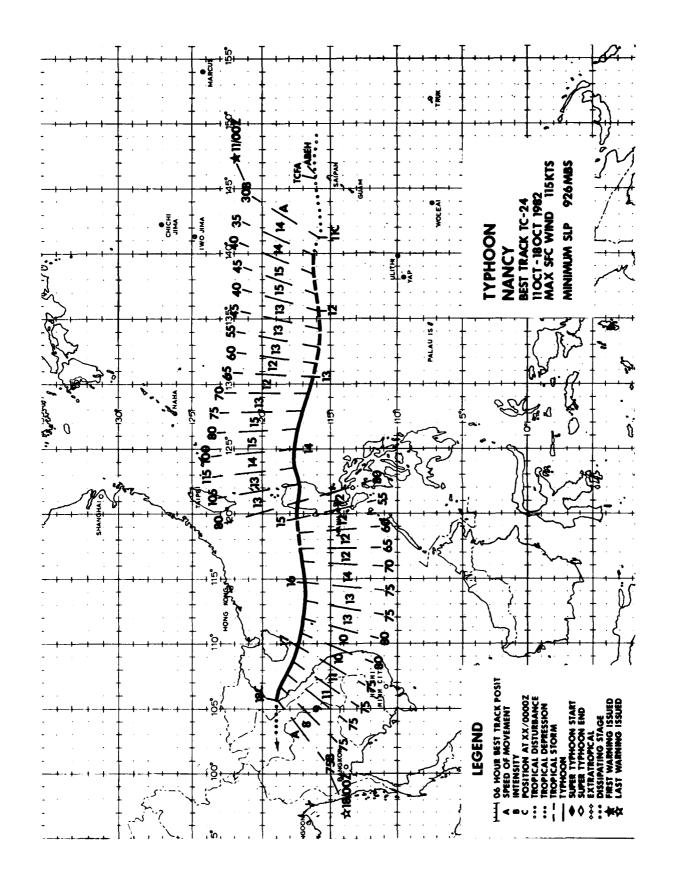


Figure 3-23-3. Comparisons of best track intensities, Dvorak intensity estimates, minimum sea level pressures, and 700 mb deupoint depressions for the first eight days of Mac's existence.



## TYPHOON NANCY (24)

A large area of weakly organized convection consolidated into a single mass on 8 October near 17N 158E in a region made favorable for cyclogenesis by the divergence aloft near an upper cold low. This convection was strong enough to become separate from the surrounding cloudiness lying south of an upper cold low embedded within a tropical upper-tropospheric trough (TUTT). Sustained surface pressure falls, however, weren't realized as this convective area degenerated later that day into a random pattern of cloudiness. The upper cold low continued to drift westward and was located

near 148E on 10 October. This time the conditions were right for cyclogenesis — the upper-level divergence coupled with a pre-existing low-level cyclonic circulation and a tropical depression formed in the enhanced cloudiness just south of the TUTT. This cloudiness was separate and distinct from the routinely observed maximum cloud zone, which lay to the south, between 7N and 10N.

A Tropical Cyclone Formation Alert was issued at 1007302 for the area 200 nm (370 km) north of Guam due to the 1005 mb surface pressures and the significant

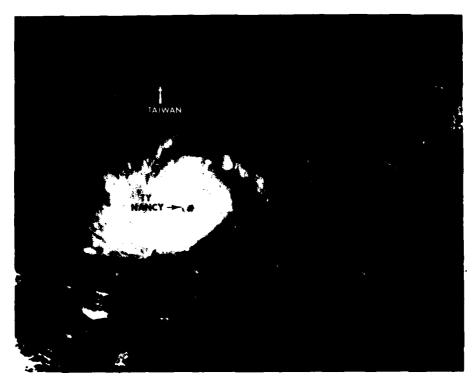


Figure 3-24-1. 1405567 October NOAA 7 visual imagery shows Typhoon Nancy at its peak intensity of 115 kt (59 m/sec) and approximately six hours away from landfall on northern Luzon. Note the island of Taiwan can be seen to the north of Nancy's cloud shields.

increase of cloud pattern organization. Again, because of the sparse conventional data, satellite images had been the key indicator of cyclogenesis and aircraft reconnaissance could not be scheduled to investigate the area until the following day.

The initial reconnaissance aircraft located a closed circulation and surface winds of 25 kt (13 m/sec) which prompted the first warning at 110200Z. Upgrading from tropical depression to tropical storm status followed within six hours, when the follow-on aircraft fix found 35 kt (18 m/sec) winds and a minimum sea level pressure of 999 mb. Nancy stabilized at moderate tropical storm strength and maintained a westward track for the next 24 hours.

Much of Nancy's early warning period was marked by several changes in the basic forecast track. The first four warnings anticipated that

Nancy would track northward toward recurvature; however, due in part to the strengthening of the low-level easterly winds north of Nancy, this forecast movement did not occur and Nancy moved rapidly westward with the low-level steering flow. The next four warnings anticipated a west-northwestward movement and through the Bashi Channel, north of Luzon. This track was ahandoned at 130000Z when analysis and numerical prognostic data showed evidence that a mid-latitude trough would deepen south of Korea and lessen the influence of the low-level steering on Nancy. Thus until 140600Z (warning 14), the JTWC forecasts showed a pronounced northwestward track toward Taiwan and mainland China. On 14 October, as it became evident that the forecast weakening of the low-level steering current would not materialize, the JTWC forecasts

During this period of changing forecast scenarios, Nancy began to intensify. On  $13\,$ 

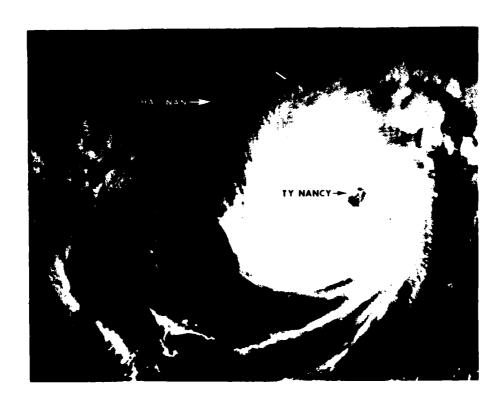
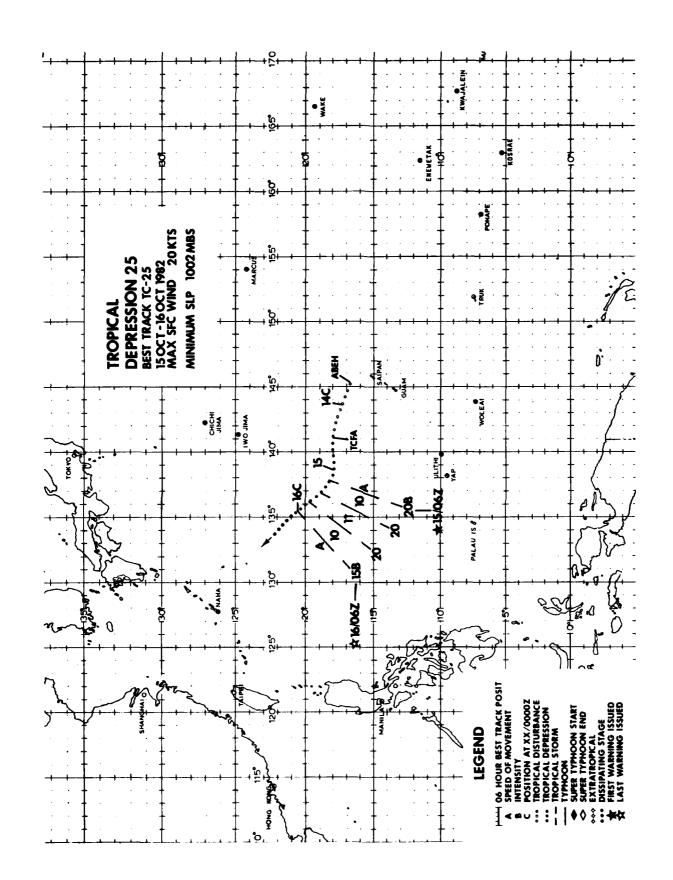


Figure 3-24-2. Typhoon Nancy was located near 17.0N 113.8E or 210 nm (389 km) east-southeast of the island of Hai-Nan at 1607142 October. Hai-Nan island was located on the northwestern edge of Nancy's cirrus cloud cover. Note the fair weather as indicated by the small, fair weather cumulus over the island and coastal areas of Vietnam, in sharp contrast to the approaching typhoon. (NOAA 7 visual imagery).

October, Nancy attained typhoon strength and then rapidly deepened to a peak intensity of 115 kt (59 m/sec) just six hours prior to landfall on northeastern Luzon. Nancy was reduced to tropical storm strength by a rugged overland transit, but was quick to regain typhoon strength upon reaching the open waters of the South China Sea. Nancy was the most intense typhoon to strike the Republic of the Philippines this year; in its wake, Nancy left at least 110 dead, 12,000 people homeless, and caused an estimated 46 million dollars damage.

The presence of a continuing strong midand upper-level circulation pattern made Nancy's reintensification in the South China Sea possible. At 1612002, Nancy reached a second peak intensity of 80 kt (41 m/sec) as it passed just north of the Paracel Islands (WMO 59981). The influence of a subtropical ridge over southern China and the continuing presence of of the low-level northeasterly (monsoon) flow across the South China Sea kept Nancy on a westward track until it approached Hai-Nan Island late on 16 October. From near Hai-Nan until landfall, Nancy maintained a slower, northwestward track along the southern periphery of the subtropical ridge.

On 18 October, Nancy crossed the coast of Vietnam 15 nm (38 km) north of the city of Vinh (18.7N 105.7E) in the Nghe Tinh province, causing at least 71 deaths, leaving 194,200 people homeless, and devasting 185 square miles (48,000 hectares) of winter rice crops that were ready for harvest. Later satellite imagery (at 1806002) indicated that Nancy's central convection had dissipated over the mountains of Vietnam.



#### TROPICAL DEPRESSION 25

On 14 October, surface observations indicated a weak circulation center near 18N 141E. Satellite analysis of the area revealed the presence of an upper-level anticyclone with potential to enhance the ventilation of the surface system. Expecting further development once the system attained vertical alignment, JTWC issued a Tropical Cyclone Formation Alert (TCPA) at 1412002.

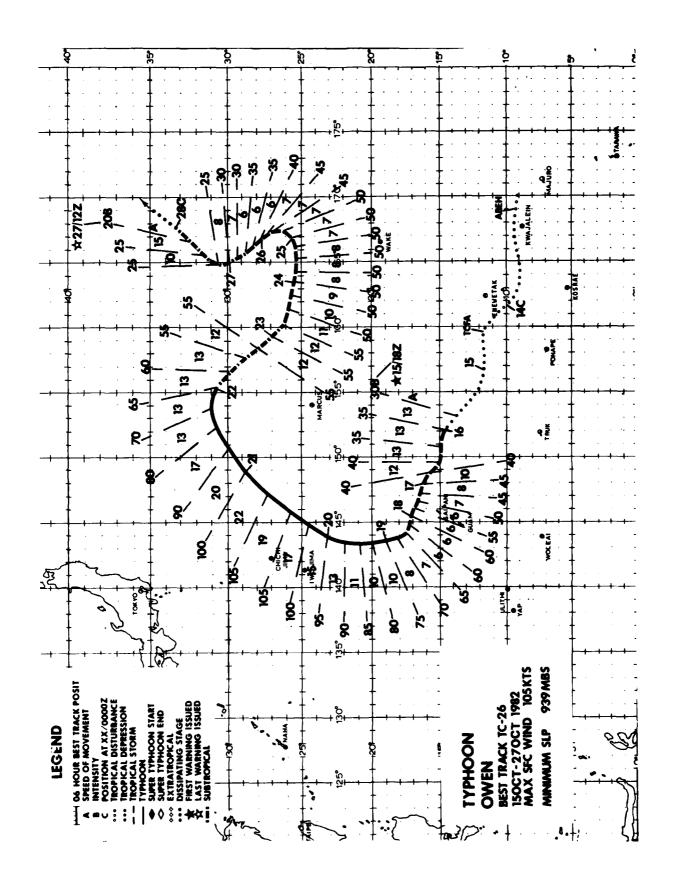
Aircraft reconnaissance at 142336Z located a weak surface circulation near 18N 139E, with central pressures estimated to be near 1006 mb. The initial warning on Tropical Depression 25 was issued after 150000Z satellite imagery showed the convective area near the center was becoming more organized.

Subsequent aircraft reconnaissance of the system at 150900Z reported maximum winds less than 10 kt (5 m/sec), and the circulation center could not be fixed by either winds or pressures. Satellite imagery indicated that the convection associated with the system had greatly weakened, and the overall organization had decreased. The subsequent warning, at 151200Z, anticipated further

weakening of Tropical Depression 25 and the forecast period was shortened to 24 hours. On the following day, visual satellite imagery at 160000Z, with corroborative synoptic data, indicated that Tropical Depression 25 had become a fully exposed low-level circulation with no associated major convection. Thus, the final warning on Tropical Depression 25 was issued at 160600Z.

For the next 48 hours, this exposed low-level circulation remained evident on visual satellite imagery, as it progressed to the northwest. Re-development of some convective banding, curving into the system was observed on 18 October. The development of a weak anticyclonic pattern aloft prompted the issuance of a TCFA for the area, near 21N 134E, at 180800Z. A low-level aircraft investigative mission was conducted at 190200Z, but was unable to locate a closed circulation center.

Early on 19 October, when the remains of Tropical Depression 25 were entrained into the expanding low-level inflow pattern associated with Typhoon Owen (26), the TCFA was cancelled.



Typhoon Owen culminated an active 14-week period (22 July through 27 October) during which 17 tropical cyclones reached warning status in the western North Pacific. During this period, only 10 calendar days did not have at least one tropical cyclone in warning status, with five days (26 to 30 September) the longest period without warnings. So obvious was the cessation of this period that four weeks elapsed between the final warning on Owen and the initial warning on the next tropical cyclone, Pamela (27).

Owen developed from a disturbance which was first detected on 13 October east of Kwajalein Atoll. On 14 October increased convective organization became evident on satellite imagery and, at 1412002, a Tropical Cyclone Formation Alert was issued. During the subsequent 36-hour period, the disturbance slowly organized, e.g. a reconnaissance aircraft investigative mission conducted on 14 October located a weak surface circulation approximately 100 nm (185 km) east of the convective center. However, by 1518002 the convective features were indicative of a

system of sufficient intensity to warrant transition to warning status, thus the initial warning was issued for Tropical Depression 26.

During the first 24 hours in warning status, positioning from aircraft and satellite data became more consistent, e.g. the 1523172 aircraft fix was located approximately 90 nm (167 km) east of the 1600002 satellite fix; by 1621002 the difference was less than 20 nm (37 km). As Figure 3-26-1 depicts, a strong upper-level tilt to the south was evident, but low-level cumulus cloud lines, detected north of the main convective mass, provided evidence of Owen's continued organization. Owen is another example of non-vertical alignment of developing tropical cyclones (Huntley and Diercks, 1981). Such systems normally become better aligned as they mature and Owen was no exception; on 18 and 19 October, the tilt became less evident and Owen responded by attaining typhoon strength at 1812002 and developing a banding-type eye on 19 October.



Figure 3-26-1. Low-level cumulus cloud lines can be seen entering Owen's center while the main convective features are displaced equatorward of the low-level center. Strong upper-level northeasterly winds are providing a unidirectional outflow channel toward the southwest. 1705202 October (NOAA 1 visual imagery).

While Owen was aligning in the vertical, it also began to slow its forward movement appreciably, from 13 to 6 kt (24 to 11 km/hr). Track forecasts (describing a west-northwest movement) were adequate until the system reached 17.5N 144E at 1812002, when Owen turned sharply northward. Although most forecasts up to this point had anticipated an eventual northward movement, none fully anticipated the extent of Owen's turn on 18 October. This movement can be related to the development of a blocking high east of Japan. (Actually, the FNOC prognostic series more than adequately forecast this development, but an extension of the midtropospheric (500 mb) subtropical ridge north of Owen and westward to 135E was seen by forecasters as an inhibiting factor to more significant northward movement). The development of the block increased the south-to-north flow in the mid-levels, leading to an erosion of the subtropical ridge north of Owen and thus, allowed the typhoon to move northward.

From 19 to 21 October, Owen accelerated northward toward an anticipated extratropical transition, reaching a peak intensity of 105 kt (54 m/sec) (Figure 3-26-2). Speed of movement forecasts during this period were quite good and fully anticipated Owen's acceleration from 10 to 22 kt (19 to 41 km/hr). However, the track forecasts did not fair as well, primarily due to the conflicting options presented by the flow around the block. Figure 3-26-3 shows the configuration of the mid-tropospheric (500 mb) flow near the block on 20 October, as well as the various forecast tracks issued (from 190000Z to 210000Z) and Owen's eventual best track. As can be seen, forecasts 14 through 17 tended toward the east (south of the blocking high), forecasts 18 and 19 anticipated that Owen would move northward toward an occluded low near Kamchatka, and forecasts 20 through 22 seemed to split the difference. On 21 October, Owen's anticipated extratropical transition was well underway; its associated convective features



Figure 3-26-2. Typhoon Owen near maximum intensity, 710 nm (1315 km) south-southcast of Tokyo, Japan at 2004432 October (NOAA 7 visual imagery)

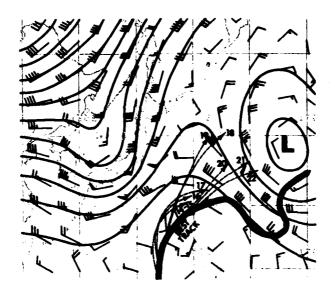


Figure 3-26-3. FNOC 500 mb analysis at 2000002 October with warnings 14 through 22 and Owen's best track superimposed. Wind speeds in knots.

were being sheared northward (away from the surface center), low-level inflow from the mid-latitudes dominated Owen's surface circulation pattern, and aircraft reports showed the band of maximum winds moving further from the center (135 nm (232 km) at 210704Z).

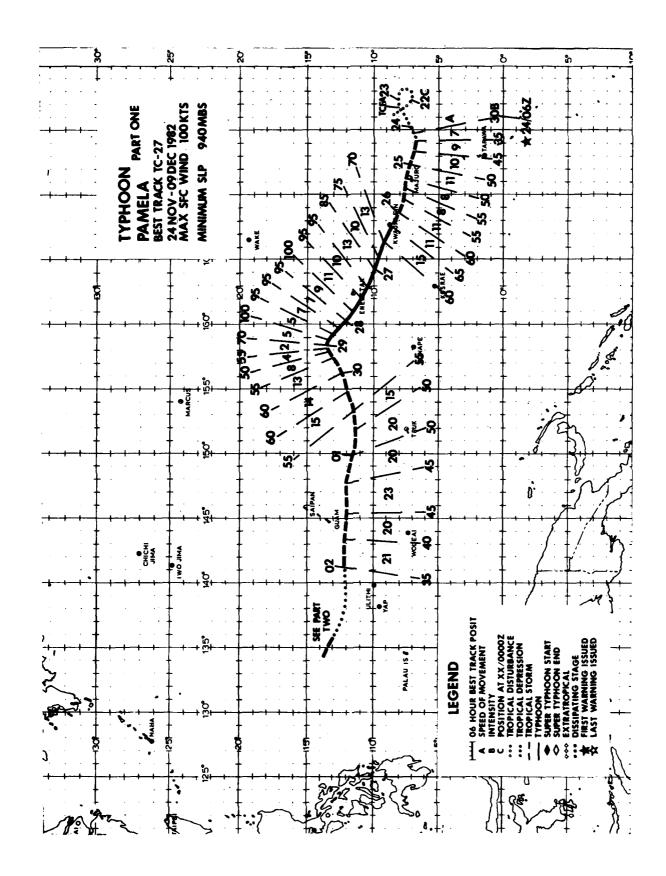
Numbered tropical cyclone warnings ended at 2200002 when satellite imagery indicated that Owen had transitioned to an extratropical low. During the next two days, extratropical gale warnings were issued by the NOCC Operations Department as the system tracked southeastward and south of the blocking high. On 23 October an increase in convective activity was noted equatorward of the system center (Figure 3-26-4) and during the next 24 hours it was closely monitored for possible reclassification as "tropical" vice "extratropical" or "subtropical" cyclone. The decision to redesignate Owen as a tropical cyclone occurred on

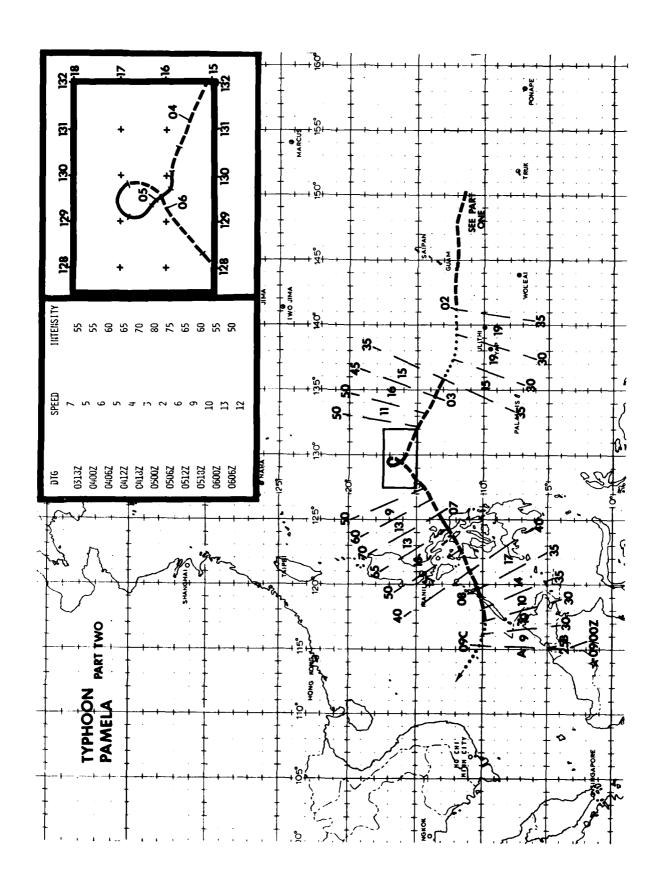
24 October when the convection began to reorganize around the system's center.

For the next 24 hours, Owen tracked eastward and maintained an estimated 50 kt (26 m/sec) intensity. Satellite fixes on 25 October began to indicate a pronounced northward track and a steady decrease in convective activity. From 25 to 27 October, the block, which had dominated the region for more than one week, began to break down and move eastward toward the International Dateline. As Owen moved northnorthwestward then northeastward, it slowly weakened and dissipated in the warm sector of an advancing frontal system. The final tropical cyclone warning was issued for Owen (as Tropical Depression 26) at 2712002 some 1400 nm (2593 km) north of its point of initial detection after completing a track in excess of 3600 nm (6668 km).



Figure 3-26-4. At 2403552 October, a significant increase in convection is evident near the system's center; at the time Owen was in warning status as an extratropical low (NOAA 7 visual imagery).





Typhoon Pamela, the 27th significant tropical cyclone of the season, formed east of the Marshall Islands on 24 November. Uncommon for a late season tropical cyclone, Pamela went on to become the longest running, in terms of time and distance, tropical cyclone of the year before dissipating in the South China Sea on 9 December. During its active warning period, Pamela was upgraded to typhoon status on four distinct occasions (reduced to three in post-analysis), a very rare phenomenon.

Development was first observed on 21 November with the formation of an upper-level anticyclone which had some convective activity along its northern outflow band. Visual satellite imagery on 22 November showed a low-level circulation was present near 6N 177E. During the next 48 hours, this disturbance lingered in the region east of 175E with convective activity fluctuating near the center; however, a slow increase in organization, conducive to further development, was observed.

The slow development of this disturbance is attributed to the proximity of Hurricane Iwa (04C) in the eastern North Pacific. As Iwa moved northeastward and passed the Hawaiian Islands, the disturbance (Pamela) began moving westward. A noticeable increase in convection was observed, leading to the

issuance of a Tropical Cyclone Formation Alert at 230600Z for an area east of Majuro Atoll. The system further organized, thus prompting the initial warning on Tropical Depression 27 at 2-0600Z. When the system developed a central convective feature, accompanied by a well-defined upper-level outflow pattern, it was upgraded to Tropical Storm Pamela at 241200Z.

The first several warnings called for movement toward the west-northwest with gradual intensification. These warnings were based on a forecast weakening of the subtropical ridge northwest of the system under the influence of a mid-latitude trough moving eastward from Japan. Indeed, Pamela moved west-northwestward through the Marshall Islands in the ensuing 84 hours. Satellite and aircraft reconnaissance data confirmed the gradual intensification of the system, with Pamela attaining typhoon status at 2606002 while passing approximately 60 nm (111 km) south-southeast of Kwajelein Atoll. By the time Pamela passed 35 nm (65 km) southwest of Enewetak Atoll at 2712002, its intensity was estimated (from aircraft data) to be 95 kt (49 m/sec) (Figure 3-27-1). Initial reports from the Marshall Islands indicated moderate to severe damage to buildings and crops from those islards affected by Pamela's passage, but there were no reports of loss of life.



Figure 3-27-1. Tupheon Pamela, 15 hours prior to reaching maximum intensity of 100 kts [5] m/sec), 2703482 November (NOAA 7 visual imagery).

Once past the Marshall Islands, Pamela's forward speed began to slow as the system started to come under the influence of a mid-latitude trough passing to the north. Pamela approached 19N it began to rapidly weaken as it encountered a mid- to upper-level shear zone associated with the trough. Evidence of the rapidity with which Pamela weakened is seen in the aircraft reconnais-sance data. At 282105Z, a central pressure of 950 mb and an observed 100 kt (51 m/sec) surface wind were reported. A second reconnaissance mission about nine and onehalf hours later (at 2906402) reported a 979 mb central pressure and observed surface winds of only 50 kt (26 m/sec). This second report necessitated the downgrading of Pamela tropical storm status on the subsequent warning. A much-weakened Pamela then moved toward the southwest and began to accelerate after breaking away from the effects of the trough and shear zone. This movement was in response to a strong northeast monsoonal flow which was present in the wake of the eastward-moving mid-latitude trough.

Commencing with the 291800Z warning, Pamela was forecast to reintensify and move westward along the southern periphery of the subtropical ridge, eventually passing near the island of Guam. The residents of Guam, remembering the devastation caused by Super Tyohoon Pamela (May, 1976), had been nervously watching "Pamela's" progress since its designation while still some 1800 nm (3335 km) east of Guam. Needless-to-say, island residents began to prepare for a possible repeat of the conditions associated with Pamela's 1976 namesake.

Pamela continued to accelerate toward the southwest until 301200Z when it began to move westward. During this period, Pamela continued to weaken; instead of gaining the expected mid- and upper-level support for reintensification, Pamela remained disorganized and the anticapted intensification did not materialize. The 011200Z December 500 mb analysis, for example, did not show any mid-tropospheric circulation center near Pamela's low-level vortex.

Although Pamela was still weakening, it was considered a potentially dangerous tropical cyclone. At 011200Z, Pamela was located 90 nm (169 km) southeast of Guam and was moving westward at 23 kt (42 km/nr); its closest point of approach (to Guam) came two hours later with the maximum recorded wind (gust) of 40 kt (21 m/sec), far below the 138 kt (71 m/sec) gust observed during Super Typhoon Pamela in 1976.

At 0115322, a reconnaissance aircraft was able to locate Pamela's 700 mb center 90 nm (169 km) southwest of Guam. Data from this fix indicated that Pamela's intensity had decreased to 49 kt (21 m/sec). The same aircraft was tasked to provide another fix of the 700 mb center at 011800Z but was unable to close off the circulation (the surface center was not observable due to darkness). The mission Aerial Reconnaissance Weather Officer (ARWO) felt that the 700 mb center had dissipated into a trough, providing further evidence that Pamela was continuing its weakening trend. A "resources permitting" "first-light" aircraft fix was requested for 0122002. The aircraft orbited south of the main convection until daybreak; then, responding to a satellite position provided to JTWC by Det 1, lWW, the aircraft was able to locate the surface center at 0121502 with an estimated 35 kt (19 m/sec) intensity.

During the next 24 hours, Pamela continued to move westward and weaken. Satellite imagery (Figure 3-27-2) and aircraft reconnaissance data revealed that Pamela had become a tropical depression by 0206002. During this period, JTWC was forecasting Pamela to dissipate as a significant tropical cyclone over water within 48 hours.

Pamela, again as Tropical Depression 27, started to slow its forward speed and began to move toward the northwest, responding to another mid-latitude trough moving off the coast of Asia. Once this northwest movement began, indications that Pamela might reintensify became evident. First, the 021200Z 500 mb analysis suggested that a midtropospheric circulation had reformed; and second, aircraft reconnaissance at 022126Z was once again able to close off a 700 mb center with data indicating that an intensity of .5 kt (18 m/sec) had been reached. Later reconnaissance aircraft missions showed that Pamela was continuing its reintensification and it passed from tropical storm status to typhoon status (again) at 041200Z. During this period of reintensification, Pamela During reached a maximum intensity of 80 kt (41 m/sec) while concurrently slowing to a minimum speed of 2 kt (4 km/hr) at 0500002 (Figure

JTWC objective forecast aids and FNOC prognostic fields began to indicate the potential for recurvature once Pamela approached the axis of the (mid-tropospheric) subtropical ridge, near 17N. The 0400002 warning was the first to reflect a recurvature scenario. The numerical prognostic

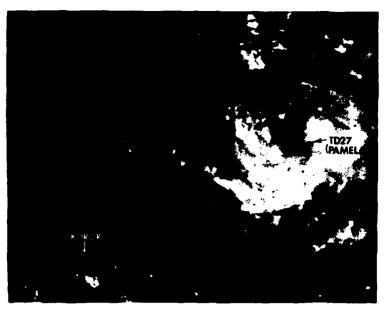


Figure 3-27-2. Pamela, now Tropical Depression 27, with estimated intensity of 30 kts (15 m/sec). 0:06112 December (NOAA 7 visual imagery).

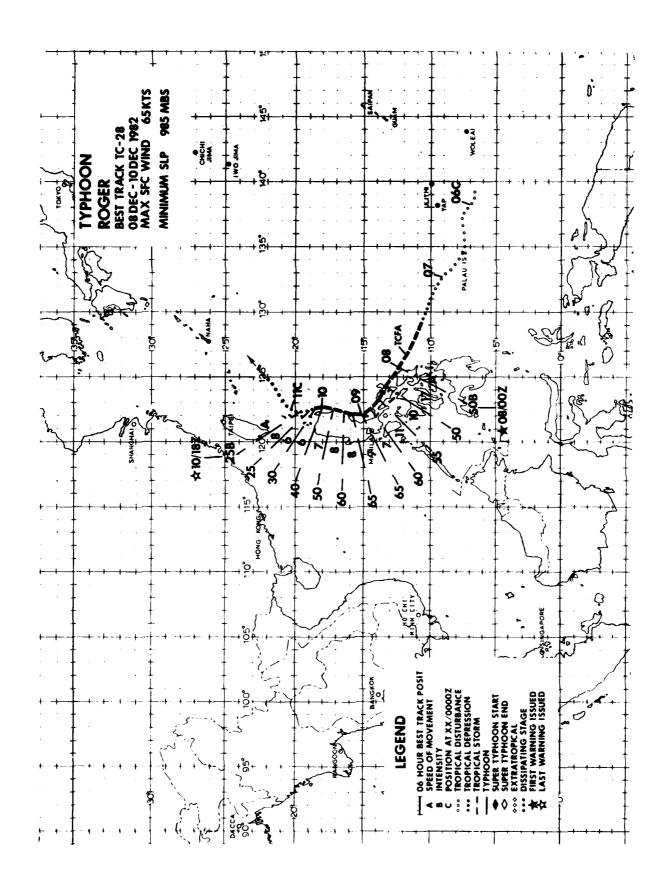
fields, from which this scenario was derived, forecast the subtropical ridge to weaken at all levels as a mid-latitude trough deepened in the East China Sea. This meteorological situation would allow Pamela to recurve toward the northeast, accelerate, and undergo an extratropical transition. However, the low-level (850 mb and below) ridge did not weaken as indicated by the prognostic series, and mamela went on to complete a small anticyclonic loop and moved southwestward toward the Philippines. Early in the loop, Pamela began to interact with the mid-latitude westerlies and once again the effect of increased vertical wind shear weakened Pamela from 80 kt (41 m/sec) to 50 kt (26 m/sec) over a 30-hour

period. However, as Pamela moved southwestward, the subtropical ridge to the north began to strengthen at all levels, allowing Pamela to reintensify to a typhoon for the third time. Pamela reached a maximum intensity of 70 kt (36 m/sec) about six hours prior to entering the islands of the central Philippines.

As Pamela moved through the Philippines and weakened, Tropical Depression 28 (Roger) formed in the Philippine Sea. The combined effects of interaction with the topography of the islands and a shift in the low-level wind regime toward Roger caused Pamela to weaken rapidly and eventually brought on its dissipation over the South China Sea.



Figure 3-27-3. Typhoon Pamela, nearly six kours after attaining a second maximum intensity of 80 kts (41 m/sec). To the south, this imagery also shows Typhoon Roger in its formative stages. 0505342 December (NOAA 7 visual imagery).



Roger was particularly interesting in that it followed closely on the heels of Typhoon Pamela (27). Both systems remained south of the subtropical ridge axis, moved to a mid-tropospheric neutral point near northern Luzon and were profoundly affected by the passage of a mid-latitude trough. In sharp contrast to Pamela, which was a long-lived, significant tropical cyclone, Roger remained an incipient circulation for four days, and required three Tropical Cyclone Formation Alerts (TCFA) before attaining warning status on 7 December.

The first hint of formation occurred at 0306002 when a large area of convection appeared in an upper-level divergence pattern 1200 nm (2222 km) southeast cf Typhoon Pamela. This pattern persisted aloft and drifted west-northwestward at 240 nm (444 km) per day. The low-level circulation center was displaced 150 nm (278 km) south of the cloud

system center. This incongruity, or tilt, was present until 7 December and was, most probably, responsible for the long period of slow development.

The persistent convection feeding an outflow pattern aloft developed into a cloud system center, which prompted a TCPA at 0420002 and its reissuance for relocation at 0508002. Development was arrested late on 5 December and the TCPA was cancelled at 0606002. The upper-level mechanism (troughing off Asia) that was inhibiting Roger's development (in addition to contributing to its vertical tilt) was also affecting Pamela. During this period, Pamela slowed its forward motion, weakened, and changed course from the northwest to the southwest along the periphery of the northeast monsoon. By 0616002 Pamela and (formative) Roger had approached to within 600 nm (1111 km) of each other.

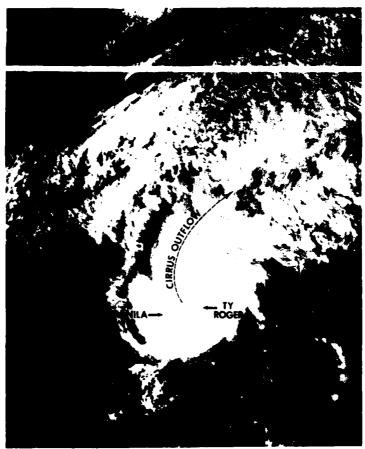


Figure 3-28-1. Expanded visual data of Roger just after reaching typhoon strength off the east coast of Luzon. The extensive low-level cloud deck to the north and northwest of the typhoon's cirrus outflow is embedded in the northeast monsoon. 0906272 December (NOAA 7 visual imagery)

During the next 24 hours the conditions for tropical cyclone development were favorable. Rawinsonde data from southwestern Taiwan (Tung-Chiang, Taiwan (WMO 46747)) indicated a 40 m height rise at 500 mb and reduced vertical wind shear. While Pamela moved into the central Philippines and weakened, Roger remained over water and underwent rapid intensification. The low-level wind circulation center and the cloud system center became vertically aligned and Roger gained tropical storm strength at 0712002. Because of the sparse conventional data and the system's small maximum wind radius, the Joint Typhoon Warning Center could not verify the change in vertical alignment. As a reconnaissance aircraft deployed, a TCFA was issued at 0720002. The first fix from the aircraft indicated a small, tight, 50 kt (26 m/sec) circulation with a minimum central pressure of 1002 mb, which prompted the initial warning at 0800002.

Roger continued to move toward the northwest along the coast of the Philippines and intensified to typhoon strength at 0900002. At 0912002 the 500 mb heights to the north at Tung-Chiang (WMO 46747) began to fall due to an approaching mid-latitude trough; the 700 mb flow had changed from northerly to southerly and the low-level northeast monsoonal flow weakened. Roger weakened to tropical storm intensity and moved northward along the east coast of northern Luzon. Satellite imagery revealed that a long cirrus plume was developing from Roger and streaming northeastward as the vertical shear increased aloft.

Increasing vertical shear, the approaching trough, and southerly low-level steering flow hinted at both recurvature (with sudden acceleration) and rapid shearing. Because of Roger's close proximity to land, aircraft reconnaissance was unable to monitor which scenario was taking place and, as a result, satellite data became the major input to the warnings. This posed a problem for the satellite analysts who could only position the top of the cloud system, which was becoming feature-less and shearing off to the east. By 100600Z the cloud system center had been poorly organized for 12 hours and the apparent location of the low-level circulation center was highly suspect. Fortunately, by this time Roger had sufficient land clearance for the aircraft to be used. The fix located a greatly weakened center just off the northeastern tip of Luzon. These data required amendment of the 100600Z warning; downgrading Roger to a tropical depression, and relocating the circulation center 80 nm (148 km) to the northwest. The increasing vertical shear caused by the mid-latitude trough dropping southeastward across mainland China had disrupted the vertical linkage between the upper- and lower-level circulations and displaced the convection to the southeast.

The remains of the system were monitored for regeneration until 1018002 when the final warning was issued. The exposed low-level center continued to track northeastward for a day and was ingested into the frontogenic zone east of Taiwan.

# 2. NORTH INDIAN OCEAN TROPICAL CYCLONES

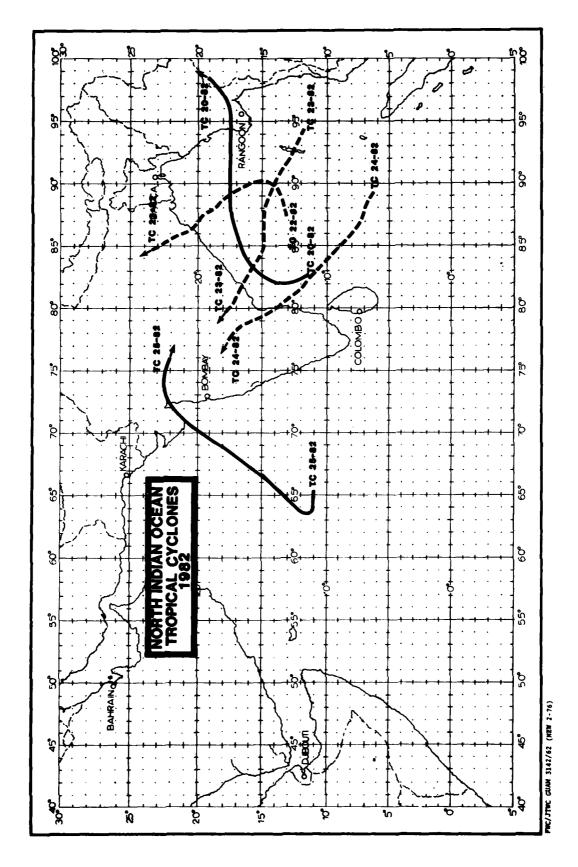
The 1982 North Indian Ocean tropical cyclone season was near normal. Five tropical cyclones reached warning status, two developed during the spring (monsoon) transition season and three developed during the fall transition season. One tropical

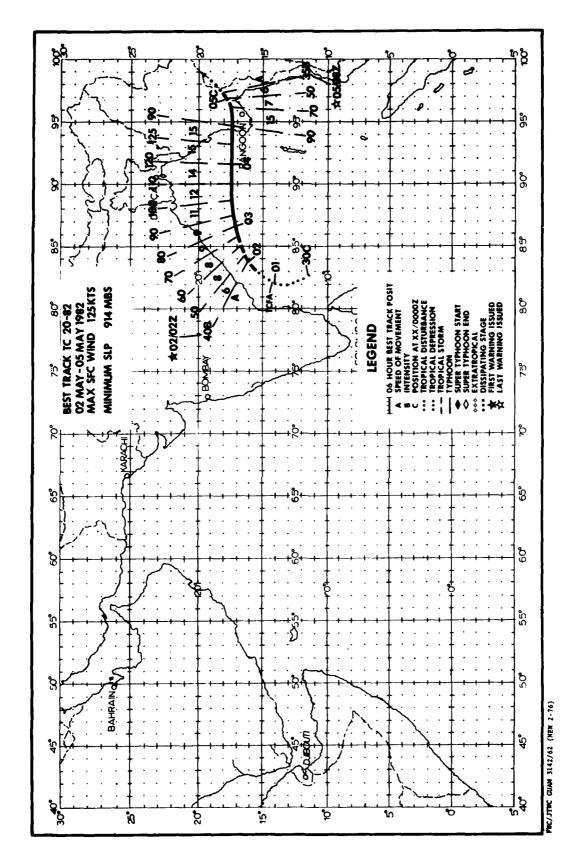
cyclone developed in the Arabian Sea and the remaining four tropical cyclones developed in the Bay of Bengal. Tables 3-6 through 3-8 provide a summary of North Indian Ocean tropical cyclones, Tropical Cyclone Formation Alerts and Warnings.

TABLE 3-6. NORTH INDIAN OCEAN															
1982 SIGNIFICANT TROPICAL CYCLONES															
TROPICAL CYCLON	TROPICAL CYCLONE PERIOD OF WARNING					CALENDAR DAYS OF WARNING		NUMBER OF WARNINGS ISSUED		MAXIMUM SURFACE WIND (KT)		ESTIMATED MSLP (MB)		BEST TRACK DISTANCE TRAVELED (NM)	
1. TC 20-82	2 MAY - 5 MAY			•	4		14	14		125		14	1135		
2. TC 22-82		2 JU	IN -	4 JUN	ì	3		8		5	5	983		482	
3. TC 23-82		14 00	T - 1	6 OCT	•	•3		9		5	0	986		681	
4. TC 24-82		17 OC	T - 1	9 OCT	•	3		7		5	0	987		389	
5. TC 25-82		5 NO	v -	9 NOV	,	5		17		9	0	952		949	
1982 TOTALS: 18 55* * IN ADDITON, TWO AMENDED WARNINGS WERE ISSUED DURING 1982															
TABLE 3-7.															
1982 SIGNIFICANT TROPICAL CYCLONES															
NORTH INDIAN OCEAN															
	<u>Jan</u>	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	<u>NOV</u>	DEC	TOTAL	:	
ALL TROPICAL CYCLONES	0	0	0	0	1	1	0	0	0	2	1	0	5		
<u>1975-1981</u>															
AVERAGE	. 1	-	-	.1	. 7	. 4	-	-	. 4	.9	1.4	. 4	4.6		
CASES	1	0	0	1	5	3	0	0	3	6	10	3	32		
FORMATION ALERTS: Five of the nine Formation Alert Events developed into significant tropical cyclones.															
WARNINGS: Number of warning days: 18															
Number of warning days with two tropical cyclones in region:															
Number of warning days with three or more tropical cyclones in region: 0															

TABLE 3-8.	·		-			·							
	En	COURN	CV OF	mnon		avar a	c n	V MON	m.,	n una			
FREQUENCY OF TROPICAL CYCLONES BY MONTH AND YEAR													
YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	<u>oct</u>	NOV	DEC	TOTAL
1971*	_	_	_	_	-	0	0	0	0	1	1	0	2
1972*	0	0	0	1	0	ō	Ö	ō	2	ō	ī	Ō	4
1973*	ō	Ó	Ō	ō	ō	ō	0	Ō	ō	ì	2	ì	4
1974*	0	0	0	0	0	0	0	0	0	0	1	0	1
1975	1	0	0	0	2	0	0	0	0	1	2	0	6
1976	0	0	0	1	0	1	0	0	1	1	0	1	6 5 5
1977	0	0	0	0	1	1	0	0	0	1	2	0	5
1978	0	0	0	0	1	0	0	0	0	1	2	0	4
1979	0	0	0	0	1	1	0	0	2	1	2	0	7
1980	0	0	0	0	0	0	0	0	0	0	1	1	2 3 5
1981	0	0	0	0	0	0	0	0	0	1	1	1	3
1982	0	0	0	0	1	1	0	0	0	2	1	0	5
1975-1982													
AVERAGE	.1	-	-	.1	.8	. 5	-	-	. 4	1.0	1.4	. 4	4.6
CASES	1	0	0	1	6	4	0	0	3	8	11	3	37

<sup>\*</sup> JTWC warning responsibility began on 4 June 1971 for the Bay of Bengal, east of 90E. As directed by CINCPAC, JTWC issued warnings only for those tropical cyclones that developed or tracked through that portion of the Bay of Bengal. Commencing with the 1975 tropical cyclone season, JTWC's area of responsibility was extended westward to include the western portion of the Bay of Bengal and the entire Arabian Sea.





During late April, the monsoon trough was anchored in the latitudes south of Sri Lanka and extended eastward into the central portion of the Bay of Bengal. On 26 April, an area of convection associated with this trough became suspect and was discussed in the Significant Tropical Weather Advisory (ABEH PGTW); however, center fixes from satellite data were not available until 30 April when an upper-level circulation center was analyzed over the convection. On 1 May, a Tropical Cyclone Formation Alert was issued as a central dense overcast (CDO) formed over the system.

During this period, there was some concern about the actual intensity of the system at the surface. Surface observations from India, Sri Lanka, and throughout the Bay of Bengal indicated light and variable winds close to the developing system and the strongest winds (15 to 20 kt (8 to 10 m/sec)) far removed from the convection. Additionally, satellite fixes lacked continuity in tracking the system and the possibility that a signif cant surface circulation had not yet established itself seemed very realistic. However, NOAA 7 satellite imagery at 0121322, received and analyzed at Air Force Global Weather Central (AFGWC), indicated a substantial increase in the system's convective organization which prompted the issuance of the first warning for Tropical Cyclone 20-82 at 0202002. From the initial warning position 440 nm (815 km) north-northeast of Sri Lanka, Tropical Cyclone 20-82 moved northeastward, remaining approximately 120 nm (222 km) east of India. Fix positions remained somewhat erratic in the early stages but improved when satellite imagery (021327Z NOAA 7) indicated that an eye had developed. The appearance of the eye also laid to rest any lingering doubts as to whether Tropical

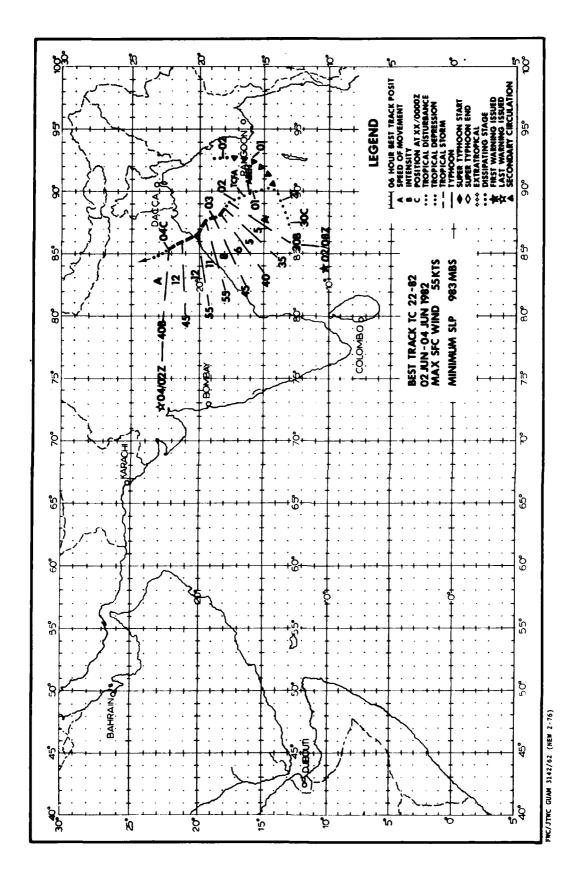
Cyclone 20-82 had developed into a significant tropical cyclone.

Track forecasts for Tropical Cyclone 20-82 were very good. From the first warning, Tropical Cyclone 20-82 was expected to move northeastward and turn more eastward with time. As Tropical Cyclone 20-82 approached 18N, it's movement became virtually eastward across the Bay of Bengal until landfall. While crossing the Bay of Bengal, Tropical Cyclone 20-82 continued to intensify and reached an estimated maximum intensity of 125 kt (64 m/sec) just prior to landfall. Best track intensities were based almost exclusively on Dvorak intensity estimates received from AFGWC and from Detachment 1,1WW, Nimitz Hill, Guam. However, despite the absence of verifying synoptic reports, satellite imagery (Figure 3-29-1) and later, casualty reports from Burma were convincing evidence that Tropical Cyclone 20-82 was a very intense (although quite compact) tropical cyclone.

The value of the meteorological satellite, especially in data sparse regions, has once again proven itself. In the era prior to the availability of imagery from satellites, Tropical Cyclone 20-82 would have been an undetected storm of great intensity that would strike without warning. A news release from Rangoon, Burma on 6 May, reported 7,000 homes destroyed in one township, and 85% of the homes and buildings in another township had their roofs blown away. Elsewhere, along Tropical Cyclone 20-82's path, schools, industries and hospitals were damaged or destroyed. Yet despite this extensive destruction, there were just five deaths reported in a region of the world where loss of human life is frequently in the hundreds from the effects of tropical cyclones.



Figure 3-29-1. Tropical Cyclone 20-82 near maximum intensity, just west of Burma, 0504232 May. (NOAA 7 visual satellite imagery from AFGWC, Offutt, AFB, Nebraska)



Tropical Cyclone 22-82 was the second significant tropical cyclone to develop in the Bay of Bengal during the spring (monsoon) transition season. During the last week of May, there was considerable convective activity over the central Bay of Bengal, resulting in two Tropical Cyclone Formation Alerts (TCFA) that were issued for a disturbance which tracked northeastward and moved into Burma on 29 May.

At 2900002, a new convective area could be detected on satellite imagery moving out of a monsoon cloud band near 9N in the central Bay. During the ensuing three days, the convective area drifted northward with little evidence of a closed surface circulation. The synoptic environment in the Bay of Bengal at this time was dominated by strong (30 to 40 kt (15 to 21 m/sec)) westerly flow south of 9N, and by a 996 mb heat low over northern India.

By 010600Z June, the convective mass became more organized as an upper-level anticyclone could be analyzed from synoptic data, while visual satellite imagery revealed an exposed low-level circulation some 120 nm (222 km) to the northeast of the convective area. During the next 12 hours, satellite imagery indicated continued convective organization and at 011835Z, a TCFA was issued with the stipulation that the potential for significant tropical

cyclone development was good, provided that either the low-level and upper-level features became better aligned or a new circulation developed under the convection. By 0208002, when satellite data suggested that the latter case had occurred (the convective system had continued to develop and the exposed low-level circulation could no longer be detected on visual imagery), the first warning was issued for Tropical Cyclone 22-82.

During its short lifetime, Tropical Cyclone 22-82 followed a fairly straight, and climatological, northwestward track. Initially moving at 5 kt (9 km/hr), Tropical Cyclone 22-82 steadily increased it forward speed to 12 kt (22 km/hr) and intensified until making landfall at 031400Z. Satellite data from Air Force Global Weather Central (AFGWC) (Figure 3-30-1) and radar reports received at the Indian regional forecast center, indicated that Tropical Cyclone 22-82 was developing an eye when landfall was made just north of Paradip, 150 nm (278 km) southeast of Calcutta. In the coastal districts near Paradip and Orissa, where the tropical cyclone hit hardest, casuality reports indicated that more than 140 people were killed and more than 500,000 homes were destroyed. After landfall, Tropical Cyclone 22-82 rapidly dissipated as it tracked into the extreme southern portion of the Ganges River Valley.

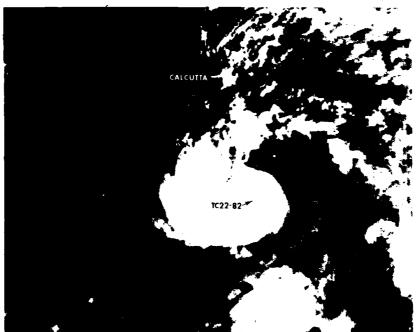
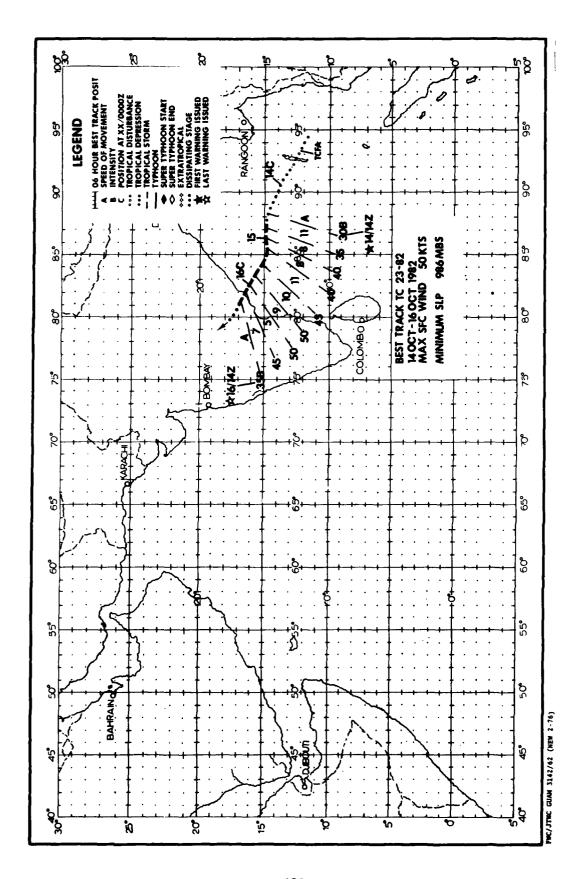


Figure 3-30-1. Tropical Cuclone 22-8: about five hours prior to landfall with an irrourar 15 nm 128 km eye near the center of the centual dense overcast, 0306587 June (NOAA 7 visual satellite imagery from AFGWC, Offult AFB, Nobraska).



### TROPICAL CYCLONE 23-82

The initial stages of Tropical Cyclone 23-82's development were characterized by a persistent upper-level anticyclone and a weak surface disturbance associated with a broad area of convection. Initially detected on 9 October, JTWC tracked a westward-moving surface circulation from the Gulf of Thailand across the Malay Peninsula. Little development was evident from synoptic or satellite data as the system entered the southern Bay of Bengal. On 13 October, convection began to increase and show signs of organization while the system moved west of the Andaman Islands. A Tropical Cyclone Formation Alert was issued at 130600Z when satellite imagery revealed that the system's convection had organized under a more distinctly defined upper-level anticyclone. Late on 14 October satellite imagery showed that a strong central convective feature had developed and that upper-level outflow had increased. Based on these data, and the

expectation of further development, the initial warning was issued at 1414002 for Tropical Cyclone 23-82.

The forecast tracks issued throughout Tropical Cyclone 23-82's lifespan anticipated movement toward the west-northwest in response to a mid-level steering current induced by a subtropical ridge centered over Burma. Tropical Cyclone 23-82 proved to be a "well-behaved" system and followed the forecast track toward the east coast of India. While in warning status Tropical Cyclone 23-82 gradually intensified and reached a peak intensity of 50 kt (26 m/sec) six hours prior to landfall. At approximately 1612002, Tropical Cyclone 23-82 passed 35 nm (65 km) south of Kakinada, India (WMO 43189) with observed maximum sustained winds of 20 kt (10 m/sec). From Kakinada, Tropical Cyclone 23-82 proceeded inland and gradually dissipated.

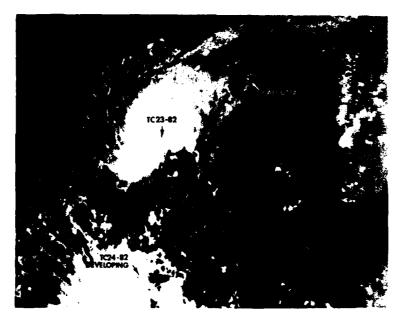
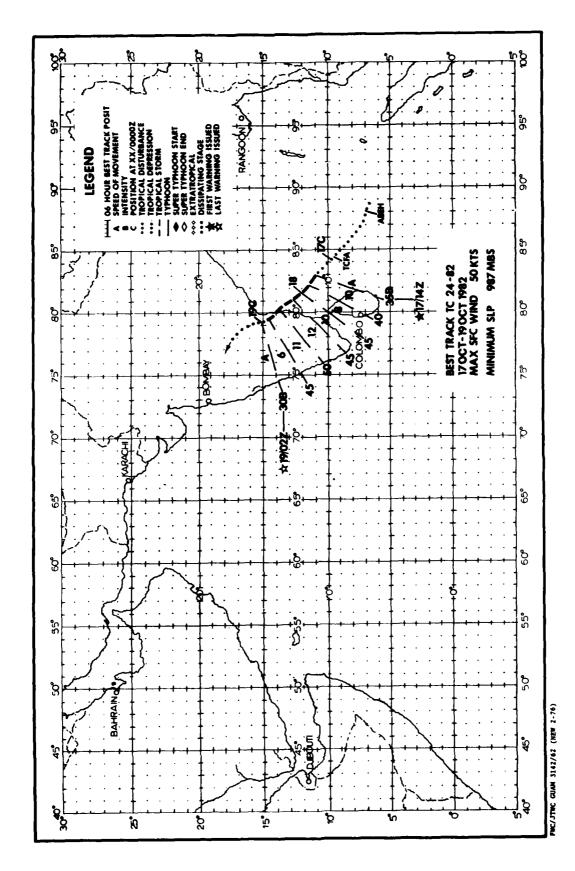


Figure :-31-1. Tropical Cyclone 23-82 near landfall along the east coast of India with surface winds near 45 kt (23 m/sec). Tropical Cyclone 24-82 can be seen in its formative stages near Sri Lanka, 1608562 October (NOAA 7 visual imagery from AFCWC Offutt AFB, Nebraska).



## TROPICAL CYCLONE 24-82

Tropical Cyclone 24-82 developed from an area of convective activity first observed on 15 October about 400 nm (740 km) east of Sri Lanka in the Bay of Bengal. No surface circulation was present but a weak upperlevel anticyclone was evident on satellite imagery. During the next two days, the area was monitored for further development as it drifted slowly to the northwest. On the 16th, synoptic data and satellite imagery indicated that a loosely organized surface circulation had developed. In combination with the upper-level anticyclone, this circulation was considered to have good potential for intensification and a Tropical Cyclone Formation Alert was issued at 1623002.

Subsequent satellite imagery indicated that the circulation had come together at the surface and mid-levels. JTWC issued the

first warning on Tropical Cyclone 24-82 at 1714002. Mid-level steering flow at the time was from the southeast due to the presence of a 500 mb anticyclone over Indochina. Numerical forecast products indicated that this mid-level anticyclone would retain its intensity and location throughout the ensuing 72 hours, thus, Tropical Cyclone 24-82 was forecast to continue moving northwestward. The system did move as expected, making landfall near Sriharikota Island at 1814002 with maximum sustained winds of 50 kt (26 m/sec).

Damage to private dwellings in Nellore District was extensive with an estimated 10,000 collapsed huts. Casualties were reported to be 5 dead and 10 injured. Tropical Cyclone 24-82 continued drifting northwestward after landfall and dissipated over central India.

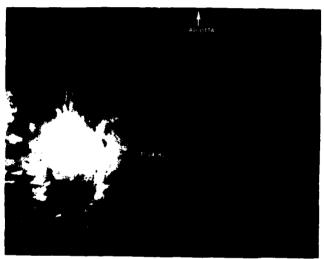
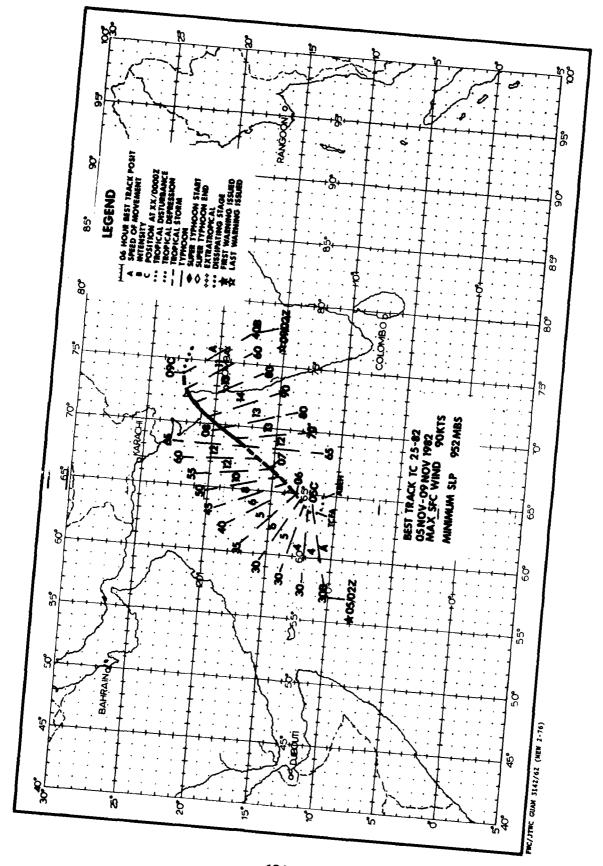


Figure 3-32-1. This satellite imagery indicated Tropical Cyclone 24-82 had organized sufficiently to warrant the issuance of tropical cyclone warnings. 1708432 October (NOAA 1 visual imagery from AFGWC Offutt AFB, Nebraska).



#### TROPICAL CYCLONE 25-82

Tropical Cyclone 25-82 developed from an area of loosely organized convection in the central Arabian Sea. Although satellite images indicated that the convection and cloud system organization were increasing, shipboard synoptic reports were the first data to accurately describe the low-level circulation center. At 042002 November, a Tropical Cyclone Formation Alert was issued when nearby shipboard observations indicated pressures near 1004 mb and winds of 20 kt (10 m/sec), confirming intensity estimates from earlier satellite data. Satellite and synoptic data during the subsequent 12-hour period indicated that development was continuing, prompting the first warning on Tropical Cyclone 25-82 at 0502002.

Tropical Cyclone 25-82 slowly consolidated during the initial 24-hour period in warning status. Based on guidance from virtually every forecast aid, the first

six warnings anticipated a movement toward the west-northwest. However, once the system organized and satellite fixes became more consistent, it became evident that Tropical Cyclone 25-82 was not moving westward as forecast. In the same time frame, a break developed in the mid-level subtropical ridge, which lay along 23N. As height falls occurred across the northern Arabian Sea coast, the tropical cyclone responded by accelerating toward the northeast and intensifying. Tropical Cyclone 25-82 continued to deepen until landfall at 0810002 near the Indian port city of Veraval (20.9N 70.4E). Veraval was particularly hard hit as the cyclone moved onshore with sustained winds of 90 kt (46 m/sec).

Once overland, and deprived of the low-level moist layer over water, Tropical Cyclone 25-82 rapidly dissipated, leaving in its wake at least 50,000 homes damaged or destroyed and a death toll in excess of 341.

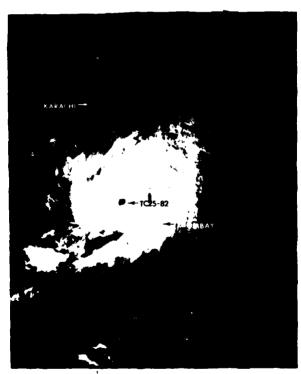


Figure 3-33-1. Tropical Cyclone 25-82 is at peak intensity with maximum winds of 90 kt (46 m/sec) and just making landfall on India's northwestern coast. 0809212 November (NOAA 7 visual imagery from AFGNC Offutt AFB, Nebraska)

NAUTICAL MILE ERROR FIGURE 4-2. Frequency distribution of the 24-, 48-, and 72-hour forecast errors for all significant tropical cyclones in the western North Pacific during the 1982 season. 24-HOUR FORECAST ERRORS (nm) 24-HR 72-HR 48-HR ŏ MEAN: MEDIAN: STANDARD DEVIATION: CASES: NAUTICAL MILE ERROR 48-HOUR CASES W) 10 NAUTICAL MILE ERROR 30 30 72-HOUR NUMBER OF 

# CHAPTER IV - SUMMARY OF FORECAST VERIFICATION

### 1. ANNUAL FORECAST VERIFICATION

#### a. Western North Pacific Ocean

The positions given for warning times and those at the 24-, 48-, and 72-hour fore-cast times were verified against the post-analysis "best-track" positions at the same valid times. The resultant vector and right angle (track) errors (illustrated in Figure 4-1) were then calculated for each tropical cyclone and are presented in Table 4-1. Figure 4-2 provides the frequency distributions of vector errors for 24-, 48- and 72-hour forecasts of all 1982 tropical cyclones in the western North Pacific. A summation of the mean errors, as calculated

for all tropical cyclones in each year, is shown in Table 4-2 for comparative purposes. The data used in this table are not to be confused with that presented in earlier years where the sample was restricted to tropical cyclones that reached typhoon intensity and then had the forecast errors calculated only for that portion of the life-cycle when the intensity was greater than 34 knots (last published as Table 5-1, 1977 Annual Typhoon Report). A comparison of the results using the truncated data set and those obtained for all tropical cyclones can be seen directly in Table 4-3. The annual mean vector errors are graphed in Figure 4-3.

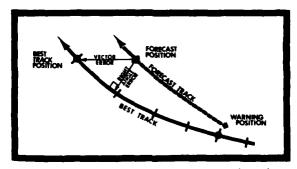


FIGURE 4-1. Illustration of the method to determine vector error and right angle error.

TABLE	4-1,												
				SIC	RECAST ER	ROR SUMMAN TROPICAL (	YCLONES (	F 1982.	(ERRORS	IN IMI)			
			WARRING			24-HOUR			48-HOUR			72-18OUR	
		POSIT	RT AFFILE	HR OF WRNGS	POSIT	RT ANGLE ERBOR	WILINGS	POSIT ERROR	RT ANGLE	NR OF WINNES	POSIT ERROR	RT ANGLE ERROR	WELFIGS
1.	TY NAMIE	25	14	35	93	48	32	186	86	24	276	115	23
2.	TY WELSON	24	13	53	95	57	49	180	l i4	44	170	72	37
3.	TY ODESSA	29	16	25	228	113	21	520	226	17	742	385	13
4.	TY PAT	26	24	23	149	134	19	299	237	15	583	394	11
5.	TY RUBY	27	12	23	144	64	19	275	143	15	425	326	11
6.	TS TESS	15	9	14	107	73	10	217	142	3	344	41	1
7.	TS SKIP	16	15	7	95	32	3						
8.	TS VAL	29	22	5	363	33	1						
9.	TS WINONA	22	13	21	100	42	16	175	93	13	224	121	9
٥.	TY ANDY	24	14	32	99	50	28	168	106	23	231	144	19
11.	STY BESS	18	13	43	121	64	39	267	122	35	396	198	31
12.	TY CECIL	14	•	39	102	41	33	172	75	30	219	141	23
13.	TY DOT	22	17	27	108	68	24	216	172	20	262	208	16
14.	TY ELLIS	14	8	36	76	42	32	171	Bl	26	263	153	22
15.	TY FAYE	18		50	142	49	41	384	273	33	639	443	27
16.	TY CORDON	15	11	38	100	62	34	214	101	30	364	210	26
17.	TS HOPE	19	9	10	186	79	6	426	118	2			
18.	TY INVING	13	9	44	73	42	40	110	72	35	172	126	32
19.	TY JUDY	19	15	29	125	73	25	298	126	19	401	262	13
20,	TY KEN	15	9	37	75	49	33	201	134	29	344	263	25
21.	TS LOLA	21	14	12	88	68	8	232	152	4			
22.	TD 22	35	21	5	155	83	1						
23.	STY MAC	14	13	32	90	63	28	162	104	24	294	149	20
24.	TY HARCY	12	10	29	86	74	26	213	175	21	430	333	17
25.	TD 25	35	33	5	113	119	1						
26.	TY OWER	24	18	40	146	103	32	364	236	24	350	285	18
27.	TY PARTILA	20	14	60	L 39	79	56	263	149	45	280	140	34
28.	TY ROCKS	17	17	12	129	116	8	383	329	4			
41.	PORECASTS:	19	13	786	113	67	665	237	139	535	34 1	206	428

TABLE 4-2.	ANI	NUAL MEAN FORE	CAST ERRO	RS (NM) FOR THE	WESTERN !	PACIFIC
İ	2.	4-HOUR	4:	8-HOUR	7	2-HOUR
<u>YEAR</u>	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971	111	64	212	118	317	117
1972	117	72	245	146	381	210
1973	108	74	197	134	253	162
1974	120	78	226	157	348	245
1975	138	84	288	181	450	290
1976	117	71	230	132	338	202
1977	148	83	283	157	407	228
1978	127	75	271	179	410	297
1979	124	77	226	151	316	223
1980	126	79	243	164	389	287
1981*	123	75	220	119	334	168
1982*	113	67	237	139	341	206

The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

BLE 4-3.	ANNUAL MEAN FO	RECAST ERRORS	(NM) FOR WE	STERN NORTH PAG	CIFIC	
	2	4-HOUR	4	8-HOUR	72	2-HOUR
YEAR	ALL	TYPHOON*	ALL	TYPHOON*	ALL	TYPHOON*
1950-58		170				
1959		117**		267**		
1960		177**		354**		
1961		136		274		
1962		344		287		476
1963		127		246		374
1964		133		284		429
1965		151		303		418
1966		136		280		432
1967		125		276		414
1968		105		229		337
1969		111		237		349
1970	104	98	190	181	279	272
1971	111	99	212	203	317	308
1972	117	116	245	245	381	382
1973	108	102	197	193	253	245
1974	120	114	226	218	348	351
1975	138	129	288	279	450	442
1976	117	117	230	232	338	336
1977	148	140	283	266	407	390
1978	127	120	271	241	410	459
1979	124	113	226	219	316	319
1980	126	116	243	221	389	362
1981	123	117	220	215	334	342
1982	113	114	237	229	341	337

<sup>\*</sup> For Typhoons only while winds were over 35 kt (18 m/sec).

<sup>\*\*</sup> Forecast positions north of 35°N were not verified.

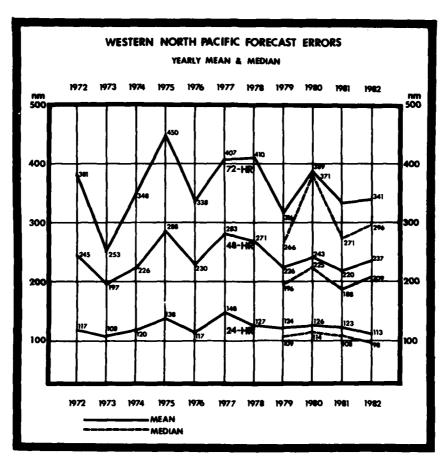


FIGURE 4-3. Annual mean and median vector errors (nm) for all tropical cyclones in the western North Pacific.

#### b. North Indian Ocean

The positions given for warning times and those at the 24-, 48- and 72-hour valid times were verified for tropical cyclones in the North Indian Ocean by the same methods used for the western North Pacific. It should be noted that due to the low number of North Indian Ocean tropical cyclones,

these error statistics should not be taken as representative of any trend. Table 4-4 is the forecast error summary for the North Indian Ocean and Table 4-5 contains the annual average of forecast errors back through 1971. Vector errors are plotted in Figure 4-4. (Seventy-two hour forecast errors were evaluated for the first time in 1979).

		_											
TAI	DLE 4-4.												
				F	ORECAST E	RROR SUMMA	RY FOR T	HE NORTH	INDIAN OCI	CAN			
						TROPICAL C			(ERRORS	IN NM)			
									•				
			WARNING			24-HOUR			48-HOUR			72-HOUR	
		POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF
		error	ERROR	WRNGS	ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS
1.	TC 20-82	23	14	14	118	43	10	283	87	6	340	116	2
2.	TC 22-82	22	16	8	106	36	5	238	85	1			
3.	TC 23-82	34	18	9	88	49	6	151	86	2			
4.	TC 24-82	22	15	7	68	22	3						
5.	TC 25-82	55	34	17	205	113	13	487	264	9	931	519	5
ALL	FORECASTS:	35	21	55		66	37	368	175	18	762	404	7

#### TABLE 4-5.

#### ANNUAL MEAN FORECAST ERRORS FOR THE NORTH INDIAN OCEAN

	24	-HOUR	48	B-HOUR	72	2-HOUR
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971*	232	-	410	-	-	-
1972*	224	101	292	112	-	-
1973*	182	99	299	160	-	-
1974*	137	81	238	146	-	-
1975	145	99	228	144	-	-
1976	138	108	204	159	-	-
1977	122	94	292	214	-	-
1978	133	86	202	128	-	-
1979	151	99	270	202	437	371
1980	115	73	93	87	167	126
1981**	109	65	176	103	197	73
1982**	138	66	368	175	762	404

<sup>\*</sup> The western Bay of Bengal and the Arabian Sea were not included in the JTWC area of responsibility until the 1975 tropical cyclone season.

<sup>\*\*</sup> The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

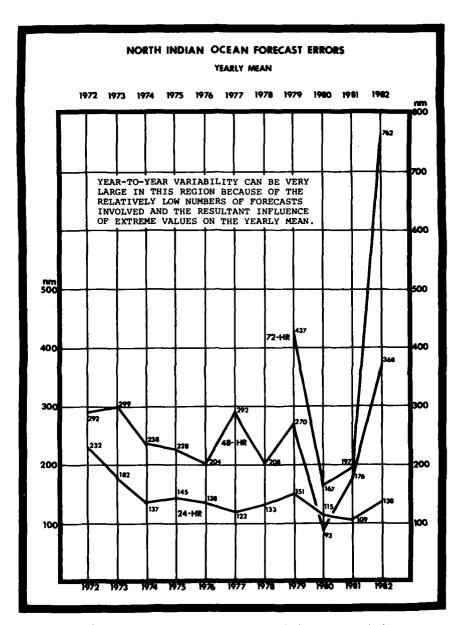


FIGURE 4-4. Annual mean vector errors (nm) for all tropical cyclones in the North Indian Ocean.

#### 2. COMPARISION OF OBJECTIVE TECHNIQUES

#### a. General

Objective techniques used by JTWC are divided into five main categories:

- (1) climatological and analog techniques;
- (2) extrapolation;
- (3) steering techniques;
- (4) dynamic models;
- (5) empirical and analytical techniques

In September 1981, JTWC began to initialize its array of objective forecast techniques (described below) on the sixhour-old preliminary best track position (an interpolative process) rather than the forecast (partially extrapolated) warning position, e.g. the 06002 warning is now supported by objective techniques developed from the 00002 preliminary best track position. This operational change has yielded several advantages:

\*techniques can now be requested much earlier in the warning development time line, i.e. as soon as the track can be approximated by one or more fix positions on, or after the valid time of the previous warning; \*receipt of these techniques is virtually assured prior to development of the next warning

\*improved (mean) forecast accuracy. This latter aspect arises because JTWC now has a more reliable approximation of the short-term tropical cyclone movement. Further, since most of the objective techniques are biased for persistence, this new procedure optimizes their performance and provides more consistent guidance on short-term movement, indirectly yielding a more accurate initial position estimate as well as lowering 24-hour forecast errors.

- b. Description of Objective Techniques
- (1) CLIM -- A climatological aid providing 24-, 48- and 72-hour tropical cyclone forecast positions (and intensity changes in the western North Pacific) based upon the position of the tropical cyclone. The output is based upon data records from 1945 to 1981 for the western North Pacific Ocean and 1900 to 1981 for the North Indian Ocean
- (2) TYAN78 -- An updated analog program which combines the earlier versions TYPN 75 and INJAH 74. The program scans history tapes for tropical cyclones similar (within a specified acceptance envelope) to the current tropical cyclone. For the western North Pacific Ocean, three forecasts of position and intensity are provided for 24-, 48- and 72-hours: RECR a weighted

mean of all accepted tropical cyclones which were categorized as "recurving" during their best track period; STRA - a weighted mean of all accepted tropical cyclones which were categorized as moving "straight" (westward) during their best track period; and TOTL - a weighted mean of all accepted tropical cyclones, including those used in the RECR and STRA forecasts. For the North Indian Ocean, a single (total) forecast track is provided for 12-hour intervals to 72 hours.

- (3) BPAC -- A program which generates 12- to 72-hour forecast positions based on blending the past motion of the tropical cyclone with the CLIM forecast positions. The blending routine gives less weight to persistence at each succeeding forecast interval.
- (4) XTRP -- Forecast positions for 24- and 48-hours are derived from the extension of a straight line which connects the most-recent and 12-hour-old preliminary best track positions.
- (5) HPAC -- 24- and 48-hour forecast positions are derived by merely connecting the mid-points of straight lines which connect these positions on the XTRP and CLIM tracks, respectively.
- (6) CYCLOPS -- An updated version of the HATTRACK/MOHATT steering program which can provide geostrophic steering forecasts at the 1000-, 850-, 700-, 500-, 400-, and 200-mb levels. The program can be run in a modified (includes a 12-hour persistence bias) or unmodified mode applied to either analysis or prognostic fields. The program advects a point vortex on a preselected analysis and/or smoothed prognostic field at designated levels in six-hour time steps through 72 hours. In 1982, only the modified version, in the prognostic mode for the 500-mb level was verified; however, JTWC routinely uses many of the other levels and modes as operational forecast aids.
- (7) OTCM -- (One-way Tropical Cyclone Model) A coarse-mesh, three-layer in the vertical, primitive equation model with a 205 km grid spacing over a 6400 x 4700 km domain. The model's fields are computed around a bogused, digitized cyclone vortex using FNOC Global Bands prognostic fields for the specified valid time. The past motion of the tropical cyclone is compared to initial steering fields and a bias correction is computed and applied to the model. FNOC hemispheric prognostic fields are used at 12-hour intervals to update the model's boundaries. The resultant forecast positions are derived by locating the 850 mb vortex at six-hour intervals to 72 hours. In 1982, the OTCM was requested for each warning; and when computer resources were available, the OTCM forecast was normally available to the TDO within one hour of the request.

- (8) NTCM -- (Nested Tropical Cyclone Model) A primitive equation model with similar properties as the OTCM. The NTCM differs by containing a finer scale "nested" grid, initializing on Global Bands analysis fields, not containing a (persistence) bias correction, and being a channel model which runs independent of FNOC prognostic fields (not requiring updating of its boundaries). The "nested" grid covers a 1200 x 1200 km area with a 41 km grid spacing which moves within the coarsemesh domain to keep an 850 mb vortex at its center. In 1982, the NTCM was incorporated into the FNOC job-stream and 72-hour forecast tracks were produced automatically from analysis fields, utilizing the 00002 and 12002 warning positions. These forecasts were normally received within 12 hours of their valid times and provided guidance for 1200Z and 0000Z warnings, respectively.
- (9) TAPT -- A technique which utilizes upper-tropospheric wind fields to estimate the latitude of initial acceleration associated with the tropical cyclone's interaction with the mid-latitude westerly steering currents. Further, the technique provides speed of movement guidelines for duration and upper-limits, and insight on the probable path of the tropical cyclone, given a prevailing upper-wind pattern during the acceleration process.
- (10) THETA E -- An empirically derived relationship between a tropical cyclone's minimum sea level pressure (MSLP) and (700 mb) equivalent notential temperature ( $\theta_{\rm e}$ ) was developed by Sikora (1976) and Dunnavan (1981). By monitoring MSLP and  $\theta_{\rm e}$  trends, the forecaster can evaluate the potential for sudden, rapid deepening of a tropical cyclone.

- (11) WIND RADIUS -- Following an analytic model of the radial profiles of sea level pressures and winds in mature tropical cyclones (Holland, 1980), a set of radii for 30-, 50-, and 100-knot winds based on the tropical cyclone's maximum intensity and radius of maximum winds have been produced to aid the forecaster in determining forecast wind radii.
- (12) DVORAK -- An estimation of a tropical cyclone's current and 24-hour forecast intensity is made from interpretation of visual satellite imagery (Dvorak, 1973) and provided to the forecaster. These intensity estimates are used in conjunction with other intensity-related data and trends to forecast tropical cyclone intensity.

#### c. Testing and Results

A comparison of selected techniques is included in Table 4-7 for all western North Pacific tropical cyclones and in Table 4-9 for all North Indian Ocean tropical cyclones. In these tables, "X-AXIS" refers to techniques listed vertically. The example in Table 4-7 compares CY50 to OTCM, i.e. in the 435 cases available for a (homogeneous) comparison, the average vector error at 24 hours was 111 nm for CY50 and 119 nm for OTCM. The difference of 8 nm is shown in the lower right. (Differences are not always exact, due to computational round-off which occurs for each of the cases available for comparison).

A comparison of mean and median forecast errors (for a non-homogeneous data set) is provided for selected techniques in Table 4-6 for all western North Pacific tropical cyclones and in Table 4-8 for all North Indian Ocean tropical cyclones.

TABLE 4-6.

# COMPARISON OF FORECAST ERRORS (NM) BY TECHNIQUE IN 1982 FOR THE WESTERN NORTH PACIFIC

		24-HOUR	RESUL STD	TS*		48-HOUR	RESUL STD	TS*		72-HOUR	RESUL STD	TS*
TECHNIQUE	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)
JTWC	113	98	73	(665)	237	209	158	(535)	341	296	225	(428)
RECR	116	97	77	(588)	237	203	144	(504)	387	344	243	(423)
STRA	121	101	85	(589)	258	205	185	(513)	434	312	271	(434)
TOTL	112	96	72	(612)	230	197	145	(523)	440	321	246	(440)
CY50	112	100	69	(579)	277	236	184	(496)	408	407	315	(408)
NTCM	143	128	85	(181)	238	208	140	(153)	353	347	180	(124)
OTCM	122	108	73	(479)	232	206	134	(405)	330	289	220	(330)
BPAC	123	104	79	(613)	248	207	169	(527)	442	309	285	(442)
CLIM	150	126	100	(648)	272	226	182	(554)	467	323	295	(467)
XTRP	117	101	89	(635)	264	229	168	(542)				
HPAC	112	98	76	(633)	217	183	143	(540)				

THIS DATA SET REPRESENTS ALL FORECAST ERRORS FOR EACH TECHNIQUE LISTED AGAINST THE CORRESPONDING BEST TRACK POSITIONS AT 24, 48, AND 72 HOURS.

TABLE 4-7. 1982 ERROR STATISTICS FOR SELECTED OBJECTIVE TECHNIQUES IN THE WESTERN NORTH PACIFIC OCEAN

									24-H0	UR FOI	RECAST	ERRO	RS (NO	I)								
24-		WC	RE	CR	ST	'RA	TO	TL	CY	50	<u>NT</u>	CM	01	CM	ВР	AC	C1	IM	X	RP	НР	AC_
JTWC	665 113	113																				
PECR	583 115	113 2	588 116	116 0							Г	NUMB	ER	,	C-AXIS	7						
STRA	584 121	110 11	561 120	114 7	589 121	121 0						CASE			CHNIQUI ERROR							
TOTL	607 112	112 0	583 110	116 -5	583 110	121 -10	612 112	112 0			7	Y-AX TECHNI	QUE		RROR FERENC	Œ						
CY50	575 112	112 0	534 110	114 -2	532 107	119 -11	554 110	111	579 112	112 0	<b>)</b> -	ERRO	R	,	<u> </u>							
NTCM	179 143	102 40	163 141	111 30	159 137	120 17	167 141	108 33	159 142	113 29	181	143										
OTCM	477 122	113	123	119	436 118	122 -2	455 122	113	119	8	138 120	137 -15	479 122	122								
BPAC	610 122	111	556 121	114 8	559 120	119 1	580 121	110 12	548 119	110 9	170 119	140 -20	458 121	120 1	613 123	123						
CLIM	643 150	112 38	585 148	116 32	587 146	121 25	609 150	112 38	574 149	111 38	176 148	142 7	476 150	122 28	611 147	122 24	648 150	150 0				
XTRP	630 117	112 5	575 114	116 -1	575 110	121 -10	599 113	112 1	566 115	111 5	171 113	142 -29	469 119	121 -1	600 116	121 -4	633 117	150 -32	635 117	117 0		
HPAC	628 111	111 0	573 109	116 ~5	575 107	121 -14	597 110	112 -1	564 110	110 0	171 108	142 -33	468 113	121 -8	600 109	121 -11	633 112	150 -37	633 112	117 -4	633 112	112 0
		-					-		48-но	UR FO	RECAST	ERRO	RS (NM	1)								
48-		WC	RE	CR	ST	RA	TO	TL	CY	50	NT	CM	01	CM	ВР	AC	CI	.IM	X1	TRP	нР	AC
JTWC	535 237	237													JTW	- OF	FICIA	. JTWC	FORE	CAST		7
RECR	476 233	233	504 237	237 0											RECI STRA	- RE	CURVE RAIGH	R (TYA T (TYA	N 78) N 78)			
STRA	486 258	231 26	489 256	234	513 258	258									CY 50	- CY	TAL (1 CLOPS STED 1	MODIF	1FD 50			ŀ
TOTL CY50	493 228 466	234 -5 235	498 227 458	238 -10 239	508 228 468	257 -28 261	523 230 475	230 0 231	496	277					BPAG	- BL	IE-WAY ENDED IMATO	PERSI			MODEI CLIM	
NTCM	267 145	32 221	277 139	39 231	272 139	12	277 141	46	277 139	0 291	153	238			XTRI	- 12	-HOUR	EXTRA				1
OTCM	238	16 237	237 373	6 248	237 380	-20 264	243 384	19	244 371	-47 270	238 122	238	405	232								
BPAC	229 498	-7 232	232 479	-14 233	231 493	-32 258	233	0 226	228 473	-41 275	236	-1 239	232	0 229	527	248						
	240	8	249	17	247	-9	249	23	251	-23	245	6	250	21	248	0						
CLIM	521 267	234 32	501 271	237 34	512 270	258 12	520 275	230 45	492 273	275 -1	151 273	238 36	402 277	233 45	526 266	248 18	554 272	272 0				
XTRP	509 262	234 28	491 260	237 23	501 255	258 -2	510 258	230 28	485 262	275 -12	147 262	237 24	397 266	232 34	517 264	248 16	540 263	270 <b>-6</b>	542 264	264 0		
HPAC	507 212	233 -20	489 214	237 -21	501 213	258 -45	508 216	230 -13	483 218	273 -53	147 220	237 -16	396 223	232 -8	517 215	248 -32	540 217	270 -52	540 217	263 -45	540 217	217 0
									72-HC	UR FO	RECAST	ERRO	RS (N	1)								
72- JTWC	J1 428	WC 341	RI	ECR	ST	TRA	TO	TL	CY	50	NT	CM	01	CM_	BP	AC	NT	rc <sub>M</sub>	-			
RECR	341 378	0 328	423	387																		
STRA	365 393	37 333	387 413	383	434	390																
TOTL	386 396	53 336	385 419	387	390 430	0 388	440	373														
CY50	360 366	25 345	364 375	-22	368 387	-19 393	373 390	0 377	408	463												
NTCM	433 113	88 326	465 116	82 387	463 116	70 418	466 116	89 378	463 111	0 487	124	353										
отсн	356 299	30 326	355 303	-30 390	356 310	-61 391	360 312	-17 364		-128 440	353 98	0 338	330	346								
BPAC	332 402	7 336	342 399	-47 379	341 414	-49 390	348 417	-16 369		-99	356 119	19 359	346 313	0	442	388						
CLIM	364 420	28 340	384 420	387	384 432	-4 389	389 437	20 373		<del>-</del> 75	375 123	17 355	375 327	34	388 442	0 388	467	409				
CLIN	390	50	399	12	406	17	415	42		-58	399	45	410	64	402	14	409	0	-			

TABLE 4-8.

# COMPARISON OF PORECAST ERRORS (NM) BY TECHNIQUE IN 1982 FOR THE NORTH INDIAN OCEAN

		24-HOUR	RESULT	TS*		48-HOUR	RESUL!	TS*		72-HOUR	RESUL	TS*
TECHNIQUE	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)
JTWC	138	115	93	(37)	368	277	189	(18)	762	887	277	(7)
TOTL	132	120	82	(20)	375	307	181	(7)	883	870	13	(2)
NTCM	319	338	69	(7)	556	578	161	(5)	918	923	80	(3)
CY85	159	142	82	(27)	289	248	136	(13)	426	405	212	(5)
CY50	192	166	129	(27)	433	628	283	(13)	940	1119	420	(5)
OTCM	235	235	66	(13)	522	522	77	(7)	765	798	224	(4)
BPAC	134	133	73	(29)	340	336	127	(12)	853	666	283	(4)
CLIM	218	242	78	(29)	483	523	123	(13)	818	838	51	(4)
XTRP	128	104	75	(28)	326	297	150	(14)				
HPAC	159	167	65	(27)	385	403	112	(13)				

<sup>\*</sup> THIS DATA SET REPRESENTS ALL FORECAST ERRORS FOR EACH TECHNIQUE LISTED AGAINST THE CORRESPONDING BEST TRACK POSITIONS AT 24, 48, AND 72 HOURS.

TABLE 4-9. 1982 ERROR STATISTICS FOR SELECTED OBJECTIVE TECHNIQUES IN THE NORTH INDIAN OCEAN

									24-HO	JR FOR	ECAST	ERROR	S (NM)							
24-	Jī	WC	TO	nl	N7	гсм	CY	85		750		CM		AC	CI	,IM	хт	RP	HP	AC
JTWC	37 138	138 0																		
TOTL	20 132	133 0	20 132	132 0							_	NUMB	70		X-AXIS	7				
NTCM	7 319	201 118	4 268	166 102	7 319	319 0					1	OF CASE		TE	CHNIQUI ERROR	E				
CY85	27 159	153 7	20 164	132 31	6 170	301 -130	27 159	159 0			,	Y-AX CECHNI			ERROR FERENCI	E				
CY50	27 192	153 40	20 179	132 47	6 219	301 -81	27 192	159 33	27 192	·192	<b>)</b> _	ERRO	R	Y	- X	j				
OTCM	13 235	172 63	9 223	128 95	3 280	329 -47	13 235	140 95	13 235	208 27	13 235	235 0								
BPAC	29 134	137 -2	19 129	121 8	5 170	293 -123	26 134	165 -30	26 134	186 -51	13 153	235 -81	29 134	134 0						
CLIM	29 218	137 81	19 198	121 77	5 210	293 -82	26 217	165 53	26 217	186 31	13 235	235 0	29 218	134 84	29 218	218 0				
XTRP	28 128	149 -20	19 126	134 -7	5 195	310 -114	25 130	150 -19	25 130	194 -63	12 135	237 -101	27 120	136 -15	27 120	219 -98	28 128	128 0		
HPAC	27 159	141 18	18 155	122 33	4 185	304 -117	24 165	155 10	24 165	187 -21	12 183	237 -53	27 159	136 23	27 159	219 -59	27 1 <b>59</b>	120 39	27 1 <b>59</b>	15 <b>9</b> 0
									48-HO	JR FOR	ECAST	ERROR	S (NM)							
48-		WC_	T	TL	N'	ГСМ	СУ	85	C	750	01	CM	ВР	AC	CI	.IM	хт	RP	HP	AC
JTWC	18 368	368 0											JTW	- 0	FFICTAL	TTW	FOREC	AST		7
TOTL	7 375	371 4	7 375	375 0									NTCM	A	NALOG (	(TYAN FROPI	78) CAL CYC	LONE		ł
NTCM	5 556	444 112	2 423	404 18	5 <b>556</b>	556 0							CY50	- c	YCLOPS	MODII	FIED 85 FIED 50 CCAL CY	0 MB	PROG	
CY85		397 -107	7 290	375 -84		564 -302	13 289	28 <del>9</del> 0					CLIM	1 - C	LIMATO	LOGY	(STENCE LPOLATI		CLIM	
CY50	13 433	397 36	7 465	375 90	4 568	564 4	13 433	289 144	13 433	433 0							AND CL			J
OTCM	7 522	473 49	3 557	449 108	2 566	705 -138	7 522	238 284	7 522	52 <b>8</b> -5	7 <b>5</b> 22	522 0								
BPAC	12 340	356 -15	6 354	331 23	2 260	494 -233	11 326	300 26	11 326	386 -59	6 417	504 -86	12 340	340 0						
CLIM	13 483	370 113	6 432	331 101		559 -122	12 480	298 181	12 480	406 73	7 549	522 27	12 475	340 135	13 483	483 0				
XTRP	14 326	392 -64	7 355	375 -19	4 419	564 -144	13 324	289 36	13 324	433 -107	7 386	522 -136	12 295	340 -43	13 307	483 -175	14 326	326 0		
HPAC	13 385	370 15	6 370	331 38	3	559 -177	12 381	298 82	12 381	406 -25	7 452	522 -70	12 375	340 36	13 385	483 -97	13 385	307 78	13 385	385 0
									72-H01	JR FOR	ECAST	ERROR	S (NM)				_			-
<u>72-</u>	Jī	WC	TO	TL	N7	гсм	CY	85	C)	/50	Oi	CM	ВР	AC	CI	IM	_			
JTWC	7 762	762 0																		
TOTL		983 -99	883	883 0																
NTCM		943 -23	1 923	870 53	3 918	918 0														
CY85		801 -374		883 -549		918 -552	5 426	426 0												
CY50		801 139		883 335	1105			426 515	5 940	940 0										
OTCM	4 765	746 20	1 899	896 3		916 -30		467 298		884 -118	4 765	765 0								
BPAC		746 107	1 935	896 39	906	916 -9	4 853	467 386		884 -30	853	765 88	853	853 0						
CLIM	818	746 72		896 -57		916 -122		467 351		884 -65	4 818	765 53		853 -34	81 <u>8</u>	818 0	_			

# CHAPTER V - APPLIED TROPICAL CYCLONE RESEARCH SUMMARY

#### 1. JTWC RESEARCH

With the addition of the Southern
Hemisphere to the JTWC area of responsibility,
JTWC's applied research has been substantially reduced. The goal of JTWC's effort in
the research area has been to improve the
timeliness and accuracy of operational
tropical cyclone warnings. During 1982,
JTWC continued to pursue projects of merit
as summarized below:

#### WEIGHTED STEERING PROGRAM

(Allen, R.L: NAVOCEANCOMCEN/JTWC)

A forecast position aid is currently under development which applies an empirically-derived bias to CYCLOPS unmodified steering prognostics. Preliminary results indicate that the 700 mb steering flow (with bias) is the best predictor of meridional motion and a biased average of 850 and 500 mb flow is the best predictor of zonal motion. Initial results from verification studies are promising; further investigation will be conducted during the 1983 tropical cyclone season.

#### JTWC FORECASTER'S HANDBOOK

(Wells, F.H.; Edson, R.E.; Weir, R.C.: NAVOCEANCOMCEN/JTWC)

An ambitious project to accumulate, in one compendium, the practical information necessary for an operational tropical cyclone forecaster in the western Pacific and Indian Ocean regions.

#### COMBINED TROPICAL CYCLONE FORECASTING AIDS

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The project objective was to receive all FNOC tropical cyclone forecasting aids as the result of a single request. Several decoder problems were tested and corrected. Additionally, procedures were developed to automate execution of the Nested Tropical Cyclone Model when a tropical cyclone was in warning status.

#### CLIMATOLOGY (CLIM) FORECAST AID UPDATE

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The CLIM data base was updated through the 1981 tropical cyclone season. In the western North Pacific, five years of new data increased the data base by 16 percent. In the other JTWC regions, the data base was increased by 30 percent with the addition of 10 years of tropical cyclone best track data.

TYAN OBJECTIVE FORECAST AID UPDATE

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The TYAN data base for the Southern Hemisphere and the North Indian Ocean was updated through the 1981 tropical cyclone season, yielding a 30 percent increase in tropical cyclone positions. Procedures were developed to implement the annual update more efficiently. It was also recommended that the western North Pacific model classification of tropical cyclone tracks (RECR, STRA and TOTL) be modified to increase the model's resolution.

#### CYCLOPS OBJECTIVE FORECAST AID UPDATE

(Edson, R.E.: NAVOCEANCOMCEN/JTWC)

In light of the recent development of dynamic tropical cyclone models, CYCLOPS could best serve the forecaster as a "plain" steering aid. This would require:

- a) Removal of the, sometime aberrant, persistance correction.
- b) Changing of the long wave filter to more accurately depict wave numbers.
- c) Testing the size/strength of the tropical cyclone for significance.  $\label{eq:condition} % \begin{array}{c} c = 1 & c \\ 

After testing for effectiveness with the NOGAPS global model, the updated CYCLOPS would be used in conjunction with the dynamic models to indicate expected steering flow at specific levels.

NAVY OPERATIONAL GLOBAL ATMOSPHERIC PREDICTION SYSTEM (NOGAPS) EVALUATION

(Edson, R.E.: NAVOCEANCOMCEN/JTWC)

JTWC participated in evaluating the tropics portion of FNOC Monterey's new global model.

#### 2. NEPRF RESEARCH

TROPICAL CYCLONE STORM SURGE

(Brand, S., NAVENVPREDRSCHFAC; Jarrell, J.D., Compton, J., Science Applications Inc.)

A tropical cyclone storm surge evaluation has been initiated to establish the following:
(a) the needs of the Navy in forecasting tropical cyclone storm surge in the western Pacific; (b) the state of the art of storm surge forecasting techniques; and (c) the best approach to solving the Navy's problems associated with tropical cyclone storm surge.

THE NAVY TWO-WAY INTERACTIVE NESTED TROPICAL CYCLONE MODEL (NTCM)

(Fiorino, M., NAVENVPREDRSCHFAC)

Testing of the NTCM concept continued throughout the 1982 season on two versions of the model - the current Cyber 175 version automatically run using the tropical NVA (global bands) analysis, and an improved model coded for the Cyber 205, (NTCM205) the results of which were clearly superior. The NTCM205 performance was markedly reduced when initialized with NOGAPS analyses compared to the NVA analyses. This discrepancy was attributed to a combination of NOGAPS initialization and data assimulation procedures and the high degree of NTCM sensitivity to the large-scale initial wind fields.

Testing will continue on the one-way influence lateral boundary conditions developed at the National Meteorological Center (NMC) which are designed to force outside-the-domain information into forecasts of a limited area model. Experiments will be conducted on expanding the domain of the NTCM Coarse Grid (the large-scale tropical nodel) to minimize the influence of the channel boundary conditions.

TROPICAL CYCLONE OPTIMUM FORECAST AID

(Tsui, T., NAVENVPREDRSCHFAC)

A comprehensive review of the performance of all JTWC objective tropical cyclone forecast aids has shown that during 19°9-1981 --- if JTWC could have selected the "correct" or the "optimum" forecast aid every time --- the average forecast error could be reduced to 71, 119 159 nm (132, 220, 295 km) for the 24-, 48-, and 72-hour forecasts respectively. The question remains as to which technique is the optimum aid for each situation.

A full-scale test of the optimum-aid concept is now underway. The logical first step of this study is to assess the strength and the characteristics of each objective forecast aid.

TROPICAL CYCLONE OBJECTIVE FORECAST CONFIDENCE AND DISPLAY TECHNIQUE

(Tsui, T., NAVENVPREDRSCHFAC; Nuttal, K., Systems and Applied Sciences Corp.)

In July 1982, forecasters at JTWC could operationally issue a single ARQ command to activate all 11 objective tropical cyclone forecast aids for North Pacific tropical cyclones.

When the system is completed in 1983, a weighted combined tropical cyclone forecast composed from all available objective aids will be issued upon each combined ARQ request. The weights of the combination are deduced from the past (1979-1981) performance of the aids.

#### SPEED OF RECURVING TYPHOONS

(Sadler, J.C. and B. Cheng-Lan University of Hawaii)

Western North Pacific tropical cyclone data were evaluated to determine the characteristics of recurving typhoons, near and after the time of recurvature, during the 10-year period 1970-1979. Three recurving typhoons which produced large forecast errors after recurvature were selected for case studies in search of aids for anticipating the acceleration in speed of movement after recurvature. Analyses of the upper-troposphere poleward of the typhoons revealed a good relation between the future storm speed and the averaged wind speed between 500 and 200 mb, observed, at and 12 hours prior to recurvature, along the future storm track.

SATELLITE BASED TROPICAL CYCLONE INTENSITY FOR CASTS

(Cook, J. and Tsui, T., NAVENVPREDRSHFAC; F. Nicholson, Systems Control Technology)

Software development is currently underway, for implementation on the NAVENVPREDRSCHFAC Satellite-data Processing and Display System (SPADS), to enable study of cloud structures in the newly developed spherical - spiral coordinate system. A Fourier analysis is performed on the cloud structure in spiral space with various harmonics correlated with atmospheric parameters.

Also under investigation is a method of studying the relationship between cyclone intensity and IR radiances/patterns in Lagrangian coordinates. Satellite images of tropical cyclones are rotated and the image parameters are correlated with the cyclone intensity and rate of intensity change.

TROPICAL CYCLONE INTENSITY FORECAST

(Tsui, T. and Cook, J., NAVENVPREDRSCHFAC; Hamilton, H., System and Applied Sciences Corporation)

A study of the western North Pacific tropical cyclone intensity forecast program (MAXWND) showed that two synoptic parameters — the central equivalent potential temperature and the large-scale vertical wind shears — correlate highly with the intensity change. Efforts have been initiated to quantify the relationships between: (1) the equivalent potential temperature and the central sea surface pressure when below 999 mb; and (2) the NOGAPS large-scale vertical wind shear and the tropical cyclone intensity change.

TROPICAL CYCLONE GUST AND SUSTAINED WIND FORECAST AIDS FOR YOKOSUKA AND CUBI POINT

(Jarrell, J.D. and Englebretson, R.E., Science Applications Inc.)

Forecast aids were developed for predicting wind conditions at Yokosuka and Cubi Point when a tropical cyclone passed within 360 nm (667 km). The forecast aids were produced by analyzing a data set comprising the ratios of station wind values to tropical cyclone center wind values. Ratio values were then assigned to the position of the cyclone center. The 360 nm (667 km) radius circle about the station was divided into 71 equal area segments and the values of the mean and maximum ratio within each segment were subjectively analyzed to produce the forecast aids.

TROPICAL CYCLONE STRIKE AND WIND PROBABILITIES

(Brand, S., NAVENVPREDRSCHFAC; Jarrell, J.D., Science Applications Inc.; Chin, D., Systems and Applied Sciences Corp.)

Tropical cyclone strike and wind probability is a method for determining up through 72 hours that a tropical cyclone will affect geographical points of interest to the user. Applications presently being developed, tested and implemented for the western North Pacific, North Indian Ocean, western North Atlantic, and Gulf of Mexico include: strike/wind probabilities and geographical depictions; optimum track ship routing (OTSR) aids; HP-9845/Tactical Environmental Support System (TESS) software for shipboard environmentalists and decison makers; terrain adjusted probabilities; and condition setting aids.

#### 3. PUBLICATIONS

Diercks, J.W., R.C. Weir and M.K. Kopper, 1982: Forecast Verification and Reconnaissance Data for Southern Hemisphere Tropical Cyclones. NAVOCEANCOINCEN/JTWC TECH NOTE: NOCC/ JTWC 82-1.

The Joint Typhoon Warning Center (JTWC) area of responsibility now includes the Southern Hemisphere, from 180° longitude westward to the east coast of Africa. This technical note documents forecast verification and reconnaissance data for those Southern Hemisphere tropical cyclones that occurred between 1 July 1980 and 30 June 1982.

Weir, R.C., 1982: Predicting the Acceleration of Northward-moving Tropical Cyclones Using Upper-Tropospheric Winds. NAVOCEANCOMCEN/JTWC TECH NOTE: NOCC/ JTWC 82-2.

Inconsistent forecasting of the acceleration of northward-moving tropical cyclones entering the domain of the mid-latitude westerlies has been a long-standing weakness in tropical cyclone forecasting. The tracks of tropical cyclones traversing a relative high-density data area of the western North Pacific have been analyzed to verify the acceleration phenomenon, and to correlate the movement with features of the uppertropospi. ric wind field. The resultant forecast tachnique is described and the results obtained with its use during the 1982 tropical cyclone season in the western North Pacific are presented.

# ANNEX A TROPICAL CYCLONE DATA

# 1. WESTERN NORTH PACIFIC CYCLONE DATA

TROPICAL STORM MAMIE BEST TRACK DATA

	BEST TRACK	( UARI	ERRORS	24	HOUR F	ERRO	IRS	48	HOUR F	DRECAST ERRORS		72 H	IOUR F	ERROR	
MD/DA/HR	POSIT WIND	POSIT WINI	DST WIND	POSIT	WIND	DST	WIND	POSIT	UIND	DST L	IND I	POSIT	UIND	DST	WIND
831486Z	7.1 153.0 15	6.8 6.8 6.	-6, 8.	8.6 6	.0 0.	-0.	0.	0.0 0.	0 0.	-8.	9. 8.	0.6	●.	-€.	ø.
031412Z	7.4 151.5 20	8.8 8.8 8.	-8. 0.	8.8 8.	.0 0.	-0.	8.	9.8 8.	0 0.	-0.	8. 8.	0 0.6		-8.	ø.
0314182	7.7 150.1 25	0.6 0.6 0.	-0. 0.	0.0 0	.0 0.	-0.	ø.	8.8 8.	0 0.	-0.	0. 0.	0 0.6		-8.	8.
031500Z	7.8 149.B 25	8.8 8.8 8.	-8. 8.	0.0 0	.0 0.	-0.	ø.	0.0 0.		-8.	A. A	0 8.6		-0.	ā.
0315062	7.7 148.3 38	0.0 6.0 8.	-0. 0.	8.0 A	.0 0.	-0.	ø.	8.8 8.		-0.	0. 0			-0.	ā.
031512Z	7.6 147.8 35	8.8 8.8 8.	-0. 0.		0.	-0.	ø.	0.0 0.		-0.	8. 6			-8.	ě.
031510Z	7.5 147.2 40	0.0 0.0 0.	-8. 8.		.0 0.	-0.	ø.	0.0 0.		-B.	8. 6			-8.	e.
031600Z	7.3 146.4 45	0.0 0.0 0.	-8. 0.	8.8 8		-0.	ě.	8.0 B.		-0.	8. 8.			-8.	ø.
031606Z	7.3 145.5 50	7.8 145.4 50.	19. 8.	5.8 141		112.	18.	6.8 137.		154.	10. 8			327.	5.
831612Z	7.3 144.5 58	7.2 144.8 58.	19. 0.	7.2 141		80.	10.	8.1 137.		214.	10. 10			584.	10.
0316182	7.3 143.4 55	7.6 143.3 58.	195.	7.9 139		42.	10.	10.1 135.		231.	10. 13.	6 132.6		585.	20.
031700Z	7.4 142.4 55	7.3 142.3 55.	8. O.	8.2 138		74.	5.	9.8 134.							25.
031706Z										278.					
				9.2 136		97.	18.	10.3 132.		289.	10. 11.			446.	25.
031712Z	7.8 148.8 55	7.9 140.0 55.	6. 0.	9.9 135		143.	5.	11.2 131.		371.	10. 11.			463.	25.
931719Z	7.9 138.6 55	8.8 138.3 55.	57. 0.	11.1 132		179.	5.	12.1 128.			15. 12.			332.	15.
031000Z	7.9 137.0 55	7.9 136.7 58.	185.	9.1 131		85.	0.	9.6 126.		220.		1 122.2		202.	5.
031006Z	8.1 135.5 55	0.0 135.3 55.	13. 0.	9.4 130		134.	0.	9.6 125.		229.	18. 8			194.	5.
031012Z	8.2 133.9 55	8.3 134.0 55.	9. 0.	9.4 128		154.	5.	9.5 124.		241.	15. 8.			187.	10.
<b>031918</b> Z	8.2 132.2 55	0.6 132.2 55.	24. 0.	9.5 127		195.	5.	9.2 123.		214.	5. 8			186.	10.
0319 <b>00</b> Z	8.2 138.1 60	8.1 129.9 55.	135.	7.6 122		48.	-5.	8.3 117.	1 35.	117.	-5. 11.	6 113.1	40.	159.	5.
8319 <b>8</b> 6Z	8.2 128.1 60	8.1 127.7 55.	255.	9.2 120	.5 35.	68.	-5.	9.7 116.	0 40.	125.	5. 12.	3 112.7	45.	169.	10.
0319122	0.4 126.0 55	0.2 126.7 55.	43. 0.	8.2 122	.0 35.	141.	8.	8.5 117.	2 48.	79.	5. 9.	5 111.6	45.	178.	15.
<b>0</b> 319182	8.4 124.2 45	8.2 124.8 48.	305.	8.4 119	.7 40.	36.	5.	9.8 114.	9 45.	115.	10. 9.	7 110.6	45.	191.	15.
032000Z	8.4 122.8 40	8.5 122.2 48.	36. 0.	9.3 115	.7 45.	184.	5.	18.2 118.	1 50.	331.	15. 11.	6 186.3	35.	394.	5.
<b>032006</b> Z	8.5 121.6 40	0.6 120.6 40.	60. 0.	9.5 114	.7 45.	201.	10.	10.0 110.	3 50.	273.	15. 10.	4 196.7	45.	352.	15.
032012Z	8.8 120.5 35	0.5 119.9 40.	40. 5.	9.4 115	.2 45.	132.	10.	18.4 110.	4 45.	227.	15. 12.	9 107.2	25.	282.	-5.
032018Z	9.0 119.8 35	0.5 118.8 35.	66. 0.	10.1 114	.7 25.	106.	-18.	11.5 111.	8 25.	187.	-5. 13.	2 118.2	20.	88.	-18.
032100Z	9.3 118.8 48	9.2 118.0 35.	485.	10.6 114		90.	~5.	11.8 111.		95.	-5. 13.			116.	-5.
032106Z	9.5 118.1 35	9.5 118.3 35.	12. 0.	10.8 115		25.	-5.	11.8 112.		12.	-5. 13.			73.	-5.
032112Z	9.8 117.4 35	10.0 117.0 30.	275.	11.5 113		35.	-5.	12.8 111.		61.	-5. 14.			134.	-5.
	10.1 116.5 35	18.2 116.2 38.	195.	11.7 112		58.	-5.	13.5 110.		96.		1 109.6		238.	ã.
	10.3 115.7 35	10.7 115.2 30.	395.	12.5 112		80.	-5.	14.2 110.		129.	-5. <b>0</b> .			-8.	ě.
	10.5 114.9 35	18.5 114.0 30.	65.	12.2 112		30.	-5.	0.0 6.		-8.	0. 0.			-0.	ø.
	11.8 114.2 38	11.1 113.6 30.	36. 0.	13.7 110.		147.	-5. -5.	0.0 0.		-0. -0.	0. D.			-0.	ø.
	11.3 113.6 30	11.3 113.2 25.	245.	12.9 110.		51.	-5. -5.	0.0 0.		-e.	8. 8.			-0.	Ð.
	11.6 113.0 30	11.7 113.2 25.	135.	13.0 111.		84.	-5. -5.			-0. -0.	0. 0.			-0. -0.	8.
								0.8 8.							
	11.0 112.5 30	11.7 112.1 30.	24. 8.	12.5 189.		50.	0.	0.0 0.		-ø.	0. 0.			-0.	6.
	11.9 111.9 30	11.2 111.5 30.	48. 0.			54.	-5.	0.0 6.		-0.	0. 0.			-0.	6.
	12.1 111.2 30	12.0 111.3 30.	0. 0.	12.5 108.		34.	5.	6.6 6.		-0.	0. 8.		e.	-0.	0.
	12.1 110.7 25	12.2 110.8 30.	e. 5.	12.4 108.		30.	5.		Ð Ð.	-0.	0. 0.		e.	-0.	0.
	12.2 110.1 25	12.1 110.0 25.	8. 0.		.0 0.	-0.	0.	0.0 0.		-0.	0. 0.	0.6		-0.	ø.
	12.2 169.1 25	12.1 109.0 25.	8. Ø <i>.</i>	0.0 0.	.0 0.	~0.	0.	0.0 B.		-0.	0. 0.		9.	-0.	ø.
	12.2 108.3 20	12.1 108.2 28.	8. 0.		.0 0.	-0.	0.	0.0 B.		-0.	0. 0.		0.	-0.	ø.
032500Z	12.1 107.8 10	0.0 0.0 0.	-0. 0.	0.0 0.	,0 0.	-0.	0.	8.0 0.	0 0.	-8.	0. 0.	0 0.6	ь.	-8.	ø.

	ALL	FORECAS	T5		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72~HR
AVG FORECAST POSIT ERROR	25.	93.	188.	276.	0.	e.	₽.	8.
AVG RIGHT ANGLE ERROR	14.	48.	86.	115.	8.	0.	₿.	0.
AVG INTENSITY MAGNITUDE ERROR	2.	5.	9.	11.	0.	0.	0.	0.
AVG INTENSITY BIAS	-1.	١.	6.	8.	8.	8.	8.	8.
NUMBER OF FORECASTS	35	32	24	23	•		Ð	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2733. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

11. KNOTS

TROPICAL STORM MAMIE
FIX POSITIONS FOR CYCLONE NO. 1

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
+ 1	140600	6.9N 154.5E	PEN 5	T8.5/8.5	INIT OBS	PGTU
2	150006	7.8N 148.7E	PCN 5	Te.5/e.5 /Se.e/18HRS		PGTU
3	150300	8.1N 148.4E	PCN 5			PGTU
4	151721	8.IN 147.8E	PCN 5			PGTU
5	160000	7.0N 146.1E	PCN 5	T1.8/1.8 /D8.5/24#RS	ULCC FIX	PGTU

45 467 489 59 51 52 53 55 56 57 58 61 62 63	230300 230625 230900 231200 231909 231910 232100 240300 240600	7.4N 145.9E 7.3N 145.7E 7.3N 145.7E 7.3N 145.7E 7.3N 145.7E 7.7N 143.6E 7.7N 143.6E 7.5N 142.4E 7.5N 142.6E 7.5N 142.6E 7.5N 142.6E 8.5N 130.6E 8.2N 130.6E 8.2N 130.6E 8.2N 130.6E 8.2N 130.6E 8.2N 130.6E 8.2N 120.6E 8.3N 127.8E 8.3N 127.8E 8.3N 127.8E 8.3N 127.8E 8.3N 127.8E 8.3N 121.6E 8.7N 124.6E 8.7N 1	PCM 5 PCM 6	T3. <b>0</b> /3.	5 /D666-/D666-/D666-/D666-/D666-/D6666-/D6666-/D666-/D6666-/D6666-/D6666-/D6666-/D6666-/D6666-/D6666-/D6666-/D6666	.5/24HR .5/24HR .5/24HR .6/24HR	5 5 5 5 5 5 5		EXP L	FIX  OBS FIX E  OCC  LCC  LCC  CONTI	ONTINU NASED O	C MOT APPAREN' ITY N CONTINUITY		CTULUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUU			
	240900 241200		PCN 5										F				
						1	AIRCR	AFT F	IXES								
FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	786119 HGT M		MAX-SFC VEL/BRG							EYE O		EYE TE OUT/ IN/		MSN NO.
1 2 3 4 5 6 7	160359 161921 162131 172217 180633 180847 182215	7.2N 145.8E 7.2N 143.1E 7.2N 142.8E 7.9N 137.2E 8.1N 135.3E 8.2N 134.3E 8.1H 138.4E	1580FT 700HB 700HB 700HB 700HB 700HB 700HB	3034 3034 3062 3086 3066	99 <b>0</b> 994 994 991	58 288 45 388 58 348 45 358 65 338 55 848	10 10 20 10	120 120 050 000 120	55 200 45 050 55 360 36 310 53 320 48 350 54 040	40 18 60 60 8	10 4 10 5 10 3 3 10 8 2 9 1 7 4	ELL IPTICAL ELL IPTICAL	15 10		+24 +25 +12 +16 +12 +15 +12 +16 +11 +17 +12 +14	+10 +10 + 8	1 2 2 4 5 5
						ı	RADAR	FIXE	5								
FIX NO.	TIME (Z)	FIX POSITION	RADAR (	CCRY	EYE SHAPE	D1		RADOB AS <b>UAR</b>	-CODE TDDFF			COMENTS			RADAR POSITION	SI1	
1 2 3	191800 192200 200000	8.5N 124.3E 8.5N 123.4E 8.7N 123.3E	LAND					25551	53220 52010 52910						10.3N 124. 10.3N 124. 10.3N 124.	BE 986	546

MOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TYPHOON NELSON BEST TRACK DATA

	BEST TRACK	WARN ING ERRORS	24 HOUR FORECAST ERROR		72 HOUR FORECAST ERRORS
MO/DA/HR		WIND DST WIND	POSIT WIND DST U	IND POSIT WIND DST WIND	PUSIT WIND DST WIND
031806Z	3.8 160.7 25 0.8 8.8	0. 0. 0.	0.0 0. <b>0 00</b> .	0. 0.0 0.0 00. 0.	8.0 0.0 8. <del>-</del> 0. <b>6.</b>
<b>031812</b> Z	4.5 158.8 25 8.8 8.6		0.0 0.0 00.	0. 0.0 0.0 00. 0.	0.0 <i>0.</i> 0 00. 0.
<b>03</b> 1010Z	4.9 157.1 30 6.0 8.0		0.0 0.0 00.	0. 8.0 0.0 00. 6.	0.0 0.0 00. O.
031900Z	5.5 155.5 40 5.3 155.5		7.6 149.0 50. 42.	0. 8.2 144.8 68. 59. 10.	8.5 139 <i>.</i> 8 70. 21. 5.
031906Z	5.9 153.9 50 5.9 154.6		8.5 149.0 60. 98.	10. 9.2 143.8 65. 91. 10.	9.0 138.2 75. 30. 15.
0319122	6.4 152.4 55 6.3 152.2		8.4 146.6 6U. 103.	10. 8.9 141.8 70. 89. 10.	8.6 136.1 75. 12. 15.
031918Z	6.7 151.0 55 7.0 150.4		9.7 144.8 60. 131.	10. 8.8 140.0 70. 88. 5.	8.5 134,4 75. 38. 15.
832888Z 832886Z	6.9 149.9 50 7.6 149.5 6.9 148.7 50 7.3 148.5		9.6 143.9 55. 116.	5. 9.2 139.2 68. 575.	8.3 133.6 65. 48. 8.
0320062 032012Z	6.9 148.7 50 7.3 148.5 7.0 147.6 50 7.0 147.6		0.5 144.2 50. 44. 8.0 143.1 55. 13.	-5. 9.2 140.0 55. 1415. -5. 8.7 138.8 58. 16010.	9.6 135.0 60. 15610.
0320122 032018Z	7.3 146.5 50 7.2 146.2			-5. 8.7 139.8 50. 16010. 10. 8.8 135.3 50. 3210.	0.7 133.7 50. 14120. 0.5 130.5 45. 6025.
032100Z	7.5 145.5 50 7.6 146.4		8.5 141.2 68. 102.	-5. B.9 136.1 60, 155, -5.	0.5 130.5 45. 6025. 0.5 130.2 55. 0320.
032106Z	7.8 144.4 55 7.9 144.3		8.8 139.8 65. 125.	5. 9.0 134.0 60, 14310.	B.7 129.8 60. 6728.
8321122	7.9 142.9 60 7.9 143.4		9.0 139.0 68. 172.	0. 9.3 134.0 60. 15410.	9.2 128.3 55. 3638.
<b>032</b> 1182	8.1 141.3 65 B.0 142.0		9.1 137.0 70. 130.	10. 9.8 131.4 65. 625.	10.4 126.2 55. 9435.
032200Z	8.3 139.5 65 8.2 139.9		9.2 134.1 75. 36.	10. 10.0 128.6 70. B55.	11.7 123.8 55. 22248.
832286Z	9.6 137.7 68 8.5 138.1		18.0 132.0 75. 54.	5. 11.6 126.0 70. 19710.	11.8 122.2 55. 28545.
832212Z	8.8 136.1 60 8.8 136.2		10.8 130.6 75. 102.	5. 11.6 125.8 65, 17828.	11.6 121.8 50. 26755.
0322182	9.0 134.8 60 9.1 134.2			-5. 11.6 124.2 55. 23835.	11.5 120.0 45. 33155.
032 <i>3</i> 00Z	9.1 133.5 65 9.2 133.5		10.3 129.3 90. 38.	15. 10.9 125.2 65. 12730.	18.9 121.1 58. 22145.
032306Z	9.2 132.4 70 9.3 132.2	90. 13. 10.	10.3 127.3 90. 94.	10. 10.8 123.3 50. 20950.	11.2 119.4 50. 27435.
<b>032312</b> Z	9.3 131.4 70 9.4 131.1	80. 19. 10.	10.6 125.9 75. 136	10. 10.2 121.5 50. 27055.	11.2 117,4 55. 35925.
<b>0</b> 323162	9.5 130.4 70 9.5 129.9		10.0 125.1 65. 154		11.9 116.8 55. 35920.
032400Z	9.7 129.5 75 9.5 129.5		9.9 126.2 65. 60. ~		11.5 119.2 50. 17715.
<b>032406</b> Z	9.8 128.8 88 9.6 128.8		9.9 125.8 70. 64		11.2 119.2 50. 12910.
032412Z	9.8 128.2 85 9.6 128.2			20. 9.7 122.7 60. 91. 20.	10.5 118.9 65. 122. 10.
032418Z	9.9 127.7 98 9.7 127.4			25. 9.9 121.8 60. 11615.	10.9 118.1 65. 106. 20.
032500Z	10.1 127.2 95 9.8 127.6		18.2 124.5 78. 19. ~		11.9 119.0 65. 42. 25.
032506Z	10.3 126.8 100 10.2 126.9		11.0 125.6 90. 99.	5. 11.7 123.2 60. 112. 0.	12.3 121.0 55. 191. 10.
032512Z 032518Z	10.5 126.2 105 10.6 126.2 10.4 125.5 100 10.7 125.6			20. 12.7 121.4 55. 76. 0. 15. 12.8 120.7 55. 85. 10.	13.8 118.6 55. 84. 5.
032688Z	10.4 125.5 100 10.7 125.6 10.3 124.0 95 10.5 124.8		11.9 123.4 60. 30	15. 12.8 120.7 55. 85. 10. 0. 12.6 118.8 65. 21. 25.	12.9 117.4 60. 67. 10. 13.5 115.0 60. 74. 15.
832686Z	10.5 124.0 85 10.7 124.2		11.9 121.6 65. 19.	5. 12.8 110.0 65. 13. 20.	13.7 114.2 60. 100. 15.
032612Z	11.0 123.5 90 10.8 123.0		11.8 119.6 68. 47.	5. 12.9 1,5.6 65. 97. 15.	13.9 111.6 65. 222. 25.
632618Z	11.5 122.9 75 11.2 122.2			10. 12.9 115.3 65. 90. 15.	14.0 111.4 60. 204. 20.
6327662	11.7 122.2 65 11.5 121.3			20. 14.0 112.7 70. 198. 25.	14.2 108.0 30. 3795.
0327862	11.8 121.3 60 11.5 120.0			25. 13.8 112.0 75. 223. 30.	13.8 108.0 30. 361. 0.
<b>03</b> 2712Z	11.9 128.4 55 11.8 128.2			20. 14.2 113.4 75, 116, 35.	14.4 109.2 60. 285. 30.
<b>032718</b> Z	12.0 119.5 45 12.0 119.7	55. 12. 10.	13.2 116.9 65. 35.	15. 14.2 113.0 75. 111. 35.	14.4 108.8 50. 294. 28.
<b>032000</b> 2	12.4 118.5 48 12.3 118.6		13.8 115.7 50. 29.	5. 15.2 112.7 58. 130. 15.	17.8 110.8 45. 336. 15.
<b>032006</b> Z	12.9 117.8 45 12.9 117.5		15.0 113.7 45. 129.	0. 20.0 110.6 35. 425. 5.	0.0 0.0 0. <b>-0.</b> 0.
032912Z	13.3 117.2 50 13.3 117.2			10. 19.6 118.2 48. 426. 18.	0.0 0.0 0. <b>-0. 0.</b>
<b>032818</b> Z	13.7 116.6 50 14.0 116.4			15. 20.9 109.9 30. 511. 0.	0.0 0.0 00. 0.
032900Z	14.1 116.1 45 15.8 115.4			15. 23.2 110.9 25. 6375.	0.0 0.0 00. 0.
032906Z	14.3 115.8 45 14.7 115.7			15. 21.4 113.7 35. 510. 5.	0.0 0.0 08. 0.
032912Z	14.2 115.4 40 15.1 115.3			15. 22.2 113.8 30. 546. 0.	0.0 0.0 06. 0.
032918Z 033800Z	14.0 114.9 40 13.8 114.9 13.9 114.5 35 13.7 114.6		12.2 112.1 30. 111.	0. 11.1 107.5 20. 37210.	0.0 0.0 00. 0.
033000Z 033006Z	13.9 114.5 35 13.7 114.6 13.8 114.2 30 13.8 114.1		12.3 111.7 30. 117.	0. 0.0 0.0 00. 0.	0.0 0.0 06. 0.
833812Z	13.5 114.0 30 13.7 113.7		13.6 112.2 30. 113. 13.2 111.8 20. 129	0. 6.0 0.0 00. 0. 10. 5.0 0.0 00. 0.	0.0 0.0 00. 0. 8.6 0.0 06. 6.
0330122 033018Z	13.2 113.7 30 13.1 113.7		0.0 0.8 00.	8. 6.8 8.8 80. 8.	8.8
033100Z	12.9 113.6 30 12.4 113.8			-5. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
<b>0331062</b>	12.9 114.0 30 12.9 113.2			-5. 0.0 0.0 80. 0.	0.0 0.0 00. 0.
633112Z	13.1 114.0 30 12.4 113.8		0.0 0.0 00.	6. 8.6 8.8 BD. O.	0.0 0.0 00. 0.
033118Z	13.1 113.5 30 12.4 113.8		0.0 0.0 00.	0. 0.0 0.0 00. 0.	6.8 <b>6.8 66.</b> 6.
848 188Z	13.1 113.1 25 0.0 0.0		8.0 0.0 D0.	0. 0.0 0.0 00. 0.	6.0 0.8 00. 0.
040106Z	13.1 112.6 25 0.0 0.0		0.0 0.0 DD.	0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	LIRNG	24-HR	48-HR	72-HR	LIRNG	24-H釈	48-HR	72-HR		
AVG FORECAST POSIT ERROR	24.	95.	198.	178.	23.	85.	122.	152.		
AVG RIGHT ANGLE ERROR	13.	57.	114.	72.	13.	47.	58.	49.		
AVG INTENSITY MAGNITUDE ERROR	5.	11.	17.	21.	5.	12.	19.	22.		
AVG INTENSITY BIAS	1.	1.	-4.	-6.	1.	8.	-5.	<b>-9</b> .		
NUMBER OF FORECASTS	53	49	44	37	45	41	37	33		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 3863. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

# TYPHOON NELSON FIX POSITIONS FOR CYCLONE NO. 2

FIX NC.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	188486	3.7N 168.9E		T1.5/1.5	INIT OBS	PG TW
2	180900	4.0N 160.1E 4.7N 157.7E	PCN 5			PGTW PGTW
	190000	5.3N 155.5E		T2.5/2.5 /DI.R/25HRS		PGTW
5	190348 190600	5.8N 154.3E 5.8N 153.9E	PCN 4 PCN 5			PGTU PGTU
7	190900	6.0H 152.6E	PCN 5			PGTW
8	191633	6.7N 158.7E	PCN 6			PGTU
9 18	192188 288888	6.9N 150.0E 7.2N 149.6E	PCN 5 PCN 5	T3.8/3.8 /D8.5/24HRS		PGTW PGTW
11	200300	7.2N 149.3E	PCN 5			PGTW
12 13	200518 201200	7.5N 149.1E 7.6N 147.4E	PCN 5 PCN 5.			PGTW PGTW
14	201621	7.2N 146.1E	PCN 5			PGTU
15 16	261868 262186	7.2H 146.8E 7.2H 145.7E	PCN 5			PGTW PGTW
17	210000	7.3N 145.2E	PCN 5	T3.5/3.5 /D8.5/244RS		PGT <b>U</b>
18 19	210300 210506	7.5N 145.8E 8.2N 144.4E	PCN 5			FGTU PGTU
20	218688	8.5N 144.0E	PCN 5			PGTU
21 22	211200 211600	7.9N 143.0E 8.0N 141.9E	PCN 5			PGTW PGTW
23	211751	8.8N 141.7E	PCN 6			PG TW
24 25	220006 220300	9.3N 139.3E 8.5N 139.0E	PCN 5	T4.8/4.8 /D8.5/24HRS		PGTU PGTU
26	228454	8.5N 138.1E	PCH 5			PGTM
27 28	220600 221200	8.5N 138.0E 8.6N 135.9E	PCN 3 PCN 5			PGTU PGTU
29	221600	8.3N 134.7E	PCN 5			PGTW
38 31	221748 238888	9.8M 134.2E 8.8N 133.6E	PCN 5	T4.8/4.8 /S8.8/24HRS		PGTW PGTW
32	238688	9.3N 132.3E	PCN 5	1410-410-1010-2-110		PGTU
33 34	2312 <b>68</b> 231728	9.4N 131.4E 9.5N 130.1E	PCN 5 PCN 6		BASED ON EXTRAP	PGTW PGTW
35	231728	9.3N 129.9E	PCN 6			RODN
36 37	232100 240000	9.6N 129.6E 9.5N 129.5E	PCN 5 PCN 3	T4.5/4.5-/D8.5/24#RS		PGTU PGTU
38	248388	9.6N 129.2E	PCN 1	74.0	EYE DIA 5NM	PGTU
39 46	240613 241200	9.8N 128.7E 9.7N 128.2E	PCN 1 PCN 1		EYE DIA SNM	PGTW PGTW
41	241600	9.6N 127.8E	PCN 1			PGTU
42 43	2418 <b>66</b> 2421 <b>60</b>	9.7N 127.6E 9.9N 127.4E	PCN I PCN I			PGTW PSTW
44	258888	10.0N 127.3E	PCN 1	T5.8/5.8-/D0.5/24HRS	EYE DIA 18NM	PGTW
45 46	250306 250601	10.1N 127.1E 10.1N 126.8E	PCN 1 PCN 1			PGTW PGTW
47	258988	10.3N 126.7E	PCN 1			PGTW
46 49	2512 <b>68</b> 2512 <b>68</b>	11.1N 123.0E 10.3N 126.3E	PCN 5 PCN 1			PGTW PGTW
50	251988	18.4H 125.5E	PCH 1			PGTW
51 52	252100 260000	18.4M 125.1E 18.3M 124.5E	PCN 1 PCN 3	T4.5/5.0 /W0.5/24HRS		PGTU PGTU
53	268388	18.4N 124.4E	PCN 1			PGTW PGTW
54 55	260600 260900	18.4N 124.1E 18.7N 123.5E	PCN 5 PCN 5			PGTU
56 57	2616 <b>88</b> 2618 <b>88</b>	11.1N 122.7E	PCN 5			PGTU PGTU
56	262188	11.1N 122.3E 11.4N 121.7E	PCN 5			PGTU
* 59 * 68	27 <b>0000</b> 27 <b>0300</b>	11.3N 121.1E 11.6N 128.7E	PCN 5	T3.5/4.0 /W1.0/24HRS		PGTU PGTU
61	278688	11.1N 120.6E	PCN 5			PGTW
	278719 278988	11.1N 120.0E 11.2N 120.5E	PCN 5 PCN 5			RPHK PGTU
64	271288	11.7N 120.3E	PCH 5			PGTU
65 66	2716 <b>88</b> 271822	11.7N 119.5E 11.9N 119.3E	PCN 5 PCN 5		BASED ON EXTRAP	PGTU PGTU
67	272188	12.3N 118.9E	PCN 5		DAGES ON EXTRA	PGTU
68 69	290000 290300	12.5N 118.3E 12.6N 117.9E	PCN 5	T2.5/3.8 /WI.8/27HRS		PGTW PGTW
78	200600	12.8N 117.3E	PCN 5			PGTU
71 72	200706 200900	13.0N 117.5E 13.1N 117.3E	PCN 5 PCN 5	T3.5/3.5	INIT OBS	RODN PGTU
73	281288	13.5N 116.9E	PCN 5			PGTW
74 75	2816 <b>88</b> 2818 <b>88</b>	13.8N 116.4E 14.1N 116.2E	PCN 5			MIDA Wida
76	292166	14.7N 115.9E	PCN 5			PGTW
* 77 78	290000 290300	15.2N 115.8E 15.2N 116.1E	PCN 5	T2.5/2.5 /S8.8/24HRS	ULCC FIX	PGTW PGTU
79	298688	14.6H 116.6E	PCH 5		****	PGTW
<b>86</b>	290655 290900	14.2N 115.5E 14.3N 115.9E	PCN 3 PCN 5	13.0/3.0	INIT OBS EXP LLCC	RPMK PGTU
82	291288	14.3H 115.4E	PCN 5			PGTU
83	291686	13.9H 115.1E	PCN 3		EXP LLCC	PCTU

84	291888	13.7N 115.8E	PCN 3			PC FW
85	291938	13.9N 115.2E	PCN 3		EXP I.LCC	RPMK
86	291948	13.9N 115.0E	PCN 3		EXP LLCC	ROPH
87	292100	13.7N 114.8E	PCN 3		EXP LLCC	PG TW
69	300000	14. IN 114.7E	PCN 3			PGTW
89	300300	14.8N 114.5E	PCN 3	T1.0/2.0 /W0.5/24HRS		PGTU
90	300600	13.9N 114.2E	PCN 3			PG I W
91	300643	13.8N 114.0E	PCN 3	T2.0/3.0 /W1.0/24HRS		RFIIK
92	300900	13.5N 113.9€	PCN 3			PG fish
93	301600	13.1N 113.8E	PCN 3		EXP LLCC	PGT⊌
94	301800	13.2N 114.1E	PCN 3		EXP LLCC	PG I'U
95	302100	13.1N 114.0E	PCH 3			PG FU
96	310000	13.0N 113.6E	PCN 3			PSTU
97	310300	13.8N 113.4E	PCN 5			PSTW
98	310630	12.8N 113.9E	PCN 3	T1.0/1.0 /S0.0/27HRS		PGTU
99	310631	12.7H 113.9E	PCN 3	T1.0/2.0 /W1.0/24HRS		RITK
100	311600	12.7N 113.9E	PCN 5		EXP LLCC	PGTU
101	311800	13.1N 113.7E	PCN 5			PGTU
182	311916	13.3N 113.3E	PCN 5			RODH
103	312100	13.3N 113.5E	PCH 5			PGTW
184	010000	13.2N 113.1E	PCN 3			PGTW
105	010600	13.0N 112.6E	PCN 3			PGTIJ

#### AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX Position	FLT LVI.	706MB HGT	OBS MSLP		-SFC- ⁄BRG/				-LVL- ⁄BRG/		HAV.		EYE SHAPE	EYE OF IEN-	CYE TEMP (C) OUT/ IN/ IMP/SST	MSN NO.
1	198615	5.9N 153.8E	700HB	3029		50	870	20	210	66	100	30	10	5			+12 +10 +10	i
2	191982	6.8N 150.8E	7 <b>96118</b>	3031	996				989	47	010	18	7	3	CIRCULAR	20	+ 9 +14 + 9	2
3	192224	6.8N 158.1E	700MB	3032	992		130	8	248		130	11	5	4	CIRCULAR	15	111 +14 + 9	2
4	200637	6.BN 148.6E	7 <b>90</b> MB	3052	994	40	030	10	968	46	330	В	5	1				3
5	200030	6.9N 140.2E	7 <b>99119</b>	3073		30	150	5	250		140	6	2	1	CIRCULAR	5	+12 +15 +12	3
6	201917	7.2N 146.3E	7001B	3084					969		360	30	10					4
7	202145	7.5N 145.9E	700MB	3020	994		010	50	989		320	20	8	10	CIRCULAR	18	+11 +14 +10	4
8	210803	7.8N 144.1E	7 <b>86</b> MB	3033			360	6	979		320	29	10	4			+11 +14	5
9	212113	0.1N 140.5E	7 <b>90</b> MB	2876	973		360	8	140		369	8	2	5	CIRCULAR	15	+15 +17 +10	6
10	220631	8.4N 137.9E	7 <b>00</b> 118	2970	986		060	30	986		310	30	5	4	CIRCULAR	20	+14 +14 + 8	7
11	220909	8.7N 137.BE	7 <b>00MB</b>	2960	986	49	180	15	220		170	10	5	4	CIRCULAR	20	+11 +14 + 8	?
12	221918	9.BN 134.2E	7 <b>00</b> MB	2973					080		010	19	10	5	CIRCULAR	15		8
13	222211	9.0N 134.1E	7 <b>00H</b> 0	2988	985		360	10	160		270	В	10	3	C TRCULAR	12	+11 +20 + 9	8
14	230645	9.2N 132.2E	7 <b>0011</b> 8	2964	984	70	360	30	666		340	30	7	5	LIRCULAR	10	+13 +16 +11	9
15	230835	9.1N 131.8E	79 <b>9</b> 119	2 <del>96</del> 6					200		138	30	10	7	CIRCULAR	12	+18 +12 +12	9
16	232210	9.5N 129.9E	700MB	2913	979				0.40		300	10	5	6	CIRCULAR	15	+13 +14 +12	16
17	240635	9.8N 128.8E	7 <b>00M</b>	2696			220	5	310		240	20	10	2	C IRCULAR	15	+14 +16 +13	11
18	240830	9.8N 128.5E	700MB	2630	952	100	180	7	180		360	7	10	2	CIRCULAR	10	+14 +15 +11	11
19	250742	10.4N 126.9E	700MB	2510	934				969		360	10	5	5	CIRCULAR	8	+11 +17 +11	13
20	250920	10.3N 126.4E	700MB	2548	938				100	113		11	4	4	C IRCULAR	7	+14 +14	13
21	270934	11.8N 120.9E	700MB	3052		50	166	28	170		140	26	3	_			+11 +15 + 6	16
22	272002	12.2N 118.9E	700MB	3057					150		020	35	3	4				17
23	272259	12.3N 118.7E	700MB	3073	998				640		310	25	3	4	C IRCULAR	15	+10 +14 + 6	17
24	280705	12.8N 117.6E	700HB	3033			270	25	210		150	13	5	3	C IRCUL AR	20	+12 +14 +18	18
25	261003	13.2N 117.4E	70UMB	3005		50	360	15	240	60	150	11	5	3	CIRCULAR	17	+13 +14 +12	18

#### RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE D I AM	RADOB-CODE ASWAR TDDFF	CONTENTS	RADAR POSITION	SITE WMO NO.
1 2 3 4 5 6 7 8 9 18	242398 259299 259399 259699 251199 251599 251799 251899 252999 269999	18.2N 126.8E 10.3N 126.7E 10.3N 126.7E 10.3N 126.4E 10.7N 125.4E 10.9N 125.8E 10.9N 125.6E 10.7N 125.4E 18.5N 125.4E	LAND LAND LAND				65582 40000 50612 52905 50642 40000 50612 42910 18302 52910 14492 52909 10322 52700 14322 52700 14211 52608 14114 52500 5///1 42509		10.3h 124.0E 10.3h 124.0E	986 46 986 46 986 46 986 46 986 46 986 46 986 46 986 46 986 46 986 46

MOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TYPHOON ODESSA BEST TRACK DATA

	BEST TRAC	UARNING ERROPS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MD/DA/HR	POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
032806Z	3.5 156.6 20	0.8 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
832812Z	4.3 156.1 25	8.8 8.8 88. 8.	0.0 0.0 00. 0.	0.0 0.0 0. A. O.	8,8 8,8 8, -0, 8.
032818Z	5.1 155.9 30	0.0 0.0 00. 0.	0.0 0.0 09. 0.	0.0 0.0 00. 0	0.0 0.0 00. 0.
0329 <del>00</del> Z	6.0 155.8 30	8.0 0.0 00. 0.	9.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
032906Z	6.8 155.9 35	6.3 155.6 35. 35. 0.	7.7 153.6 40. 32410.	9.3 150.5 50. 760. 0.	8.6 147.3 60. 923. 10.
032912Z	7.2 156.4 35	7.2 155.2 35. 71. 0.	9.3 153.7 55. 381. 5.	10.6 150.8 60. 784. 10.	10.3 146.2 60. 962. 5.
<b>0</b> 32918Z	7.6 157.0 35	7.6 156.0 48. 59. 5.	9.6 156.0 60. 313. 10.	11.2 154.3 65. 594. 15.	11.2 150.3 65. 696. 10.
033000Z	8.1 158.0 45	7.8 157.8 48. 225.	6.5 159.4 60. 216. 10.	6.2 157.2 65. 448. 15.	8.0 154.8 65. 435. 5.
0330062	8.5 159.8 58	8.4 158.3 40. 4210.	7.3 160.0 60. 218. 10.	7.4 157.6 65. 357. 15.	9.2 155.0 65. 369. 5.
033012Z	8.7 160.1 50	9.5 160.1 50. 12. 0.	7.3 160.1 60. 261. 10.	8.8 155.7 65. 416. 10.	10.6 149.0 70. 624. 10.
<b>8338</b> 18Z	8.7 161.2 50	9.2 161.2 50. 30. 0.	9.5 166.2 60. 116. 10.	9.2 170.0 65. 475. 10.	7.0 169.2 65.6505.
033100Z	8.8 162.2 50	9.6 162.2 55. 48. 5.	10.2 167.0 60. 207. 10.	9.2 170.8 65. 560. 5.	7.2 168.7 65. 64510.
033106Z	8.9 163.3 50	9.0 163.2 55. 0. 5.	8.9 165.8 60. 199. 10.	8.8 167.3 65. 417. 5.	8.8 168.3 65. 564. 0.
0331122	9.3 164.0 50	9.2 164.2 50. 13. 0.	9.2 168.3 50. 3535.	9.6 172.6 45. 74815.	10.6 176.6 40.105115.
<b>033</b> 118Z	10.0 164.3 50	9.2 164.0 50. 56. 0.	9.4 167.9 50. 3515.	9.4 171.2 45. 69625.	9.8 174.3 40.101810.
<b>040</b> 100Z	10.3 163.5 50	10.3 164.5 55. 59. 5.	11.4 166.9 55. 3195.	12.1 169.4 55. 57220.	14.3 171.8 55. 929. 15.
04 <del>8</del> 106Z	10.4 162.8 50	10.8 162.4 50. 34. 0.	9.8 162.3 50. 13510.	11.4 164.6 50. 29615.	12.6 168.0 45. 784. 15.
048112Z	10.6 162.5 55	10.6 162.1 50. 245.	9.8 161.2 50. 14810.	10.6 163.3 50. 3025.	0.0 0.0 00. 0.
0401182	10.7 162.1 55	10.6 161.8 50. 195.	9.9 161.2 50. 19020.	10.3 163.5 50. 399. 0.	0,0 0.0 00 <b>.</b> 0.
04 <b>0</b> 2 <del>0</del> 0Z	11.0 161.5 60	1 <b>8.8</b> 161.8 55. ?15.	11.8 160.8 60. 11115.	12.6 162.5 65. 387. 25.	8.8 8.8 80. O.
949296Z	11.5 160.8 60	11.6 161.0 65. 13. 5.	14.2 161.4 75. 65. 18.	15.6 165.3 70. 640. 40.	0.0 0.0 00. 0.
<b>040</b> 212Z	12.1 160.3 60	12.2 160.2 65. 8. 5.	14.9 161.3 75. 173. 20.	0.0 0.6 00 <b>. 0</b> .	9.0 0.0 00. 0.
<b>640</b> 218Z	12.8 159.9 70	12.6 159.8 65. 135.	15.3 160.1 75. 213. 25.	0.8 0.0 00. 0.	0.0 0.0 00. O.
040300Z	13.3 159.7 75	13.3 159.8 75. 6. 0.	15.8 160.8 75. 328. 35.	0.0 0.0 B9. 0.	0.0 0.0 00. 0.
<b>040306</b> Z	14.0 160.3 65	13.3 159.6 68. 595.	11.6 157.2 35. 177. 5.	0.0 0.0 0. <del>-0</del> . 0.	9.0 0.0 00. D.
<b>040</b> 3122	13.2 158.9 55	13.0 158.8 50. 135.	0.0 0.8 0e. n.	0.0 0.0 0. <del>-0</del> . 0.	0.0 <b>0.0 00.</b> 0.
<b>0403</b> 18Z	13.0 157.3 50	12.8 157.6 45. 215.	<b>0.</b> 0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
<b>040</b> 400Z	13.1 155.9 40	13.0 156.3 35. 245.	<b>0.0 0.0 00. 0</b> .	0.0 0.0 00. 0.	6.0 0.0 00. O.
040406Z	13.1 154.6 38	13.2 154.6 30. 6. 0.	0.6 0.6 00. 0.	6.6 6.6 <b>66.</b> 6.	0.0 0.0 00. O.

	ALL	FORECAS	its		TYPHO	35 KT		
	<b>URNG</b>	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-H
AVG FORECAST POSIT ERROR	29.	228.	520,	742.	30.	231.	513.	739.
AVG RIGHT ANGLE ERROR	16.	113.	226.	305.	17.	115.	221.	392.
AVG INTENSITY MAGNITUDE ERROR	3.	12.	14.	9.	4.	12.	12.	Θ.
AVG INTENSITY BIAS	-1.	4.	4.	3.	-1.	4.	2.	2.
NUMBER OF FORECASTS	25	21	17	13	24	20	16	12

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1528. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

#### TYPHONH UDESSA FIX POSITIONS FOR CYCLONE NO. 3

#### SATELLITE FIXES

FIX	TIME	FIX					
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE	
1	280300	3.4N 156.8E		T1.0/1.0	INIT OBS	PGTU	
2 3	288688 298888	3.4N 156.6E 6.0N 155.8E	PCN 5		ULCC FIX	PG TW PG TW	
4	290300	6.2N 155.7E		T2.0/2.0 /D1.0/24HRS		PG TIJ	
5 6	290900 291200	6.7N 155.5E 6.9N 156.2E	PCN 5		BRKS CONTINUITY	PG NJ PG NJ	
7	291615	7.3N 157.1E	PCN 6		BASED ON EXTRAP	rgtw	
8	291880 38888	7.6N 157.5E 7.9N 158.6E	PCN 5		BASED ON EXTRAP	PG II,I PG IGI	
18	300300	8.4H 158.4E	PCN 5	73.0/3.0-/D1.0/24HRS		PGTH	
11 12	300600 300900	8.4N 158.6E 8.8N 159.4E	PCN 5			PGTU PGTU	
13	301600	9.8N 168.7E	PCN 5			PGTU	
14 15	301603 301603	9.1N 160.5E 9.3N 161.6E	PCN 6 PCN 5		ULAC FIX	KCUC PGTW	
16	302053	9. IN 161.3E		T3.5/3.5 /D1.5/21HRS		KGUC	
17	302053	8.9N 161.3E	PCN 5		POSSIBLE EYE	PKIJA	
18 19	302100 310000	9.5N 161.7E 9.3N 162.4E	PCN 5	T3.0/3.0 /S0.0/21HRS		PGTU PGTU	
26	310306	9.1N 162.4E	PCN 6			KGWC	
21 22	311200 311551	9.2N 164.3E 10.0N 164.0E	PEN 5 PCN 6			PGTW KGMC	
23	311600	9.6N 164.5E	PCN 5			PGTU	
24 25	311800 312030	18.1N 164.6E 18.3N 164.8E	PCN 5	T4.8/4.0 /D0.5/24HRS		PG TW KGUC	
26	312030	10.3N 163.5E	PCN 5	14.0, 4.0 , 50.0, 54.10		PKUA	
27 <b>28</b>	910000 910300	10.5N 164.7E 10.5N 163.2E	PCN 5	T4.8/4.0 /D1.8/27HRS		Pr. fiji PG fiji	
29	818688	18.7N 162.4E	PCN 5	14.0/4.0 /DI.0/2/145		PGTW	
38	010900	10.8N 162.4E	PCN 5			PGTW PGTW	
31 32	011540 011600	18.9N 162.1E 18.8N 162.1E	PCN 6 PCN 5			PGTU	
33	011900	10.7N 161.8E	PCN 5			PGTW	
34 35	812100 820000	10.6N 161.8E	PCN 5 PCN 1		EYE DIA 18NM	PG TW PG TW	
36	020300	11.4N 161.2E	PCN 1	T4.0/4.0 /50.0/24HR5	EYE DIA 5NM	PGTÜ	
37 38	828425 828688	11.6N 161.1E	PCN 3 PCN 3			PGTW PGTW	
39	828988	12.0N 160.4E	PCN 5			PGTW	
<b>40</b> 41	021200 021600	12.2N 160.3E 12.4N 159.9E	PCN 5			PGTU PGTU	
42	821888	12.4N 160.1E	PCN 5			PGTU	
43 44	022100 030000	12.9N 159.9E 13.4N 159.5E	PCN 5 PCN 5		BASED ON EXTRAP	PG fu PG fu	
45	030300	13.7N 159.5E	PCN 5	T3.0/4.0-/W1.0/24HRS	BROCK ON EXTENT	PG TU	
46 47	030413 03 <del>0600</del>	13.9N 159.8E 14.1N 168.1E	PCN 5 PCN 5			PGTW PGTW	
48	030900	14. IN 168.0E	PCN 5			PGTW	
49 58	031200 031600	13.2N 158.8E 13.2N 157.4E	PCN 5		EXP LLCC	PGTW PGTW	
51	631900	13.3N 157.6E	PCN 5			PGTW	
52	040000	13.2N 155.9E	PCN 3	TO E O B AD E O HIDE	EXP LLCC	PGTW PGTu	
53 54	848386 848481	13.2N 155.2E 13.2N 154.9E	PCN 3 PCN 3	T0.5/2.8 /42.5/24HRS	EXP LLCC	PGTU	
55	040600	13.2N 154.6E	PCN 3		EXP LLCC	PGTW	
				p:pr:	RAFT FIXES		
				n anca	THE PERSON		
FIX NO.	TIME (Z)	FIX POSITION	FLT LVL		MAX-FLT-LVL-WND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE EYE ORIEN- SHAPE DIAM/IATION	EYE TEMP (C) MSN OUT/ IN/ DP/SST NO.
1	296328	6.2N 155.BE	1500FT	994 35 248 15	270 35 210 45 5 1	CIRCULAR 18	+25 +26 +24 28 1
2	292217	7.8N 157.6E	788119	3030 35 180 18	070 31 350 25 7 5	CINCOLIK ID	+14 + 9 2
3 4	301140 310213	8.6N 160.BE 8.9N 162.5E	7861B 7861B	2947 985 2990 989 45 258 18	968 52 348 15 8 2 358 43 288 48 15 3		+16 +16 +18 3 +13 +17 + 8 4
5	318638	8.9N 163.2E	7 <b>9919</b>	2999 48 868 18	030 42 320 30 10 5		5
6 7	310044 312017	9.2N 163.5E 18.1N 164.8E	7881B 7861B	3015 989 2973 985 68 890 15	348 51 248 28 18 5 178 47 838 8 5 5	CIRCULAR 8	+12 +19 + 8 5 +15 +23 +14 6
8	010037	10.5N 162.7E	7001B	2981 987	368 45 218 17 15 3	EI.L IPTICAL 25 18 828	+12 +19 + 9 7
9 18	812126 828688	10.9N 161.9E	7801B 7801B	2951 986 58 188 11 2897 65 898 6	256 55 188 11 4 4 188 72 898 6 5 5		+13 +14 +12 8
11	828837	11.8N 168.4E	7001B	2933 977	239 68 168 15 18 5	CIRCULAR 18	+15 +19 + 8 9
12 13	622619 638668	12.9N 160.0E 13.3N 159.5E	7881B 7861B	2986 964 88 858 4 3891 999 58 388 15	100 79 020 12 5 2 110 27 010 60 10 2	ELLIPTICAL 15 10 898	+13 +21 + 7 10
14	032056	13.1N 156.5E	78819	3115 25 040 35	270 23 210 30 10 0		+14 +14 + 5 12
15	032256	13.8N 156.3E	7 <b>801</b> 8	3127 35 320 60	188 23 378 68 18 6		12

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACY PUMPOSES.

TYPHOON PAT BEST TRACK DATA

	BEST TRACK	WARNING FRRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR	POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
051618Z	10.2 135.9 25	0.8 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.8 00. 0.	0.0 8.0 00. 0.
0517002	10.9 134.6 25	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 D.0 GD. G.
051706Z	11.5 133.2 30	11.4 133.2 30. 6. 0.	12.5 129.1 40. 102. 0.	13.0 124.9 50. 14415.	13.4 121.0 50. 37550.
051712Z	11.6 131.6 38	12.0 132.2 30, 43, 8.	13.2 128.0 45. 71. 5.	13.5 124.2 50. 16220.	13.7 120.5 45. 43160.
<b>0</b> 51718Z	11.3 130.0 35	11.9 130.4 35. 43. 0.	12.0 125.9 55. 69. 5.	12.7 122.4 50. 28935.	12.6 118.8 45. 59960.
651800Z	11.2 128.6 35	10.8 120.2 35. 34. 0.	10.9 123.2 25. 26630.	10.5 118.4 30. 55765.	11.0 113.8 45. 94155.
051806Z	11.5 127.7 40	10.8 126.8 40. 68. 0.	10.6 122.1 25. 33440.	18.6 117.4 35. 63665.	10.8 112.8 45.106045.
0518122	12.4 127.1 48	12.2 126.4 45. 43. 5.	12.5 121.5 35. 27935.	12.7 117.4 40. 59965.	13.5 113.3 45.104040.
051818Z	13.8 126.5 50	13.8 125.8 45. 415.	15.8 121.7 55. 16730.	16.5 117.7 45. 51360.	16.9 113.7 50.102925.
851988Z	14.6 125.7 55	15.2 125.6 45. 3610.	20.9 125.2 50. 18945.	25.5 130.0 50. 35950.	28.3 137.2 45. 36325.
051906Z	15.4 125.0 65	15.6 124.5 55. 3110.	19.3 122.4 65. 13235.	24.5 125.9 65. 24325.	28.2 133.2 45. 25420.
<b>05</b> 1912Z	16.2 124.4 78	16.4 124.1 65. 215.	21.1 124.2 70. 12235.	25.0 129.0 65. 19323.	20.2 137.2 55. 171. 0.
<b>65</b> 19182	17.2 124.2 85	17.3 123.8 65. 2428.	21.8 124.2 70, 157, -35,	25.5 129.5 60. 20915.	27.8 137.9 50. 145. 0.
052000Z	17.9 124.2 95	17.8 124.8 95. 13. 8.	21.5 125.5 100. 115. 0.	26.2 132.7 65. 1635.	0.0 0.0 00. 0.
052006Z	18.6 124.6 100	18.9 124.6 100. 10. 0.	23.0 128.2 90. 127. 0.	27.3 138.2 60. 2225.	0.0 0.0 0 <i>.</i> -0. 0.
052012Z	19.3 125.2 105	19.3 125.1 100. 65.	23.0 126.2 85. 94. 0.	27.1 137.2 55. 107. 0.	0.0 0.0 00. 0.
<b>052018</b> Z	19.8 126.0 105	20.0 125.6 105. 26. 0.	23.8 129.4 80. 126. 5.	27.8 139.2 50. 95. 0.	0.0 0.0 00. 0.
052100Z	20.2 127.0 100	20.3 126.8 100. 13. 0.	24.3 132.9 70. 49. 0.	0.0 0.0 0. —0. 0.	0.0 0.0 00. 0.
052106Z	20.9 127.9 90	21.0 120.0 95. 8. 5.	25.8 134.8 65. 87. 0.	0.0 0.0 OO. O.	0.0 0.0 90. 0.
Ø52112Z	21.8 129.3 85	21.8 129.1 90. 11. 5.	27.8 137.2 60. 148. 5.	0.0 0.0 00. D.	0.0 0.0 00. 0.
052118Z	22.3 131.0 75	22.8 130.7 75. 34. 0.	29.8 141.2 50. 205. 0.	0.0 0.0 00. 0.	0.0 <del>0</del> .0 00 <i>.</i> 0.
<b>052200Z</b>	23.5 133.1 78	23.7 133.0 70. 13. 0.	0.0 0.0 00. 0.	0.8 0.0 00. 0.	0.0 0.0 0. <del>-</del> 0. 0.
<b>05220</b> 62	24.5 135.5 65	25.2 135.7 65. 43. 0.	0.0 0.0 0, -0. 0.	0.0 0.0 00. O.	0.0 0.0 00. 0.
<b>052212</b> Z	25.4 137.8 55	25.8 137.7 55. 25. 0.	0.0 0.0 D0. 2.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
<b>0</b> 522182	26.5 140.2 50	27.2 140.7 50. 50. 0.	0.0 0.0 00. 0.	0.0 0.0 90. 0.	0.0 6.P 00. 0.

	ALL	FORECAS	TS		TYPHO	35 KTS			
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48 HR	72-HR	į
AVG FORECAST POSIT ERROR	28.	149.	299.	583.	29.	149.	299.	583.	
AVG RIGHT ANGLE ERROR	24.	134.	237.	394.	24.	134.	237.	394.	
AVG INTENSITY MAGNITUDE ERROR	3.	16.	30.	35.	3.	16.	30.	35.	
AVG INTENSITY BIAS	-2.	-14.	-30.	-35.	-2.	-14.	-30.	-35.	
NUMBER OF FORECASTS	23	19	15	1.1	21	19	15	11	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1994. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

14. KNOTS

TYPHOON PAT FIX POSITIONS FOR CYCLONE NO. 4

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
* 1	141666	12.6N 141.2E	PCN 5		ULAC FIX	PGTW
2	160547	9.3N 137.3E	PCN 5	T1.0/1.0	INIT OBS	PGTW
3	161200	9.7N 136.4E	PCN 5		ULCC FIX	PGTW
4	161600	9.9N 135.5E	PCH 5		ULCC FIX	PGTW
5	161832	10.7N 135.1E	PCN 5		ULCC FIX	PGTW
6	170300	11.4N 133.8E	PCN 3			PGTW
7	170535	11.6N 133.4E	PCN 5	T1.5/1.5 /D0.5/24HRS		PGTW
8	170900	11.8N 132.6E	PCN 5		ULCC FIX	PGTW
. 9	171200	12.0N 132.1E	PCN 5			PRTU
10	171600	11.5N 130.3E	PCN 5			PGTU
11	171800	11.5N 129.6E	PCN 5			PGTW
12	172100	11.2N 128.2E	PCN 5			PGT⊎
13	188888	11.1N 128.4E	PCN 5			PGTW
14	180523	11.2N 127.6E	PCN 3	T3.0/3.0~/D1.5/24HRS		PGTW
15	180900	11.6N 127.4E	PCN 5			PGTW PGTW
16	181200	12.2N 127.1E	PCN 5			
17	181600	13.6N 126.5E	PCN 5			PGTW PGTW
18	181800	14.1N 126.3E	PCN 5			
19	181800	13.9N 126.1E	PCN 5			PGTW PGTW
20	102100	14.5N 125.6E	PCN 5		ULCC FIX	
21	190000	14.7N 125.6E	PCN 5			PGTW PGTW
22	190300	15.1N 124.6E	PCN 3	** * * * * * * * * * * * * * * * * * * *		PGTU
23	190600	15.4N 124.5E	PCN 3	T3.5/3.5 /D0.5/25HRS		PGTW
24	190900		PCN 3 PCN 5			PGTW
25	191200	16.2N 124.3E				PGTW
26	191600	16.5N 123.8E	PCN 5			PGTW
27	191756	17.0N 124.1E	PCN 3 PCN 3		EYE FORMING	PGTW
28	191888	17.0N 123.9E 17.4N 124.0E	PCN 3		ETE PURTING	PGTW
29 30	200000	17.7N 124.3E	PCN 1		BANDING EYE	PGTW
30 31	200600	18.5N 124.5E	PCN 1	15.5/5.5 /D2.8/24/RS	DHUNIUR FIC	PGTW
		18.3N 124.3E	PCN I	T5.0/5.0	INIT DOC	RODH
32 33	200641 200900	19.8N 124.9E	PCN I	13.0/3.0	INIT 085	PGTW
33	200300	13.01 124.76	ren i			FGIW

34 35 36 37 38 39 41 42 43 44 45 46 47 48 50 51 52	201200 201600 201980 201992 202100 210000 210600 210629 210600 211200 211600 211800 2211800 2220300 220300 220300 220900	19.3N 125.1E 19.6N 125.3E 19.7N 125.7E 19.8N 125.9E 19.9N 127.0E 20.7N 127.3E 21.0N 120.2E 21.0N 120.2E 21.4N 120.3E 21.4N 120.3E 21.4N 120.3E 22.5N 131.6E 22.5N 131.6E 22.5N 133.1E 24.4N 133.1E 24.4N 133.1E 24.4N 135.9E	PCN 1 PCN 1 PCN 1 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5	T5.5/	5.5 /9	18 . 5/2 I HRS 18 . 8/2 4 HRS 12 . 8/2 4 HRS	<b>.</b>		UI UI UI UI	LICC F	IX IX IX IX	nuri				PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU				
						e	IRCR	AFT F	IXE	5										
FIX NO.	TIME (Z)	FIX POSITION	FLT	700MB HGT	08S MSLP	MAX-SFC- VEL/BRG/				-LVL- ⁄BRG/				EYE SHAPE		OR IEN TAT IO		YE TEMP		MSN NO.
	210913 212001 220926	11.3N 133.8E 10.9N 120.9E 12.1N 127.4E 15.3N 124.9E 16.2N 124.3E 17.6N 124.15E 18.5N 124.5E 18.6N 124.5E 18.7N 124.9E 20.1N 126.3E 20.2N 126.3E 21.1N 120.1E 21.4N 120.5E 23.6N 131.7E 25.8N 137.0E 25.1N 136.8E	70018 70018 70018 70018 70018 70018 70018 70018 70018 70018 70018 70018	3058 2993 2854 2842 2664 2623 2594 2631 2634 2625 2656 2769 2928 2896	1004 999 990 970 949 944 943 947 952 968 988	25 338 35 348 40 250 50 210 65 120 65 120 65 120 65 130 100 270 60 100 80 210 80 180 65 228 65 320	30 10 20 30 45 10 5 45 60 10 30 60 35	150 848 270 869 170 030 290 190 348 030 270 280 310 270	37 50 75 80 94 84 99 92 100 90 103 69 93	290	40 20 15 14 62 15 8 30 15 30 30 30 30 30 30 30	20 15 5 10 5 15 10 10 10 3	10 2 2 2 7 16 3 1	CIRCULAR CIRCULAR CIRCULAR CIRCULAR ELLIPTICAL	15 20 15 20 30 23	8 950	+11 +15 +13 +15 +12 +11 +11	+12 +1 +13 +1 +14 +1 +19 + +19 + +18 +1 +16 +1 +21 +1 +19 +1	3 3 8 6 4 4 4 5	3 4 5 6 6 7 7 8 8 9 9 10 11 12 12 12
						F	RDAR	FIXE	S											
FIX NO.	TIME (Z)	FIX POSITION	RADAR AC	CRY:	EYE SHAP			RADOI ASWAI					c	COMMENTS			RAI POS I	DAR TION	SITE UMO N	
3 4 5	182000 182100 182200 182300 190100 200200	14.2N 126.0E 14.5N 125.8E 14.6N 125.6E 14.8N 125.4E 15.2N 125.1E 18.4N 123.0E	LAND					22273 22272 22882 22813 22813 38494	533 531 3 432 3 532 4 536	316 114 218 21 <b>0</b>							14.8N 14.8N 14.8N 14.8N	124.3E 124.3E 124.3E 124.3E 124.3E 124.3E	9844 9844 9844	7 7 7
						SYN	IOPT I	C FIX	ŒS											
FIX NO.	TIME (Z)	FIX POSITION	INTENSIT ESTIMATE		REST	D		c	OMME	ENTS										

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

\* 1 221800 27.0N 142.5E 040

TYPHOON RUBY BEST TRACK DATA

	BEST TR	RACK		WARN:		RORS		24 H	OUR FO	ORECA!			48 H	DUR F	DRECA!			72 H		DRECA!	
MO/DA/HR	POSIT WI	MD	POS 1 T	WIND	DST	WIND	POS	IT	MIND	DST	MIND	P09	TI	WIND		MIND	POS	IT	MIND	DST	WIND
861886Z		15	0.8 0.6	0.	-0.	D.	0.0	0.0	A.	-B.	0.	9.0	0.0	0.	-0.	e.	8.6	0.0	0.	-0.	ø.
061812Z	9.3 147.4	15	0.0 0.6		-B.	ø.	0.0	0.0	ø.	ě.	ē.	0.0	9.0	Ä.	-0.	ø.	8.0	8.0	6.	-Ð.	ø.
061818Z		20	0.0 0.0		-0.	ø.	0.0	0.0	ø.	-0.	ē.	0.0	9.0	a.	Θ.	ě.	8.6	0.0	e.	-0.	0.
061900Z		20	0.0 0.0		~8.	ø.	8.0	0.0	ø.	-0.	ø.	0.0	0.0	ă.	-0.	e.	6.8	0.0	6.	-0.	ě.
061906Z		20	8.0 0.6		~0.	ø.	0.0	0.0	ø.	- Đ.	ø.	0.0	0.0	й.	-0.	8.	6.6	0.0	ě.	-ø.	ø.
061912Z		25	0.0 0.0		-0.	ø.	6.0	0.0	ě.	-B.	A.	0.0	0.0	ě.	-9.	ø.	0.0	0.0	ø.	-0.	ē.
061918Z		25	0.0 0.0		-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.8	0.0	ø.	-0.	ø.
962000Z		25	0.0 0.0		-0.	ø.	0.0	0.0	Ñ.	-ē.	ø.	0.0	8.8	ø.	-0.	ě.	0.8	0.0	a.	-0.	ø.
062006Z		25	0.0 0.0		-0.	ñ.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	~e).	0.	0.0	0.0	e.	-0.	ø.
0620122		30	0.0 0.6	ø.	-0.	ø.	0.0	0.0	e.	-0.	ē.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-ē.	ē.
062018Z		30	0.0 0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	e.	0.0	0.0	0.	-0.	ø.	8.8	0.0	ē.	-0.	ø.
0621002		30	9.6 139.2		6.	5.	10.3	137.0	50.	312.	15.	11.6	134.2	65.	565.	25.	13.4	130.6	80.	703.	25.
062106Z	9.5 139.7	35	9.6 138.9		48.	в.		137.3	45.	347.	10.		134.7	68.	567.	15.	12.7	131.9	75.	651.	15.
0621122		35	9.5 139.9		36.	ø.	10.0	139.5	50.	290.	15.	11.0	138.2	68.	427.	15.	11.7	135.8	78.	543.	5.
06211BZ			10.2 139.6	40.	94.	5.	11.4	138.2	55.	334.	15.		136.5	65.	432.	15.	13.4	134.2	75.	549.	10.
8622882			11.2 142.3	45.	8.	10.		143.3	60.	ø.	20.		142.9	75.	57.	20.	21.2	145.7	70.	319.	e.
0622062	12.4 142.8	35	11.9 142.8	45.	30.	10.	15.5	143.2	60.	13.	15.	19.4	143.5	78.	130.	10.	22.4	147.8	65.	466.	-5.
0622122			13.6 143.2		19.	10.	17.2		55.	97.	10.		140.2	55.	133.	-10.	24.8	143.6	50.	240.	-25.
0622182	14.1 143.2	40	14.6 143.2	45.	30.	5.	18.2	141.5	55.	99.	5.	21.3	139.6	50.	87.	-15.	24.9	141.8	40.	139.	-35.
062300Z	14.8 143.3	40	15.4 143.1	50.	38.	10.	19.2	141.1	60.	66.	5.	21.4	139.3	60.	39.	-10.	24.8	141.9	50.	183.	-25.
0623062	15.7 143.3	45	15.4 143.2	60.	19.	15.	10.0	143.3	70.	98.	10.	20.9	143.0	75.	266.	5.	23.6	146.7	65.	486.	-5.
862312Z	16.3 143.1	45	16.4 143.5	60.	24.	15.	19.6	143.1	70.	112.	5.		143.2	75.	226.	0.	26.1	144.6	65.	397.	e.
062318Z	16.8 142.4	50	17.2 142.6	66.	33.	10.	20.4	141.9	70.	74.	Ś.	23.5	141.8	75.	178.	0.	0.0	0.0	0.	-e.	ø.
062400Z	17.5 142.0	55	17.6 141.6	60.	13.	5.	19.8	139.2	70.	106.	ø.	22.4	136.2	70.	348.	-5.	6.0	0.0	0.	-0.	a.
0624062	18.2 141.6	69	18.7 141.4	55.	32.	-5.	21.5	139.7	50.	77.	-20.	25.0	136.8	45.	334.	-25.	8.8	0.0	ø.	-8.	e.
B62412Z	19.1 141.2	65	19.9 140.9	60.	51.	-5.	23.0	138.2	50.	62.	-25.	27.1	130.2	45.	343.	-20.	6.0	0.0	ø.	-8.	0.
062418Z	20.2 140.6	65	20.2 148.7	60.	6.	-5.	23.5	130.3	78.	126.	-5.	0.0	9.9	Đ.	-B.	θ.	<b>9.0</b>	0.0	0.	-Ø.	₿.
062500Z	21.4 140.0	78	21.2 140.6	65.	12.	~5.	25.7	137.9	70.	136.	-5.	0.0	0.0	0.	-0.	ē.	0.0	0.0	0.	-0.	0.
062506Z	22.6 139.4	70	22.2 139.2	65.	26.	-5.	27.0	138.2	75.	193.	5.	0.0	0.0	0.	-0.	e.	0.0	0.0	ø.	-8.	0.
062512Z	24.0 139.3	75	23.6 139.2	70.	25.	-5.	29.2	140.2	70.	185.	5.	0.0	0.0	0.	-0.	ø.	0.0	9.0	9.	- <b>e</b> .	0.
062518Z	25.4 139.3	75	24.8 139.2	75.	36.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	e.	-0.	ø.	0.0	9.0	ø.	-0.	0.
0626002	27.2 139.8	75	27.1 139.8	75.	6.	0.	8.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	8.	9.6	9.6	8.	-0.	0.
062606Z	29.5 140.5	70	29.6 140.6	70.	θ.	ø.	0.0	0.0	ē.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	e.
0626122			32.2 141.1	65.	16.	ø.	0.0	0.0	ø.	-0.	e.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECAS	STS		TYPHOONS WHILE OVER				
	WRNG	24-HR	49-HR	72-HR	WRNG	24-HI	R 48-HR	72-HR	
AVG FORECAST POSIT ERROR	27.	144.	275.	425.	28.	144.	275.	425.	
AVG RIGHT ANGLE ERROR	12.	64.	143.	326.	12.	64.	143.	326.	
AVG INTENSITY MAGNITUDE ERROR	6.	10.	13.	14.	6.	10.	13.	14.	
AVG INTENSITY BIAS	3.	4.	1.	-4.	3.	4.	1.	-4.	
NUMBER OF FORECASTS	23	19	15	11	22	19	15	11	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2173, NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON RUBY
FIX POSITIONS FOR CYCLONE NO. 5

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	192100	8.9N 141.1E	PCN 5			PGTW
2	200000	9.2N 148.7E	PCN 5			PGTU
3	200300	9.2N 148.1E	PCN 5	T1.0/1.0	INIT 08S	PGTW
4	200600	9.3N 139.5E	PCN 5			PGTW
5	2009 <b>00</b>	9.4N 139.5E	PCN 5			PGTW
6	2012 <b>00</b>	9.3N 139.4E	PCN 5			PGTW
7	2016 <b>00</b>	9.2N 139.0E	PCN 5			PGTW
8	201800	9.2N 138.4E	PCN 5			PGTU
9	202100	9.4N 138.1E	PCN 5			PGTW
10	210000	9.5N 138.8E	PCN 5			PGTW
11	210300	9.2N 139.1E	PCN 5	T1.0/1.0 /S0.0/24HRS		PGTW
12	210600	9.3N 139.5E	PEN 5			PGTU
13	21 <b>0900</b>	9.2N 148.1E	PCN 5			PGTU
14	211200	9.6N 139.5E	PCN 5			PGTW
* 15	211600	10.5H 140.0E	PCH 5			PGTW
* 16	211900	10.7N 139.9E	PCN 5			PGT⊎
* 17	212100	10.8N 139.3E	PCN 5			PGT⊎
18	220000	11.2N 142.4E	PCN 5		BASED ON EXTRAP	PGTU
19	228388	11.5N 142.2E	PCN 6	T2.5/2.5 /D1.5/24RS		PGT⊎
28	220509	12.6N 142.8E	PCH 5			PGTW
21	228900	12.6H 142.7E	PCH 6			PGTU
22	221200	13.5H 143.3E	PCH 6			PGTU

23	221600	13.8N 143.3E	PCN 6			PG (U
24	221800	14.4N 143.2E	PCN 6			PGTU
25	222188	14.7N 143.2E	PCN 6			PGTW
26	238888	14.8N 143.1E	PCN 4			PGTU
27	238388	15.8N 143.4E	PCN 4	T4.0/4.0 /D1.5/24HRS		PGTU
28	230457	15.4N 143.7E	PCN 4			PGTW
29	230600	15.7N 143.5E	PCH 4			PGTW
30	230900	16.1N 143.3E	PCN 4			PGTU
31	231200	16.6N 143.2E	PCN 6			PGTW
32	231600	17.8N 142.4E	PCN 6			PGTU
* 33	231880	17.5N 141.9E	PCH 4			PGTW
34	232100	17.1N 141.8E	PCN 6			PGTU
35	248888	17.8N 142.3E	PCN 6			PGTW
36	249399	17.6N 142.2E	PCN 6	T4.8/4.0 /S8.8/24HRS		PGTW
* 37	240445	19.3N 142.0E	PCH 6	1-110- 110 - 0010- 2-410	ULCC 17.8N 142.1E	PGTU
* 38	248688	19.4H 141.6E	PCN 6		ULCC 18.0N 141.8E	PGTW
39	240900	18.4N 141.3E	PCN 6		ULCC FIX	PGTW
40	241200	18.7N 140.8E	PCN 6		ULCC FIX	PGTU
41	241600	19.5N 1-48.3E	PCN 6		ULCC FIX	PGTW
42	241730	28.2N 148.8E	PCN 6		ULCC FIX	PGTW
43	242032	21.1N 148.7E	PCN 6		ULCC FIX	PGTW
44	242100	21.8N 148.4E	PCN 6		OCCC FIX	PGTW
45	250000	21.6N 140.1E	PCN 4			PGTW
46	250300	21.9N 139.7E	PCN 4	T4.5/4.5-/D0.5/24HRS		PGTW
47	250600	23.0N 139.9E	PCN 2	14.3/4.3-/00.3/24mc5		PGTU
48	250900	23.2N 139.7E	PCN 2			PGTW
49	251200	24.8N 139.8E	PCN 4			PGTU
50	251600	24.6N 139.6E	PCN 4			PGTU
51	251718	25.3N 139.5E	PCN 4			PGTU
52	251800	25.3N 139.5E	PCN 4			PGTU
52 53	252100	26.7N 148.8E	PCN 4		ULCC FIX	PGTU
54	260000	27.6N 140.0E	PCN 6		ULCC FIX	PGTU
55	268388			T7 F 44 F 411 B 40 8100		PGTW
		28.6N 140.7E	PCH 6	T3.5/4.5 /U1.0/24HRS		
* 56 57	260421	29.4N 141.1E	PCN 5			PGTU PGTU
	260600	30.1N 141.4E	PCN 6			
58	268966	31.4H 142.2E	PCN 6		# 60 FM	PGTU
59	261200	32.4N 142.7E	PCN 6		ULCC FIX	PGTU
60	261600	33.3N 143.0E	PCN 6			PGTU
61	270000	36.0N 143.7E	PCN 6			PGT⊎
62	270300	37.0N 143.9E	PCN 6			PGT⊎
63	270600	37.9N 144.7E	PCN 6			PGT₩

#### AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	788MB HGT	OBS MSLP		-SFC- /BRG/					-LIND ∕RNG			EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	202339	9.6N 139.2E	700MB	3097	995	68	188	15	878	33	848	15	3	2			+12 +13 + 9	ı
2	210930	9.3N 139.9E	700MB	3062	995	45	070	10	340	26	260	15	3	10			#11 +16 + 8	2
3	228633	12.5N 142.8E	788MB	3076		48	150	30	220	26	150	30						4
4	220838	13.0N 143.0E	700MB	3070	1003	48	160	40	230	41	120	120	2	10			+10 +13 + 9	4
5	231959	16.9N 142.8E	786MB	3000					130	42	848	120						5
6	232044	17.8N 142.8E	7 <b>0011</b> B	2993	989	68	130	95	218	49	130	98	5	10	ELL IPTICAL	30 10 360	+10 +13 +10	5
	240809	18.5N 141.4E	700MB	2989	989	65	150	70	180	60	060	90	10	19			+12 +13 + 9	6
8	250630	22.9N 139.3E	700MB	2985		45	260	98	330	52	268	98						8
9	258911	22.7H 139.2E	700MB	2841	977	65	248	15	218	95	100	70	5	15			+12 +16	8
18	251914	25.BN 139.4E	7 <b>00</b> MB	2887					230	78	170	95						9
11	252157	26.2N 139.7E	78811B	2912	988	48	898	8	290	62	220	60	10	10			+12 +14 +13	9
12	268682	29.6N 140.5E	700MB	2923		55	160	50	210	94	899	68						10
13	260912	30.3N 140.7E	788MB	2025	972	50	270	60	350	56	270	60	5	8			+14 +13	10
14	261929	35.0N 142.2E	70 <b>011</b> 0	2847					190	72	090	120						11
15	262149	35.5N 142.7E	700MB	2837		65	260	60	698	71	350	70	5	4			+9+9+9	11

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

#### TROPICAL STORM TESS BEST TRACK DATA

	8ES1	TRACK	:		WORN I		ORS		24 H	DIR F	ORECA: ERKI			46 H	DUR F	DRECA ERRO			72 H		DRECAS ERRORS	
MD/DA/HR	POSIT	LIND	POSIT		WIND		MIND	PO:	SIT	WIND		HIND	PO!	SIT	UIND			PO:	TIE	MIND		UIND
862888Z	17.2 113.			8.8	ø.	-8.	0.	8.0	0.0	8.	-8.	8.	8.6	8.8		-8.	0.	0.0			-6.	
862886Z	17.5 113.			0.0	Ä.	-8.	Ø.	8.8	8.8	ě.	-0.		8.8	9.0	Ĭ.	-ē.		8.0	8.8	ā.	_	
862812Z	17.9 113.			8.8		-8.	ē.	8.8	0.6	ă.	-ē.		0.0	8.8		-6.	ě.	8.0	8.8	Ξ.	-a.	ē.
062B1BZ	18.2 112.		0.0	A. A		-8.	ø.	8.6	8.6	Ď.	-Đ.	ě.	8.8	0.0	ă.	-8.		2.0	8.4	Ĭ.	-0.	ě.
862980Z	18.5 112.			3.0	30.	35.	ð.	19.8	114.3	46	113.	16.	19.8	115.2	45.	116.	15.	21.3	115.7	44	144.	25.
862986Z	18.6 112.			2.4	30.	٠,٠	Ă.	28.4	111.4	30.	96.	0.	22.2		25.	240.	-5.	21.3		<b></b> -	-8.	
0629122	19.2 112.			2.2	36.	11.	ø.	20.5	111.2	30.	135.	-5.	22.3	110.0	20.		-10.	8.8	8.6	9.		
062918Z	19.6 112.			2.0	30.	23.	8.	26.9		38.	175.	-5.		0.0	20.	~B.	9.	0.0	8.8	٠.	-0.	8.
				2.3	30.			20.9					0.6		٥.		= -			٠.	~₽.	Ξ.
	20.0 112.					18.	0.		112.6	30.	123.	0.	0.6	0.0	٥.	-0.	8.	0.0	0.0	٠.	-₽.	0.
	20.5 113.		20.5 11		30.	17.	٠.		113.7	30.	91.	₽.	0.0	0.0	θ.	-0.	0.	0.0	0.0	8.	-0.	٠.
<b>0630</b> 12Z	20.9 113.	6 35	21.6 11	3.7	30.	8.	-5.	22.8	114.3	20.	100.	-10.	9.0	8.0	0.	-0.	0.	0.0	0.6	6.	-0.	ø.
<b>0630</b> 182	21.2 114.	1 35	21.4 11	4.1	39.	12.	-5.	23.2	114.9	20.	123.	-5.	0.0	8.8	₽.	-8.	0.	6.6	8.8	8.	-0.	0.
878186Z	21.7 114.	8 30	21.6 11	4.5	35.	18.	5.	23.6	116.8	€.	58.	-25.	0.0	6.0	A.	-8.	0.	8.8	8.8	8.	-8.	8.
0701062	21.9 115.	3 30	22.2 11	5.5	35.	21.	5.	23.9	118.2	35.	45.	15.	0.0	0.0	ø.	-8.		3.8	0.0	ē.	-6.	8.
	22.1 116.		22.4 11		35.	19.	5.	8.8	6.6	a.	-ē.	0.	0.0	0.0	ø.	−e.		8.8	6.0	ē.	-0.	
	22.3 116.			6.7	30.	ii.	5.	0.8	8.0	ě.	~B.	ø.	8.0	0.0	Ä.	-0.		8.8	6.0	ă.	-e.	ē.
	22.7 117.			7.8	25.	٠	ē.	8.8	0.0	ñ.	~0.	a.	0.0	0.0	ä.	-e.		0.0	6.0	ě.	-8.	e.
	23.2 118.			8.5	28.	8.	8.	8.8	0.0	0.	-0.	0.	8.8	8.8	٥.	-B.	e.	0.0	0.0	٠.	-6.	8.

	ALL	FORECAS	TS .		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	15.	107.	217.	144.	0.	0.	0.	0.			
AVG RIGHT ANGLE ERROR	9.	73.	142.	41.	0.	0.	0.	0.			
AVG INTENSITY MAGNITUDE ERROR	2.	e.	10.	25.	8.	0.	0.	e.			
AVG INTENSITY BIAS	1.	-3.	0.	25.	0.	8.	8.	0.			
NUMBER OF FORECASTS	14	18	3		Ă	ă.	Ä	Ă			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 585. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

6. KNOTS

TROPICAL STORM TESS
FIX POSITIONS FOR CYCLONE NO. 6

	FIX 10.	TIME (Z)	FIX POSITION	ACCRY	DVORAK	CODE	CONTENTS	SITE
*	1	272100	17.6N 111.3E	PCN 6				PGTW
*	2	288388	16.6N 118.7E	PCN 6			ULCC FIX	PGTW
*	3	290721	18.1N 112.5E	PCN 5	T1.5/1.5	5	INIT OBS	RPMK
*	4	280721	17.5N 112.8E	PCN 5				RODN
	5	266966	17.4H 111.4E	PCN 6			ULCC FIX	PGTW
*	6	261288	16.7N 111.3E	PCN 6			ULCC FIX	PGTU
*	7	281696	16.5N 189.7E	PCN 6			ULCC FIX BRKS CONTINUITY	PGT⊌
*	8	281688	16.2N 189.2E	PCN 6			ULCC FIX	PGTW
*	9	282886	18.8N 114.1E	PCN 6				RPMK
*	18	282188	16.8N 189.8E	PCN 6			ULCC FIX	PG TU
*	11	282223	17.4H 116.9E	PCN 6	T1.6/1.0	•	INIT OBS	RODN
*	12	296366	18.5N 113.2E	PCN 6			1515 INIT 08S	PGTW
	13	290688	18.6N 113.0E	PCN 6				PGTW
	14	290708	19.3N 112.2E	PCN 6				RODN
	15	290709	19.2N 113.3E	PCN 5	T1.5/1.5	5 /S8.8/244RS		RPTSK
	16	290900	19.2N 111.9E	PCN 6			ULCC FIX	PGTU
	17	291288	18.2N 111.5E	PCN 6				PGTU
*	18	291600	18.3N 111.2E	PCN 6				PGTU
*	19	291988	18.6N 118.7E	PCN 6				PGTU
*	28	291953	19.8H 111.8E	PCN 5				RPMK
	21	291953	20.2N 112.1E	PCH 6				RODN
*	22	292198	20.2N 111.3E	PCH 6				PGTU
	23	300000	20.0N 113.5E	PCH 6			ULCC 20.3N 111.5E	PGTU
	24	300300	28.2N 112.9E	PCH 4	T1.5/1.	5-/58.8/24HRS		PGTU
	25	300600	28.4N 113.7E	PCH 4				PGTW

* 26	300656	21.8N 114.1E	PCH 3	T1.5/1.5-/S8.8/24RS	EXP LLCC	RPHK
27	300900	21.4N 112.7E	PCN 6		ULCC FIX	PGTU
<b>* 28</b>	301200	21.4N 112.3E	PCN 6		ULCC FIX	PGTU
* 29	301600	21.5N 111.7E	PCN 6		ULCC FIX	PGTU
* 30	301800	21.9N 111.5E	PCN 6		ULCC FIX	PGTU
31	301941	22.5N 113.5E	PCN 5		<del></del>	RPHK
* 32	010000	22.5N 113.2E	PCN 6		ULCC FIX	PGTU
* 33	818386	22.5N 114.1E	PCN 6	T2.5/2.5 /D1.8/24RS		PGTU
34	610600	21.9N 114.BE	PCH 6			PGTU
35	810644	22.6N 115.3E	PCN 5	T1.5/1.5-/S8.8/24RS		RPMK
36	610900	22.8N 115.6E	PCN 6			PGTU
37	011200	21.9N 116.1E	PCN 6		ULCC FIX	PGTU
38	011600	22.0N 116.1E	PCN 6			PGTU
39	011800	22.8N 116.5E	PCN 6			PGTW
48	020000	22.8N 117.5E	PCN 6			PGTW

### SYNOPTIC FIXES

FIX	TIME	FIX	INTENSITY	NEAREST	COMPENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NM)	
* 1 * 2 * 3 * 4 * 5 * 6 * 7	292100 300300 300900 301600 302100 010300	19.3N 114.0E 21.2N 113.0E 21.3N 114.0E 21.6N 114.0E 21.5N 113.7E 21.5N 114.5E 21.5N 115.0E 21.5N 115.0E	36 36 30 30 38 35 35	218 118 75 58 68 48 68 98	

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

#### TROPICAL STORM SKIP BEST TRACK DATA

BEST TRACK	LIARN ING	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
	ERRORS	ERRORS	ERRORS	ERRORS
MO/DA/HR POSIT WIND POS	GHIW TRE GHIW TIR	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
062906Z 21.7 131.7 35 0.0	8.8 88. 6.	0.8 8.8 88. 0.	8.8 8.8 80. 8.	0,0 0.0 S0. C.
062912Z 22.2 133.5 40 0.8	0.0 Q0. Q.	0.0 0.0 00. 0.	8.8 8.8 88. 8.	8.8 0.0 90. O.
<b>962918</b> 2 22.9 135.4 49 6.8	8.0 O0. O.	0.8 0.8 00. 0.	8.6	e.0 e.0 B0. C.
963888Z 24.1 137.2 48 24.2	137.3 45. 8. 5.	27.6 146.2 35. 3915.	8.8 8.8 B0. B.	0.0 0.0 00. O.
963886Z 25.1 138.9 48 25.2	139.1 45. 12. 5.	27.8 147.4 35. 13118.	0.0 B.D DD. B.	0.0 0.0 00. 0.
8638122 26.8 141.1 45 26.8	141.0 45. 5. 0.	30.0 149.3 30. 11415.	0.0 0.5 0D. D.	0.0 0.0 00. 0.
8638182 26.8 143.7 45 26.8	143.2 48. 275.	0,8 0.0 00. D.	0.0 8.0 D, -0. D.	0.8 8.8 88. 8.
878186Z 28.2 146.5 50 29.2	145.7 40, 11, -10,	0.0 0.0 00. 0.	8.8 8.8 88. 8.	0.0 0.6 GO. O.
878186Z 29.4 149.1 45 29.6	149.3 48. 165,	<b>A.</b> 0 0.0 0. −0. 0.	0.0 0.0 0, -0. 0.	8.6 6.8 80. 8.
878112Z 38.8 151.3 45 31.8	151.9 48. 335.	8.0 0.0 00. 0.	O.E. O.D. O0. C.	8.8 6.8 88. 8.

	ALL FORECASTS				TYPHOONS WHILE OVER 35 KTS					
	<b>URNG</b>	24-HR	48-HR	72-HR	LIRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	16.	95.	0.	₽.	8.	8.	0.	0.		
AVG RIGHT ANGLE ERROR	15.	32.	₽.	8.	8.	8.	Ø.	0.		
AVG INTENSITY MAGNITUDE ERROR	5.	13.	0.	8.	8.	8.	8.	6.		
AVG INTENSITY BIAS	-2.	-13.	8.	8.	8.	8.	0.	0.		
NUMBER OF FORECASTS	7	3	ä	Ā	8	ā	8	Ā		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1197. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 22. KNOTS

TROPICAL STORM SKIP
FIX POSITIONS FOR CYCLONE NO. 7

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
<b>*</b> 1	290526	22.7N 132.8E	PCN 6	T1.8/1.8	INIT OBS	PGTU
2	290900	21.BN 132.4E	PCN 6		ULCC FIX	PGTW
3	291200	21.8N 132.BE	PCN 6			PGTW
4	291688	22.IN 134.2E	PCH 6			PGT⊎
5	291811	22.5N 135.8E	PCN 5			PGT⊎
6	291811	22.8N 135.7E	PCN 5			RPMK
?	292100	23.7N 136.6E	PCN 6			PGTW
8	300000	24.2N 137.8E	PCN 4			PGTW
9	30030/	4.5N 137.4E	PCH 4	T2.5/2.5 /D1.5/22HRS		PGTU
10	3862:4	24.9N 138.8E	PCN 3			PGTW
11	388679	25.BN 139.1E	PCN 4			PGTU
12	300900	25.7N 148.7E	PCN 6		ULCC FIX	PGTU
13	38128C	25.9N 142.1E	PCN 6			PGTU
14	301600	26.3N 144.0E	PCN 6			PGTW
* 15	301800	26.5N 145.0E	PCN 6			PGT⊎
* 16	302100	27.1N 146.6E	PCN 6			PGTW
17	910000	28.5N 147.4E	PCN 6		BRKS CONTINUITY	PGTU
18	010300	28.9N 147.8E	PCH 6	T3.0/3.8-/D0.5/24HRS		PGTU
19	010600	29.4N 148.6E	PCN 6			PGTW
* 20	818988	30. IN 152.0E	PCH 6		BRKS CONTINUITY	PGTU
21	011200	31.8N 152.2E	PCN 6			PGTU
22	011600	31.3N 152.5E	PCN 4		EXP LLCC	PGTW
23	011900	31.6N 153.6E	PCN 4		EXP LLCC	PGTU
24	012100	32.6N 154.9E	PCH 4		EXP LLCC	PGTU

AIRCRAFT FIXES

	TIPE (Z)	FIX POSITION				MRX-SFC-LIND VEL/BRG/RHG						EYE	EYE ORIEN- DIAM/TATION		MEN NO.
2 3 + 4	300933 301959 302156	24.3N 137.6E 25.6N 146.6E 28.1N 144.9E 28.9N 144.7E 38.7H 158.7E	70018 70019 70019	3824 3850	991 995	40 210 70 40 140 30 50 200 90 45 150 120 45 190 120	270 278 200	53 150 50 200 46 150	90 120	10	6 15			+24 +23 +18 29 +13 +16 + 6 + 9 + 9 + 4 +11 +13 +12	1 2 3 3 4

SYNOPTIC FIXES

TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	COPPENTS

88 26.5N 142.5E 40 40 UPD 4798

HOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

# TROPICAL STORM VAL

BEST TRACK	WARM ING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR POSIT WIND	POSIT UIND DST LIND	POSIT WIND DET WIND	POSIT UIND DET UIND	POSIT LIND DET LIND
8782882 24.3 123.3 35	0.8 0.0 00. 0.	0.0 0.0 00. 6.	0.8 0.0 00. 0.	0.0 6.0 00. 0.
878286Z 24.3 123.9 35	8.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
8782122 24,3 124,3 4	0.0 0.0 00. 0.	8.8 8.9 B8. B.	0.0 0.0 00. 0.	0.0 6.0 00. 0.
978218Z 24.3 125.6 45	5.0 6.0 00. O.			
	24.8 127.8 45. 018.	26.9 132.0 55. 363. 28.	0.8 8.8 88. 6.	6.8 8.8 88. 8.
978386Z 26.2 129.9 50 ;	26.2 129.9 50. 0. 0.	0.8 0.8 06. 0.	0.8 0.0 00. 0.	8.8 f.S S6. S.
<b>0703122 27.7 132.3 45</b>	27.5 131.9 50. 24. 5.	0.8 0.0 00. 0.	0.0 0.0 00. A.	0.0 0.0 06. 0.
878318Z 28.9 135.1 45	28.9 134.5 58. 32. 5.	8.8 8.9 80. 9.	D.B D.B BB. B.	0.0 0.0 00. 0.
	30.0 136.9 50. 91. 15.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	8.0 8.0 80. 8.
0104002 23.7 130.7 33	30.0 130.9 30. 91. 15.	0.6 0.0 00. 0.	3.0 0.0 P0. D.	0.0 0.0 00. 0.

	ALL	<b>FORECAS</b>	TS		TYPHOONS WHILE OVER 35 KT						
	LITTING	24-HR	48-142	72-1根	LIRNG	24-HR	46-HR	72-HR			
AVG FORECAST POSIT ERROR	29.	363.	●.	●.	■.	8.	●.	8.			
AVG RIGHT ANGLE ERROR	22.	33.	₽.	ø.	8.	0.	8.	Ü.			
AVG INTENSITY MAGNITUDE ERROR	7.	20.	●.	●.	8.	8.	8.	Ð.			
AVG INTENSITY BIAS	3.	20.	₽.	0.	8.	8.	8.	8.			
NUMBER OF FORECASTS	5	1	•	•		8		•			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 876. HM
AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

TROPICAL STORM VAL.
FIX POSITIONS FOR CYCLONE NO. 8

#### SATELLITE FIXES

	1X 10.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
	1	828668	24.9N 125.1E	PCN 6	T8.5/8.5	INIT DBS	PGTU
*	2	020300	25.4H 125.5E	PCN 6			PGTU
*	3	828988	25.3N 126.1E	PCN 6		ULCC FIX	PGTW
	4	021600	23.3N 125.6E	PCN 6		ULCC FIX	PGTW
	5	921988	23.7H 125.7E	PCH 6		ULCC FIX	PGTW
	6	638666	24.8N 127.8E	PCN 6		BASED ON EXTRAP	PGTW
	7	838300	25.6N 128.9E	PCN 6	T2.5/2.5	INIT ORS	PGTU
	8	038600	26.2N 129.9E	PCN 6		BASED ON EXTRAP	PGTU
	9	636966	27.2N 131.8E	PCN 6		BASED ON EXTRAP	PGTM
	10	831266	27.6M 132.3E	PCN 6		ULCC FIX	PGTM
	11	031600	28.8N 134.5E	PCN 6			PG <b>TU</b>
	12	831723	28. IN 135.4E	PCN 5		ULCC FIX	PGTU
	13	032100	29.2N 137.5E	PCH 6			PGTU
	14	840600	29.4H 138.2E	PCN 6		ULCC 29.6N 139.7E	PGTW

### AIRCRAFT FIXES

TIME (2)	FIX POSITION	FLT LVL			MAX-FLT-LVL-UND DIR/VEL/BRG/RNG	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
	25.1H 124.2E 24.7H 127.8E		2938		3 0 312 2 0 009 250 56 030 26			24+ 26+ 242 9 +25 +26 29	1 2

#### SYNOPTIC FIXES

FIX	TIPE	FIX	INTENSITY	NEAREST	CONTENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NM)	
2 3	821266 821868	24.5N 123.4E 24.3N 124.2E 24.4N 125.5E 26.4N 138.2E	35 35 35 35	38 28 20 60	UMD 47912 47918 UMD 47918 UMD 47927 UMD 47945

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNKEPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TROPICAL STORM WINDHA

	BEST T	RACK	:	UARN I		RORS		24 H	OUR F	DRECA: ERRI		48	HQUR F	ORECAS			72 H		DRECAS	
HD/DA/48	POSIT U	IND	POSIT	UIND			ene	SIT	MIND		MIND	POSIT	MINE			POS	:IT	UIND	PST	
871212Z	11.8 132.6	25	11.8 132.1		29.	5.	13.4				15.	14.9 123		76.			119.2		46.	
871218Z	12.2 131.5					= -									Ξ.				70.	
		25	12.1 138.9		36.	5.	13.7			195.	19.	15.2 122		78.	5.				44.	<del>-5</del> .
0713 <b>06</b> 2	12.8 138.8	25	12.3 138.5		35.	5.	14.0			78.	5.	15.5 121			e.		117.9	35.		-15.
871386Z	13.5 130.2	30	13.2 129.6	30.	39.	₽.	15.0	125.3	45.	30.	-5.	15.8 121.	3 50.	6.	5.	17.9	117.8	35.	1¢8.	-20.
871312Z	13.6 129.1	38	14.8 129.4	30.	21.	₽.	15.0	125.5	45.	61.	~5.	15.8 121	6 58.	99.	15.	18.3	110.5	35.	281.	-28.
871318Z	13.8 128.8	35	14.1 127.6	30.	29.	-5.	15.4	123.0	50.	29.	ø.	17.6 119.	1 35.	58.	-5.	20.5	116.3	38.	219.	-15.
871486Z	14.1 126.6	40	13.7 126.8	48.	27.	ā.	15.1	122.1	55.	27.	5.	17.8 118	7 38.	109.	-20.	21.6	117.2	38.	339.	-5.
871486Z	14.4 125.5	Sa	14.4 125.6		6.	-š.	15.0		46.	29.	-5.	19.8 118			-20.		116.8		396.	ě.
871412Z	14.7 124.5	50	14.8 124.5		6.	Ξ.		120.2		13.	5.	19.7 117					117.2		468.	5.
871418Z	15.1 123.4	56		•••		Ξ.												8.		
			15.1 123.2		12.	8.		119.6		69.	ø.	20.4 117		201.	-15.	8.8	0.0	e.	-0.	₹.
871588Z	15.5 122.3	50	15.3 122.2		13.	ø.		118.5	30.	99.	-20.	22.5 117.			-5.	0.0	8.8	0.	-8.	٥.
871586Z	15.9 121.3	45	15.8 121.2	40.	θ.	-5.	18.0	118.1	30.	176.	-25.	23.8 117	3 38.	416.	8.	8.6	8.8	8.	-0.	8.
071512Z	16.4 128.8	35	16.1 120.5	35.	34.	8.	17.8	117.8	30.	257.	-25.	21.3 115.	9 30.	375.	5.	6.6	8.8	0.	-8.	8.
871518Z	16.9 118.4	40	16.5 119.2	45.	52.	5.	19.8	115.6	50.	199.	5.	0.0 0	8 8.	-0.	a.	8.8	0.0	0.	-0.	θ.
871686Z	17.8 116.8	50	17.6 117.8		17.	-5.			60.	92.	25.	8.8 8.		-8.	0.	0.0	0.8	ø.	-0.	8.
071686Z	18.8 115.0	55	18.8 115.2		ii.	ē.				213.	-10.	8.6 6.		-8.	ø.	8.8	8.8	9.	-0.	Ð.
871612Z	19.8 113.8	55	20.0 113.5		21.	ě.	8.8	8.6	0.	-ø.	ø.	0.0 0.			ø.	0.0	0.0	ě.	-ē.	ě.
0716182	20.4 112.4									•										
		45	29.7 112.1	45.	25.	e,	0.0	0.0	0.	-0.	0.	0.8 0.		-0.	8.	6.0	0.0	8.	-0.	0:
071700Z	20.8 111.2	35	20.0 110.0		22.	е.	8.8	9.6	8.	-8.	8.	8.8 8.		-8.	₽.	0.0	0.0	Ð.	-0.	Ð.
871786Z	21.1 110.1	30	20.8 110.2	30.	19.	8.	8.8	0.0	ø.	-ø.	₽.	9.0 0.	0 0.	-8.	θ.	6.0	6.0	8.	-0.	0.
871712Z	21.3 109.2	25	21.3 109.1	30.	6.	5.	0.0	9.0	ø.	-ø.	e.	8.0 0.	0 8.	-0.	0.	8.0	0.0	8.	-0.	θ.

	ALL FORECASTS				TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48~HR	72-HR	LIRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	22.	198.	175.	224.	8.	8.	Θ.	Ð.		
AVG RIGHT ANGLE ERROR	13.	42.	93.	121.	0.	8.	0.	0.		
AVG INTENSITY MAGNITUDE ERROR	2.	10.	10.	9.	θ.	0.	0.	0.		
AVG INTENSITY BIAS	€.	-2.	-4.	-0.	0.	0.	8.	0.		
NUMBER OF FORECASTS	21	16	13	9	0	8	0	0		

12. KNOTS

DISTRICE TRAVELED BY TROPICAL CYCLONE IS 1486. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

TROPICAL STORM WINDNA FIX POSITIONS FOR CYCLONE NO. 9

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORRK CODE	COFFENTS	SITE
1	892188	7.7N 145.1E	PCN 6			PGTU
2	100000	8.8N 143.4E	PCN 6	T1.0/1.0	INIT OBS	PGTU
3	106300	7.2N 142.8E	PCN 6		MID LVL DLCC FIX	PGTW
4	100456	7.1N 142.2E	PCN 5		MID LVL ULCC FIX	PGTW
5	100600	7.6N 143.2E	PCN 6		ULCC FIX	PGTW
6	101600	7.9N 139.4E	PCH 6		ULCC FIX	PGTW
7	110000	11.4H 140.6E	PCN 6	T1.6/1.8	INIT OBS	PGTW
8	110300	11.3H 138.7E	PCH 6			PGTU
. 9	118444	11.2N 138.6E	PCN 5			PGTW
10	110600	11.4H 137.9E	PCH 6		ULAC FIX	PGTU
11	110900	11.4N 137.1E	PCN 6			PGTU PGTU
12	111600	11.5N 136.7E	PCN 6			PGTU
13	111988	11.5N 136.3E	PCN 6		BASED ON EXTRAP	PGTU
14 15	120000	11.4H 135.1E	PCN 6	T2.8/2.8 /D1.8/24RS	BHSED ON EVIKHA	PGTU
16	120300	11.7N 134.8E	PCN 6	12.0/2.0 /DI.0/2-WS	BRKS CONTINUITY	PGTW
17	120500	12.0N 133.4E	PCN 5		BRKS CONTINOTIT	PGTW
10	128614	12.1N 133.7E	PCN 5	T2.0/2.0	INIT OBS	RPMK
19	120900	12.6H 132.8E	PCN 6	12.00 0.0	1111 303	PGTU
20	121200	12.6N 132.1E	PCN 6			PGTW
21	121888	11.9N 131.1E	PCH 6			PGTU
22	122100	12.0N 130.4E	PCN 6			PGTW
23	130000	12.6N 131.7E	PCN 4	T2.5/2.5 /D8.5/24RS		PGTU
24	130300	13.2N 131.1E	PCN 4			PGTU
25	1 3060 t	14.0N 138.4E	PCN 5			PGTW
26	138681	13.9N 129.8E	PCN 5	T2.5/2.5 /D8.5/24RS		RPMK
* 27	131200	13.3N 127.7E	PCN 6		BRKS CONTINUITY	PGTU
<b>* 28</b>	131606	13.6N 126.9E	PCN 6			PGTW
* 29	131888	13.2N 126.9E	PCN 6		BRKS CONTINUITY	PGTU
36	131846	12.9N 127.4E	PCN 5			PGTU
31	132100	12.8H 127.8E	PCH 6			PGTU
32	140000	13.8N 127.1E	PCH 4	T3.8/3.8-/D0.5/244RS		PGTU
33	140300	14.6N 126.1E	PCN 4			PGTU
34	140549	14.9H 125.4E	PCN 3			PGTU
35	148549	14.9N 125.5E	PCN 3	T3.8/3.8~/D0.5/24#RS	DANES ON EVERAGE	RPM
36	141200	14.6N 124.4E	PCH 6		BASED ON EXTRAP	PGTU PGTU
37	141600	14.9N 123.8E	PCN 6		BASED ON EXTRAP	PGIW

38	141866	15.1N 123.2E	PCN 6		BASED ON EXTRAP	PGTU
39	141834	15.2N 123.1E	PCN 5		BASED ON EXTRAP	PGTU
40	141834	14.6N 123.1E	PCN 5		BASED ON EXTRAP	RPHK
41	142188	15.1N 122.8E	PCN 6		BRSED ON EXTRAP	PGTU
42	150000	15.3N 123.2E	PCN 6	T4.8/4.8-/D1.8/24HRS		PGTU
43	150300	15. IN 122.4E	PCN 6			PGTU
44	158537	15.3N 121.8E	PCN 5	T4.8/4.8-/D1.8/24HRS		RPIK
45	150600	15.5N 121.8E	PCN 6		ULCC FIX	PGTL
46	158719	15.2N 121.6E	PCH 5			RPISK
47	158988	15.4H 121.2E	PCN 6		ULCC FIX	PGTU
48	151200	16.1N 128.4E	PCH 6			PGTU
49	151688	16.5N 119.4E	PCN 6		BASED ON EXTRAP	PGTU
50	151866	16.5H 118.7E	PCN 6			PGTU
51	151822	16.6H 118.4E	PCN 5			PGTW
52	151822	17.1N 118.1E	PCN 5			RPHK
53	152004	16.7H 117.6E	PCN 5			RPISK
54	152186	17.6N 117.4E	PCH 6		BASED ON EXTRAP	PGTU
55	160000	18.8N 116.7E	PCN 4	T2.5/3.8 /U1.5/24IRS		PGTW
56	16 <b>6388</b>	18.8N 115.8E	PCN 4		EXP LLCC	PGTU
57	160600	19.1N 115.8E	PCN 4		EXP LLCC	PGTW
58	168787	18.9N 114.6E	PCN 3	T2.5/3.8-/01.5/25HRS		RPHK
59	160707	18.6N 114.2E	PCN 3	T3.8/3.8 /S8.8/26HRS		RODN
68	160900	19.4H 114.8E	PCN 6			PGTU
61	161200	28.6N 114.1E	PCN 6			PGTU
62	161688	20.1N 112.4E	PCN 6			PGTU
63	161952	28.44 111.6E	PCN 6			RODH
64	162100	20.4H 111.1E	PCN 6			PGTU
65	178666	28.3N 111.8E	PCN 4	T1.0/1.5 /U1.5/24RS	EXP LLCC	PGTU
66	176386	20.3N 110.9E	PCN 6			PGTU
67	178688	28.8N 118.5E	PCN 4		EXP LLCC	PGTW
68	178655	21.1H 189.9E	PCN 3	T1.5/2.8-/U1.8/24HRS	EXP LLCC	RPHK
69	176900	21.3N 189.8E	PCN 6			PGTW
78	171200	21.9N 189.4E	PCN 6			PGTU
71	171600	21.3N 187.9E	PCN 6			PGTU
72	171948	21.1N 100.0E	PCN 5			RPMK

#### AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700HB HGT	08S MSLP	MAX-SFC- VEL/BRG								eye Shape	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	120500	11.5N 133.7E	788MB	3110	1000			648	30	330	68	5	40			+18 + 9 + 9	3
2	130036	12.6N 130.7E	7 <b>98</b> 18	3071	1001	25 100	68	168	27	120	46	18	10			+10 +10	4
3	130782	13.8N 138.2E	700MB	3071	1000	25 240	110	878	38	278	120		-				5
4	138858	13.4N 129.9E	1500F1		1998	25 268	98	320	29	260	90	18	38			+24 +23 +21 29	5
5	132186	13.8N 127.4E	1500FT		994	25 120	20	128	49	838	68	6	4				6
6	132233	13.6N 127.1E	1588FT		991	35 828	98	340	50	270	128	3	4			+24 +26 29	6
7	148654	14.6N 125.3E	700MB	2986		65 290	38	899	68	330	30	5	10				7
8	140815	14.5N 125.8E	788MB	2978	986	78 238	15	020	53	268	58	A	8			+12 +17 +18	7
9	152249	17.6H 116.9E	788118	2988	988	40 890	60	188	49	188	98	4	2			+12 +14 +18	9
18	160110	18. IN 116.6E	70018	2991		58 188	6	150	52	188	6	4	2				9
11	160639	18.6H 114.8E	760MB	2972	985	55 140	35	200	31	138	65	18	10			+13 +15 +12	18

#### RADAR FIXES

FIX NO.	TIPE (2)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASUAR TODEF	COMENTS	RADAR POSITION	SITE UMD NO.
1 2 3 4 5 6 7 8 9	142300 142340 150100 150230 150600 150730 150000 150930 150910 150910	15. IN 122.6E 15. IN 122.9E 15. IN 122.8E 15. IN 122.4E 15.6N 121.5E 15.5N 121.5E 15.5N 121.6E 15.6N 121.6E 15.7N 120.9E 15.7N 120.9E	LAND LAND LAND LAND LAND LAND LAND LAND	GOOD FAIR FAIR	CIRCULAR ELLIPTICAL ELLIPTICAL	4 10 18	1088/ 42904 119/3 42706 108// 43012 108// 42812 108// 42712 108// 42722	28 DEG SPRL OVRLY STHRY EYE 188 PCT CI DIA 58 KMS EYE 188 PCT CI DIA 58 KMS EYE 188 PCT CI DIA 58 KMS EYE 188 PCT CI DEN N DIA 35 KMS EYE 78 PCT CI OPEN N DIA 35 KMS EYE 88 PCT CI OPEN S DIA 35 KMS EYE 88 PCT CI DIA 28 KMS EYE 68 PCT CI DIA 25 KMS  AXIS 28/18	16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 15.2N 128.6E 15.2N 128.6E 15.2N 128.6E 15.2H 128.6E	98321 98321 98321 98321 98321 98321 98321 98327 98327 98327
12 13 14	151835 151288 152388	15.9H 120.7E 16.1H 120.2E 17.8H 116.3E	LAND	POOR	CIRCULAR	18	110// 43210	EYE 100 PCT EL AXIS 35/15 KMS	15.2N 128.6E 16.3N 128.6E 16.3N 128.6E	98327 98321 98321

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TYPHOON ANDY BEST TRACK DATA

	BEST TRAC	K LIARN ING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
HD/DA/HR	POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
872112Z	11.1 147.8 25	0.0 0.0 00. 0.	0.0 0.8 08. 0.	8.8 8.8 88. 8.	0.0 0.0 00. 0.
872118Z	11.3 146.3 38	0.8 0.8 00. 0.	8.8 0.8 00. 8.	0.0 0.0 88. 0.	0.0 0.0 0. <del>-0</del> . 0.
872286Z	11.4 145.6 35	8.8 8.8 88. 8.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
8722862	11.7 144.9 35	11.8 145.8 35. 8. 8.	13.1 142.9 55. 92. 8.	14.6 139.6 65. 183. 0.	15.7 135.7 75. 24715.
872212Z	12.2 144.9 48	12.5 144.3 58. 48. 18.	14.1 141.6 55. 168. 8.	14.7 137.5 65. 256. 8.	14.9 133.4 75, 352, -15,
072218Z	11.8 145.1 46	12.0 143.8 58. 97. 18.	14.3 148.5 68, 192. 6.	14.8 136.4 65, 285, -5.	14.9 132.3 75. 32115.
872388Z	11.9 144.5 45	12.1 144.5 45. 12. 8.	12.5 142.1 50. 7215.	14.8 139.3 68. 14228.	14.9 135.1 75. 28415.
072306Z	12.1 144.1 55	12.0 144.0 50. 05.	12.8 141.4 60. 885.	14.2 138.1 65. 28225.	15.8 133.3 75. 284. ~28.
872312Z	12.4 143.7 55	11.8 143.8 55. 36. 8.	12.1 142.7 55. 14610.	13.0 139.6 65. 30625.	13.3 135.4 75. 36325.
872318Z	12.8 143.4 68	11.0 143.3 55. 605.	12.3 142.8 68. 17918.	13.1 130.9 65. 33125.	13.2 134.7 75. 41838.
872488Z	13.2 143.1 65	13.1 142.9 65. 13. 8.	14.8 148.6 75. 725.	15.7 136.5 85. 1815.	16.2 132.3 98. 25318.
872486Z	13.7 142.6 65	13.7 142.5 65. 6. 8.	15.1 139.8 75. 12615.	15.8 135.7 85. 28810.	16.3 131.6 98. 20518.
072412Z	14.4 141.9 65	14.2 141.9 65. 12. 8.	15.7 130.9 00. 13910.	16.5 134.7 85. 19215.	17.3 130.5 90. 26925.
872418Z	15.2 141.3 78	15.8 141.8 78. 21. 8.	16.2 136.0 85. 1205.	16.9 132.8 90. 17815.	17.5 128.2 95. 22925.
072500Z	16.8 148.6 88	15.9 140.7 88. 8. 0.	10.2 137.2 90. 131. 0.	18.8 132.9 95. 2065.	20.1 128.3 189. 21228.
072586Z	17.2 139.7 98	16.4 148.4 85. 635.	18.7 137.5 95. 248. 0.	19.3 133.3 116. 295. 16.	19.8 129.1 185. 32215.
872512Z	18.6 138.6 98	10.2 139.3 90. 42. 0.	21.1 135.2 100. 243. 0.	22.2 129.3 110. 1805.	24.3 123.8 115. 164. 8.
<b>0</b> 72518Z	10.2 136.7 90	18.8 137.7 98. 67. 8.	20.8 132.6 185. 181. 0.	22.7 128.2 118. 19218.	24.5 123.6 115. 164. 10.
872688Z	10.3 134.9 90	18.2 135.2 98. 18. 8.	18.9 129.3 1 <b>66</b> . 24. 6.	28.8 124.4 185. 4915.	22.9 120.8 90. 335.
<b>072686</b> Z	18.4 133.3 95	10.0 133.1 95. 27. 0.	19.9 128.2 185. 13. 5.	21.8 123.2 110. 3710.	24.5 118.8 70. 7315.
872612Z	10.4 132.0 100	19.8 131.3 100. 46. 0.		21.2 121.1 110. 915.	23.2 117.3 80. 127. 10.
872618Z	10.0 130.4 105	18.8 138.7 185. 17. 0.	19.9 125.2 115. 465.	21.6 128.3 95. 91. 10.	23.8 116.4 <b>50</b> . 1425.
87278eZ	19.3 129.3 100	19.2 128.8 188. 29. 8.	21.2 123.9 100. 4620.	23.6 119.3 85. 8510.	0.6 0.0 00. 0.
072786Z	19.7 128.1 100	19.6 128.2 100. 8. 8.	21.4 123.4 100. 1320.	23.6 119.4 85. 38. 8.	0.0 0.0 0. <del>-0</del> . 0.
872712Z	20.2 126.9 115	20.3 126.9 115. 6. 0.	22.9 122.6 110. 665.	24.9 118.2 58. 6228.	8.0 8.0 8. <b>-8. 8.</b>
872718Z	20.5 125.7 120	20.8 125.8 128. 19. 0.	23.2 121.4 100. 515.	24.9 117.0 35. 8320.	0.0 0.0 90. 0.
872 <del>888</del> Z	20.8 124.6 120	21.8 124.5 128. 13. 8.	23.5 120.2 80. 4115.	0.0 0.0 00. 0 <i>.</i>	0.0 0.0 0O. O.
872986?	21.3 123.6 120	21.4 123.4 120. 13. 0.	23.8 119.1 88. 445.	0.0 0.0 00. 0.	3.0 0.0 0. <del>-0</del> . 0.
872812Z	21.8 122.6 115	21.8 122.6 115. 0. 0.	23.5 119.5 70. 56. 0.	0.0 0.0 00. P.	0.B 0.B 00. D.
8729182	22.4 121.7 185	22.2 121.9 105. 16. 0.	24.8 119.1 78. 79. 15.	0.0 0.0 00. D.	0.0 0.0 0. <b>-0.</b> 0.
8729 <b>86</b> Z	23.0 120.7 95	23.6 121.0 95. 17. 0.	25.7 118.0 30. 505.	0.0 0.0 00. 0.	8.8
072906Z	23.8 119.9 85	23.8 120.0 85. 5. 0.	8.0 6.0 90. 8.	9.0 0.0 00. 6.	0.0 0.0 0. <del>-0.</del> 6.
072912Z	24.4 119.2 70	24.4 119.2 70. 0. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 0. <b>-0</b> . 0.
872918Z	25.2 110.5 55	25.2 118.6 55. 5. 8.	0.0 0.8 00. 0.	0.0 0.0 00. 0.	0.0 Q. <del>0</del> 00. Q.
873888Z	26.4 117.5 35	26.9 117.1 35. 32. 8.	0.0 0.0 00, 0.	0.0 0.0 00. 0.	6.8 <b>6.6 68.</b> 6.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER			
	WRNG	24-HR	48-HR	72-HR	URNG	24十級	48-HR	72-11
AVE FORECAST POSIT ERROR	24.	99.	160.	231.	24.	99.	168.	231.
AVG RIGHT ANGLE ERROR	14.	50.	196.	144.	14.	50.	106.	144.
AVG INTENSITY MAGNITUDE ERROR	1.	6.	12.	15.	1.	6.	12.	15.
AVG INTENSITY BIAS	0.	-5.	-11.	-13.	0.	-5.	-11.	-13.
NUMBER OF FORECASTS	32	28	23	19	32	28	23	19

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2872. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

#### TYPHOON ANDY FIX POSITIONS FOR CYCLONE NO. 10

	TIME	FIX	ACCEN	NUMBER CORE	0010471177	
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1 2		12.2N 144.7E 12.6N 144.2E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
3	212100	10.8H 145.7E	PCN 6		ULAC FIX	PGTU
5	228413	12.6N 145.9E 11.7N 145.2E	PCN 6 PCN 5	T2.5/2.5	INIT OBS	PGTW PGTW
* 6	220900	12.7N 144.3E 11.6N 143.0E	PCN 6	T2.5/2.5	ULCC FIX	PGTU PGTU
	221288 221688	12.1N 144.3E 11.8N 143.9E	PCN 6 PCN 6		ULCC FIX ULCC FIX	PGTU PGTU
<b>= 18</b>	221650	11.5N 143.2E 11.5N 142.9E	PCN 5 PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
* 12	222100	11.1N 142.9E	PCN 6		ULCC FIX	PGT⊎
14	230386	11.9N 144.6E 11.6N 145.8E	PCN 4 PCN 6			PGTU PGTU
		11.9N 144.4E 12.1N 144.8E	PCN 5	T3.5/3.5 /D1.8/25HRS T4.8/4.8	INIT OBS	PGTW RPHK
17	238988	12.8N 144.8E 12.8N 143.5E	PCN 6		ULCC FIX	PGTU PGTU
19	231688	11.7N 143.4E 11.8N 144.1E	PCN 6		ULCC FIX	PGT⊌
21	231800	11.7N 143.7E	PCN 5		ULCC FIX ULCC FIX	PGTW PGTW
23	232188 248888	11.7N 143.0E 12.9N 143.0E	PCN 6		ULCC FIX ULAC FIX	PGTU PGTU
25	240300 240530	13.5N 142.8E 13.8N 142.2E	PCN 6 PCN 5	T4.8/4.8 /D8.5/24MRS	ULCC FIX	PGTU PGTU
26	240600 240900	13.8H 142.1E	PCN 6			PGTU PGTU
28 29	241200	14.44 141.4	PCN 6		ULCC FIX	PGTU
30	241886	14.7H 140.2E	PCN 6		ULCC FIX ULCC FIX	PGTU PGTU
32	242100 250000	15.2H 140.2E 15.9H 140.9E 16.3H 140.3E	PCN 6		ULCC FIX ULCC FIX BRKS CONTINUITY	PGTU PGTU
	250386 250518	16.3N 148.3E 17.1N 139.9E	PCN 6 PCN 5	T4.5/4.5 /D8.5/24RS	ULCC FIX ULCC FIX	PGTU PGTU
35	258688	17.2N 139.8E 17.8N 139.3E	PCH 6		ULCC FIX ULCC FIX	PGTU PGTU
37	251200	17.9H 138.5E	PCN 6		ULCC FIX	PGTM
39	251866	18.1N 137.1E 19.3N 136.4E	PCN 6		ULCC FIX	PGTU PGTU
48	252198 268688	18.4H 135.6E 18.5H 135.6E	PCN 6 PCN 6		ULCC FIX	PGTU PGTU
42 43		18.9N 133.7E 18.6N 133.3E	PCN 6	T5.8/5.8-/08.5/24/RS	ULCC FIX ULCC FIX	PGTU PGTU
	268586 268688	18.5N 132.9E 18.5N 133.2E	PCN 5	T5.8/5.8-/08.5/24RS T5.5/5.5	INIT OBS ULCC FIX	RPHK PGTU
46	268988	18.6H 132.2E	PCN 6		ULCC FIX	PGT⊌
47 48	261688	19.5N 132.0E	PCH 2 PCH 2			PGTU PGTU
58	262188	18.9H 138.1E 19.3N 128.9E	PCH 2 PCH 6			PGTU PGTU
		19.4N 129.3E 19.5N 128.7E	PCN 6 PCN 6			PGT⊍ PGT⊍
53	270688	19.6N 128.8E 19.6N 127.8E	PCH 2	T6.8/6.8-/01.8/25HRS T6.8/6.8 /D8.5/25HRS	EVE DIO 18MM	PGTU RPHK
55	278988	28.6N 127.7E	PCN 2 PCN 2	10.070.0 750.3723mc3	EIE DIN 10MI	PGT⊎
57	271888	20.4H 125.9E 20.4H 125.5E	PCN 6			PGTU PGTU
59	272100	28.1N 125.4E 28.5N 125.8E	PCN 5 PCN 6			RPHK PGTW
68 61	200000 200300	20.5N 124.8E 21.4N 123.6E	PCN 6 PCN 6			PGTU PGTU
62 63		21.5N 123.6E 21.5N 123.8E	PCN 6	T6.8/6.8-/58.8/244RS T6.8/6.8-/58.8/244RS		PGTU RPHK
64 65	298988	21.5N 122.5E 21.7N 122.8E	PCN 6 PCN 6			PGTU PGTU
66 67	291688	22.4H 122.1E	PCN 6		ULCC FIX	PGT⊎
68	281989	22.6N 121.8E 22.6N 121.5E	PCN 6 PCN 3		ULCC FIX	PGTU RPMK
69 78	282 186 298888	22.6H 121.3E 22.6H 120.9E	PCN 6		ULCC FIX UI.CC FIX	PGTU PGTU
71 72	290300 290611	23.4H 120.1E 23.5H 119.4E	PCN 6 PCN 5	T4.5/4.5-/WI.5/25HRS	ULCC FIX	PGTU PGTU
73 74	290612 290900	23.9N 119.5E 23.6N 119.4E	PCH 5 PCH 6	T4.5/4.5 /UI.5/24RS		RP16K PGTU
75	291200 291600	24.5N 119.1E	PCH 6			PGTU
76 77	291888	24.9H 118.6E 25.3H 118.4E	PCH 6 PCN 6			PGTU PGTU
78 79	291857 292168	25.7N 118.4E 25.9N 117.7E	PCN 5 PCN 6			PGTU PGTU
00 01	300000 300300	26.6H 117.4E 25.2H 117.6E	PCH 4 PCH 6			PGTU
82	300600	26.3H 116.0E	PCH 6			PGTW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	7881B HGT	08S MSLP	MAX-SF VEL/8R			-FLT- /VEL/			ACC NAV/		EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
,	228223	11.5N 145.2E	7881B	3868	995	68 85	0 30	270	50	228	40	5	3			+15 + 7	1
2	228538	11.7N 144.9E	700MB	3046		58 16	0 15	060	40	298	25	5	2			+15 +16 + 8	1
3	221981	11.8N 145.8E	700118	2992				166	48	358	38	6	6				2
4	222158	11.9N 144.7E	700MB	2998	985	48 36	8 15	238	33	328	21	6	5			+15 +17 +11	2
5	239799	12.8N 143.9E	700MB	2941		65 12		358	33	220	120	10	4				3
6	230943	11.8N 143.8E	700MB	2986	986			228	45	150	110	18	6			+12 +14 +11	3
ž	232002	12.5N 143.2E	700MB	3983				238	62	120	40	6	Ř				4
ė	232218	13.1N 143.2E	700MB	2982	986	75 15	8 68	110		340	68	5	5			+14 +18 +12	4
ğ	248513	13.6N 142.6E	788MB	2938	982	48 85	D 50	120	58	050	42	5	3			+16 + B	5
10	248835	13.9N 142.4E	786MB	2941		65 13	B 75	220	56	120	58	5	3			+12 +19	5
11	242256	15.8N 140.9E	780(18	2879	976	98 86		198	88	868	40	5	5	ELL IPTICAL	15 10 040	+18 +15 +11	6
12	252138	18.2N 135.4E	788MB	2836	978	100 36		160		898		10	ž			+12 +14 +12	ē
13	268023	18.4N 134.BE	700MB	2789		65 29		688		839	112	18	3			+15 +11	8
14	261216	18.4N 132.BE	78818	2654	949			160			40	10	ě	CIRCULAR	10	+11 +16 +12	ğ
15	270011	19.3N 129.3E	788MB	2611	944	100 36	9 78	100		350	68	.,	3	CIRCULAR	`,	+15 +16 +14	10
16	270921	20. IN 127.4E	788HB	2353	915	110 32		868	188		98	Ā	4	CIRCULAR	,	+14 +19 +15	ii
	2.032.	201111 1211-2			7.0	02	•				,,	٠	7	CINOCLIAN	•		

## RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE	RADOB-CODE ASUAR TODEF	COMMENTS	RADAR POSITION	SITE
	-									
	232135	11.9N 143.2E	LAND	POOR					13.6N 144.9E	91218
,	248445	13.5N 142.7E	LAND	FAIR					13.6N 144.9E	91218
3	248545	13.6N 142.7E		FAIR					13.6N 144.9E	91218
4	248635	13.8N 142.8E		FAIR					13.6N 144.9E	91218
5	248735	13.6N 142.6E		FAIR					13.6N 144.9E	91218
6	288288	21.2N 124.2E					22815 53219		24.3N 124.2E	47918
7	280300	21.3N 124.6E	LAND				55//4 52714	OPEN NU	24.3N 124.2E	47918
8	298488	21.2N 123.6E					61111 53012		25.1N 121.6E	46696
9	288488	21.2N 123.7E					20874 52619		24.3N 124.2E	47918
10	288588	21.2N 123.7E	LAND				25/44 50000		24.3N 124.2E	47918
11	288688	21.4N 123.5E	LAND				6//// 53512		25.1N 121.6E	46696
12	280600	21.5N 123.7E					12674 50122		24.3N 124.2E	47918
13	280700	21.7N 123.4E					6//// 53216		25.1N 121.6E	46696
14	2807 <del>00</del>	21.7N 123.3E					12514 52927		24.3N 124.2E	47918
15	280800	21.5H 122.9E	LAND				10514 73015		24.3N 124.2E	47915
16	200000	21.6N 123.1E					35//2 52500		25.1N 121.6E	46696
17	288988	21.4H 122.9E					25544 72615		24.3H 124.2E	47918
18	200900	28.9N 122.2E					21538 41125		16.3N 120.6E	98321
19	281000	21.7N 122.9E					65/64 72705		24.3N 124.2E	47918
20	281000	28.7N 122.3E	LAND				21554 41610		16.3N 120.6E	98321
21	281100	21.8N 122.8E	LAND				50584 73486		24.3H 124.2E	47918
22	281300	21.8H 121.6E					21514 42814	OPEN NU	16.3H 128.6E	98321
23	281300	21.9N 122.6E					20573 4010? 10515 53105		25.1N 121.6E 24.3N 124.2E	466 <b>96</b> 47918
24	281388	21.9N 122.5E					21424 40409	F. F. I.	24.3N 124.2E	98321
25 26	281330 281400	21.1N 121.1E 22.6N 122.4E					6/// 53118	EYE ELLIPTICAL OPEN N	16.3H 120.6E 25.1H 121.6E	26521 46696
27	281488	22.1N 122.3E					10425 73110		24.3N 124.2E	47918
28	281488	22.0N 122.5E	LAND				2063/ 53108		24.6N 121.6E	46699
29	281500	22. IN 122. IE					10415 73010		24.3N 124.2E	47918
30	281600	22.2N 122.0E					6/// 53012		25.1N 121.6E	46696
31	281688	22.2N 122.BE					10693 53113		24.8H 121.6E	46699
32	281700	22.3N 121.9E	LAND				6/// 53218		25.1N 121.6E	46696
33	281700	22.3N 122.0E	LAND				20413 5340?		24.0N 121.6E	46699
34	281748	20.7N 120.8E	LAND				21575 62334	OPEN HINL	16.3N 128.6E	98321
35	281900	22.5N 121.BE	LAND				10415 73211	<del>-</del>	24.3N 124.2E	47918
36	281838	22.5N 121.7E					61038 42970		24.6N 121.6E	46699
37	281988	22.6N 121.5E					20325 73111		24.3N 124.2E	47918
38	282666	22.7N 121.4E					6///5 73112		24.3N 124.2E	47918

# SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
2	282200	22.8N 121.2E	895	818	LP10 46768	
2	298188	23.7N 128.6E	885	636	UMD 46751	
3	290600	23.8N 119.8E	665	818		
4	298988	24.2N 119.5E	879	625		
5	291500	24.8N 119.8E	965	636		
6	291988	25.8N 118.5E	838	636		
7	292166	26.3N 117.3E	636	636		

## SUPER TYPHOON BESS BEST TRACK DATA

	86	EST	TRACK			WARN		RORS		24 H	OUR F	DRECA: ERR			49 H	OUR FO	DRECA: ERRO			72 H	DUR F	DRECA:	
MD/DA/HR	POSIT		MIND	POS	TI	MIND		MIND	POS	IT	WIND	DST	WIND	P05	IT.	WIND	DST	MIND	P09	IT.	MIND	DST	LIND
872288Z	11.1 10			0.0	 		-8.	0.	0.0			-0.	ø.	0.0	6.0	ø.	-0.	0.	0.0	8.0	8.	-0.	8.
8722 <b>8</b> 6Z	11.6 16			0.0	0.0		-8.	ø.	8.8	0.0		-0.	ø.	0.0	0.0	ø.	-0.	ã.	0.0	8.0	ā.	-8.	ě.
8722122	12.2 16			0.0	0.0	ě.	-8.	8.	8.8	0.0	ø.	-0.	ě.	8.8	8.0	8.	-0.	ē.	0.0	0.0	ã.	-8.	ě.
672218Z	12.8 1				160.1	30.	88.	Ð.		156.6		93.	ě.		152.5	50.	162.		16.0	148.2	60.	233.	
072300Z	13.2 16				160.8	30.	24.	0.		157.1	45.	54.	ø.		153.2	68.	67.			150.2	70.	120.	
072306Z	13.8 15				159.8	30.	13.	0.		156.2		36.	ø.		152.4	65.	53.	-10.		148.4		236.	
872312Z	14.4 15				158.7	30.	17.	-5.		154.6		50.	-10.		150.3	65.				145.8	80.		
072318Z	15.1 15				157.8		13.	-5.		153.0		63.	-15.		149.3		192.			144.9	80.		
672486Z	15.7 15				157.1	45.	0.	-3. Ø.		153.2			-15.		148.2		315.			143.3		579.	
872486Z	15.9 15				156.8	40. 58.	48.	Ø.		151.5		159.			146.2		418.			148.4		648.	
872412Z	16.3 19				155.8	68.	21.	B.		152.6			-10.		147.6		352.			142.8		511.	
0724182	16.7 19				154.8		8.	Ø.		151.6		91.	-10.		146.4		361.	-20.		141.8	60.	516.	
872588Z	16.9 15				154.0		6.	Ø.		150.5					145.4	98.	406.	-20. -5.		141.8	95.		-13. 8.
072506Z	17.8 19				153.1	75.	13.	Ø.		149.5			-10.		144.6	95.		В.		148.8			8.
072512Z	16.8 1				152.4		18.	Ð.		149.9		181.	-5.		147.8		314.	ä.		144.9		174.	
872518Z	16.6 15				152.4	80.	19.	-5.		150.3		179.	-5.		148.0	95.		ø.		145.3		73.	- 25.
072600Z	16.2 19				151.8	90.	17.	-s. Ø.		149.5			-J.		146.4		190.	5.		143.0			
072606Z	15.8 15				151.6	98.	27.	-5.		149.3		86.	5.		146.2			5.		143.6			
072612Z	15.5 15				151.0		34.	-3. 0.		149.5		47.	10.		146.2			10.		142.8			
872618Z	15.7 15				151.5		13.	0.		149.5		29.	10.		146.2			-5.		142.8			-10.
072790Z	15.3 15				151.3	95.	19.	0.		149.5		79.	10.		146.6					143.2		486.	o.
072706Z	15.3 15				150.2		26.	ø.		147.3		186.	5.		144.1					149.3		498.	5.
872712Z	15.4 15				150.2		20. 6.	Ø.		147.3		211.	Ø.		144.1					140.3		539.	18.
872718Z	15.7 15				150.2	95.	21.	Ø.		149.4		355.			147.4					144.2			15.
072808Z	16.8 14				150.0		43.	0.		148.1			-25.		146.1		565.			142.8		643.	29.
0728862	18.2 14				148.4		29.	-5.		143.8		90.	-25.		138.8			0.		133.6			25.
872812Z	18.9 14				147.1	95.	21.	-10.		141.2		96.	-35.		136.0			0.		131.2		331.	30.
072818Z	19.8 14				145.5		6.	-10.		139.2		155.	-5.		134.1			28.		130.7			30.
872988Z	20.6 14				144.5		19.	-10.		139.2		56.	25.		134.1		236.	25.	25.5		115.	480.	30.
072906Z	21.3 14				143.6		8.	ø.		139.9		42.	25.		136.2		86.	20.		133.3		265.	25.
072912Z	22.2 14				142.4		18.	a.		138.8		21.	25.		135.4		111.	25.		132.4		364.	30.
072918Z	22.7 14				141.2		В.	5.		137.7		23.	25.		134.4			25.		131.9		526.	50.
8738882	23.3 14			23.3		138.	ø.	ø.		137.2		42.	5.		135.5	100.	76.	15.		135.8	80.	265.	30.
873886Z	23.9 13				139.4		13.	5.		136.7		66.	10.		135.0		107.	15.		138.0	70.	278.	30.
8738122	24.7 13				130.9		8.	5.		136.2		65.	10.		134.9	90.	144.	28.	0.0	8.8	8.	-0.	Ð.
073018Z	25.2 13				137.9		11.	Ð.		135.9		66.	10.		135.1		249.	35.	0.0	0.0	e.	-0.	Ð.
873188Z	25.7 13				137.8		13.	В. В.		136.2		114.	20.		135.0	98.	478.	49.	0.0	0.0	e.	-0.	8.
873106Z	26.2 13				137.4		22.	5.		136.2		149.	20.		134.9	85.	493.	45.	0.8	0.0	8.	-0.	e.
873112Z	27.1 13				137.7		16.	5.		135.5		153.	20.	0.0	0.0	0.	-8.	-O.	0.0	0.0	0.	-8.	8.
0731122 073110Z	27.8 13				137.1	95.	8.	5. 5.		135.3			35.	0.0	8.0	8.	-0.	Ð.	8.8	8.8	0.	-0.	0.
0801002	29.2 13				136.B	95.	13.	Ð.		137.5	65.	185.	15.	0.0	8.6	Ð.	-0.	Ø.	0.0	0.0	8.	-0.	0.
080 1002 080 106Z	38.7 13				136.8	80.	19.	Ð.		137.5	68.	198.	28.	0.0	8.8	Ø.	-0.	8.	8.0	8.0	0.	-0.	Ð.
0801122	32.9 13				136.8	78.	8.	Ø.	9.8	139.8	ъп. О.	-0.	20.	6.6	8.8	Ð.	-0.	e. 8.	8.8	0.0	Ø.	-0.	Ð.
0801122	36.3 13				137.2		13.	10.	0.0	8.8		-0. -0.	Ø.	6.0	8.0	8.	-0.	Ø.	8.8	0.0	Ð.	-0.	8.
080200Z	38.7 13				136.7		24.	6.	0.0	0.0		-0. -0.	Ð.	0.0	0.0	0.	-0.	8.	0.0	8.8	e.	-0.	8.
888286Z	40.0 13				135.5		6.	ø.	8.0	8.8		-0. -0.	ø. Ø.	0.0	9.0	0.	-e.	0. 0.	0.0	0.0	e.	-A.	e.
0002002	40.0 1.	33.3	-40	37.7	133.3	40.	٥.	0.	0.0	0.0	о.	-0.	0.	9.0	0.6	о.	⊸6.	6.	3.6	3.6	٠.		٥.

	ALL	FORECAS	TS		TYPHO	DNS WHI	.E OVER	35 KTS
	LIRNG	24-HR	48-HR	72-HR	URNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	18.	121.	267.	396.	16.	121.	267.	396.
AVG RIGHT ANGLE ERROR	13.	64.	122.	198.	12.	64.	122.	198.
AVG INTENSITY MAGNITUDE ERROR	2.	13.	17.	20.	2.	13.	17.	20.
AVG INTENSITY BIRS	-0.	2.	1.	1.	-0.	2.	1.	1.
NUMBER OF FORECASTS	43	39	35	31	48	39	35	31

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2811. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

#### SUPER TYPHOON BESS FIX POSITIONS FOR CYCLONE NO. 11

	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMENTS	SITE
1	211600	18.5N 164.8E	PCN 6			PGTU
2	211888	18.9H 164.8E	PCN 6		ULCC FIX	PGTW
3	212100 220000	10.5N 164.1E 11.1N 163.7E	PCN 6 PCN 6			PGTW PGTW
5	229413	11.8N 162.7E	PCH 5	T1.5/1.5	INIT OBS	PGTW
¥ 7	220600	12.2N 162.3E	PCN 6			PGTU
* 8	22 <b>8900</b> 2212 <b>80</b>	12.9N 160.8E 12.7N 160.6E	PCN 6		ULCC FIX	PGTW PGTW
* 9	221688	11.8N 168.9E	PCN 6		ULCC FIX	PGTIJ
* 18	221658 221 <b>888</b>	12.2N 160.2E	PCN 5 PCN 6		ULCC FIX ULCC FIX	PG (W PGTW
* 11 * 12	222100	12.0N 160.3E 11.8N 160.4E	PCN 6		ULCC FIX	PGTU
13	238666	13.4N 160.2E	PCN 6			PGTU
14 15	238481 238988	14.3N 159.8E 13.8N 159.4E	PCN 5 PCN 6	T2.5/2.5+/01.8/24#RS		PGTU PGTU
16	231600	15.1N 150.2E	PCN 6		ULCC FIX	PGTU
17	231645	15.1N 157.9E	PCH 5			PGTU
18 19	231988 232186	15.1N 157.6E 15.3N 157.3E	PCN 6 PCN 6		ULCC #12	PGTU PGTW
28	240000	15.6N 157.2E	PCN 6		ULCC FIX	PGTU
21	248348 248688	16.6N 157.1E	PCN 5	T3.5/3.5 /D1.8/24HRS		PGTU
22 23	248988	16.7N 156.9E 16.2N 156.2E	PCN 6		ULCC FIX	PGTU PGTU
24	241200	16.7N 155.4E	PCN 6			PG TU
25	241600	16.7N 155.1E	PCN 2 PCN 4		EYE DIA 30NM	PGTW PGTW
26 27	2418 <b>00</b> 2421 <b>0</b> 0	16.9N 154.8E 16.9N 154.5E	PCh 4			PGTU
28	250000	16.9N 154.1E	PCN 2			PGTW
29 30	250300 250336	16.9N 153.4E 16.9N 153.1E	PCN 2 PCN 2	T4.5/4.5 /D1.8/24HRS		PGT⊌ PGT⊍
31	250600	17.8N 153.1E	PCN 2	14.3/4.3 /91.0/24m3		PCTU
32	250900	16.9N 152.BE	PCN 2			PGTW
33 34	251200 251600	17.8N 152.7E 16.9N 152.3E	PCN 2 PCN 2			PGTW PGTW
35	251800	16.9N 152.2E	PCN 2			PGTW
36	252100	16.6N 152.0E	PCN 2			FGTU PGTU
37 38	260000 260300	16.4M 151.9E 16.3M 151.8E	PCN 2 PCN 2			PGTU
39	260506	16.8N 151.7E	PCN 1	T5.5/5.5 /D1.8/25HRS		PGTW
48 41	268586	15.9N 151.7E	PCN 1 PCN 2	T6.0/6.0	INIT OBS	RPMK PGTU
42	268688 268988	15.9N 151.7E 15.7N 151.7E	PCN 2			PGTU
43	261200	15.7N 151.4E	PCN 2			PGTU
44 45	261600 261800	15.7N 151.6E 15.8N 151.5E	PCN 2 PCN 2			PGTU PGTU
46	262100	15.7H 151.4E	PCN 2			PGTU
47	270000	15.6N 151.8E	PCN 2			PGTW
46 49	278388 278688	15.4N 150.6E 15.4N 150.6E	PCN 2 PCN 2	T6.5/6.5-/01.0/25HRS		PGTW PGTW
50	270900	15.4N 150.5E	PCN 2			PGTU
51 52	271200 271600	15.4N 150.3E	PCN 2 PCN 2			PGTW PGTW
52 53	271739	15.7N 158.2E 15.8N 158.4E	PCN 2			PGTU
54	271800	16.0N 150.2E	PCN 2			PGTU
55 56	272100 200000	16.5N 150.8E 17.1N 149.7E	PCN 2 PCN 2			PGTW PGTW
* 57	200442	18.2N 149.3E	PCN 2	T6.8/6.8-/W8.5/23HR\$		PGTU
58	290680	10.3N 148.4E	PCN 2			PGTU
59 68	288988 281288	19.0N 147.8E 19.0N 146.9E	PCN 2 PCN 2			PGTU PGTU
61	291686	19.3N 146.0E	PCH 2			PGTU
62 63	281727 291988	19.6N 145.6E	PCN 1 PCN 2			PGTU PGTU
64	282188	19.6N 145.6E 19.8N 145.1E	PCN 2			PGTU
65	290000	20.4N 144.7E	PCH 2			PGTU
66 67	298388 298429	21.6N 144.8E 21.2N 143.6E	PCN 2 PCN 1	T6.5/6.5 /D8.5/24HRS		FGTU PGTU
68	298688	21.5N 143.4E	PCN 2	TOTAL COLOR POPULATION		PGTU
69	290900	21.9N 143.6E	PCH 2			PGTU
78 71	2912 <b>88</b> 2916 <b>88</b>	22.3N 142.2E 22.5N 141.5E	PCN 2 PCN 2			PGTU PGTU
72	291715	22.5N 141.2E	PCH 1			PGTW
73	291866	22.5N 141.2E	PCN 2			PGTW PGTW
74 75	292166 366666	23.1N 140.9E 23.3N 140.2E	PCN 2 PCN 2			PGTU

76 77 78 79 80 81 82 83 84 85 86 87 88 99	300407 300600 300900 301200 301200 301703 301805 302100 310300 310540 310900 311260 311600	23,7N 139,9E 23,8N 139,6E 24,3N 139,3E 24,3N 139,9E 25,1N 139,2E 24,8N 138,1E 25,6N 138,1E 25,2N 138,1E 25,2N 138,0E 25,5N 137,7E 26,1N 137,7E 26,0N 137,7E 27,3N 137,7E	PCN PCN PCN PCN PCN PCN PCN PCN PCN PCN	1 T6.8/6 2 2 2 2 1 2 2 1 2 2 1 7 1 7 7 7 7 7 7 7		3.5/24R:								한 원 원 원 원 원 원 원 원 원 원 원 원 원 원 원 원 원 원 원					
92 93 94	311888	27.9N 137.3E 29.8N 136.9E	PCN 4	4										P	GTW GTW				
95 96	018388 018536 811288	29.9N 136.0E 30.9N 136.9E 33.1N 137.5E	PCH !	5 T4.8/5	.e-/u	1.5/24HR	5							P	GTW GTW GTW				
97 98	811688 820888	34.3N 137.1E 38.4N 136.6E	PCN (	5										P	GTU GTU				
99 100	020300	39.2N 135.6E 39.4N 136.6E	PCN (						INIT	085				Pi	STW KSZ				
101	020524	48.2N 134.4E	PCN	5 . T4,5/4	1.5				INIT	085				Ri	DDH				
						•	IRCR	AFT F	IXES										
FIX	TIME	FIX	FLT	788HR	0 <b>9</b> S	MAX-SFC-	-LIND	MAX-	FLT-LM	-LIND	ACC	:RY	EYE	EAE O	RIEN-	EY	e TEt	r (c)	MSN
NO.		POSITION	ĹVL	HGT		VEL/BRG/												DP/SST	NO.
1	222157	13.8N 161.2E			1991	25 368	15	140	10 170								+12 +	<b>₽</b>	1
3	230853 232128	14.2N 159.8E 15.4N 157.4E	700H	2970	998 985	50 186	66	919 229	40 280 57 180	88	8	3 5				+12	+14 1[4 +	<b>⊦10</b>	2 3
4 5	240039 241909	15.7N 156.8E 16.7N 154.7E	786M	2031	978	50 100 ?0 320	90 39	2 <del>00</del> 300	54 100 70 200	50	10	5 18	CIRCULAR	35		+11	+13 +	<b>.</b> 8	3 4
6 7	258686 258853	17.0N 153.1E 16.8N 152.5E			961	88 948	30	120 190	67 <b>848</b> 72 128			4 15	CIRCULAR	48		+12	+17 +	+10	5 5
8	252129 268718	16.4N 152.8E	70011	2711	955	78 388 58 188	45 5	030 829	91 300	30	6	5	ELL IPTICAL	48 25	999	+13	+19 +	+16	6
10	268988	15.7N 151.8E	788M	2661	949	30 100	•	030	86 346	30	10	3	CIRCULAR	30		+14	+20 +	<b>∤15</b>	7
11 12	261829 262 <b>043</b>	15.7N 151.3E 15.5N 151.3E		2679	954	88 368	30	016 100	B1 278		5 18	5 5	C IRCULAR	30		+15	+17 4	+14	8
13	278688 278842	15.3N 150.7E 15.2N 150.3E	700H		948	55 138 45 838	68	238	83 148 100 326	39	6	5 3	CIRCULÁR CONCENTRIC	28		+12			9
15	288232	17.6H 149.8E	70011	2641	948	90 250	48	300	64 256	40	2	4	CIRCULAR	20		+ 9	+16 +	10	18
16 17	281201 281431	18.9N 146.BE 19.2N 146.2E			927				113 148		10 18		CIRCULAR ELLIPTILA	18 15 18	aua	+11			11
18	281909	20.0N 145.4E	700H	2302			98	170	111 098	20	12	2	C IRCULAR	28	030	+11	+23 +	<b>+11</b>	12
19 20	282202 290634	20.2N 144.8E 21.4N 143.3E			901	90 360 80 270	35 12		105 348		5 5	2	CIRCULAR	20		+13	+28 +	+ 6	12 13
21	299654	21.9N 142.9E	700M	2260	964	100 360	5	316	53 186	30	5	5.	CIRCULAR	7		+12			13
22 23	292219 301234	23.2N 148.4E 24.BN 139.8E		9 2311 9 2518	914 934	125 190	10		101 050		10	10	CIRCULAR CIRCULAR	20 30		+12 -			14 15
24	302116	25.2N 137.9E	788M	2562	939			300	80 240	20	6	4	CIRCULAR	30		+14			16
25 26	310645 310912	26.8N 137.7E	700ME 700ME		956	45 290 60 090		110	76 350 92 090		10		CIRCULAR	20		+13	+17 +	<b>+16</b>	17 17
27 28	311915 312110	28.1N 137.0E			956	88 298		200 150	98 138 72 978		19	4				+13			18 18
29	810733	28.7N 136.8E 31.7N 136.8E	798HE	2823		80 290	110	160	69 060	69	16								19
30	010906	31.6N 137.6E	7 <b>901</b> 6	2029	968	45 168	120	980	98 358	90	5	18				+10	+17 +	,12	19
						F	ADAR	FIXE	s										
FIX	TIME	FIX			EYE	EYE	į	RADOF	-CODE							RAD	AR	SI.	TE
HO.	(Z)	POSÍTION	RADAR	ACCRY	SHAPE				TDDFF			(	CONTENTS			POSIT			NO.
	010000	31.6N 136.6E							,,,,,							35,3N			639
2	011300	33.6N 136.9E	LAND					55///	11111							35.2N	137.0	走 47	636

FIX HO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TODEF	CONTENTS	RADAR POSITIUN	SITE UMO NO.
3	011300 011300	31.6N 136.6E 33.6N 136.9E 33.6N 137.0E 33.6N 136.7E	LAND				5/// //// 55/// //// 5/// 51522 6/// 5///		35.3N 130.7E 35.2N 137.0E 35.3N 138.7E 34.6N 135.7E	47636 47639

# SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	1	COMMENTS
1	011500	34.4H 137.1E	068	648	UMD 47663	
5	011630	35. IN 137. IE	968	828	UMD 47635	
3	011986	36.3N 137.1E	868	646	UMD 47685	
4	812186	37.8N 136.9E	658	B25	WMO 47681	

## TYPHOON CECIL BEST TRACK DATA

	BEST TRACE	C WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
HD/DA/HR	POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
888412Z	19.0 130.9 20	8.8 8.8 88. B.	8.0 8.0 R8. B.	0.0 0.8 00. 0.	0.0 0.5 00. 0.
686418Z	20.0 127.8 20	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
886588Z	20.3 127.0 20	0.0 0.0 00. 0.	8.6 8.6 80. 0.	0.0 B.0 BD. D.	0.0 0.0 00. 0.
080506Z	28.6 126.4 25	28.8 126.6 25, 16, B.		27.0 121.3 50. 38920.	8.6 0.0 0D. B.
888512Z	20.7 125.9 25	20.0 126.2 25. 23. 0.	22.7 123.8 48. 14818.	24.4 122.1 49. 21858.	26.5 120.7 20795.
000518Z	21.6 125.2 30	21.2 125.2 30. 12. 0.	23.8 123.3 45. 15810.	24.9 121.8 35. 24575.	26.9 120.3 25. 296100.
899688Z	28.7 124.8 35	21.7 124.6 35. 61. 8.	23.7 122.4 50. 20115.	26.1 120.9 30. 31485.	20.6 119.7 20. 363180.
000606Z	20.1 124.6 45	20.1 124.6 45. 8. 8.		22.6 120.2 45. 18175.	23.1 117.2 38. 37380.
9996 12Z	20.3 124.4 50	20.6 124.0 50. 29. 0.		22.9 120.8 50. 14770.	23.5 118.4 30. 29975.
8886 18Z	28.5 124.2 55	20.5 124.3 55. 6. 0.		22.3 128.8 68. 15465.	23.2 118.8 35. 29165.
888786Z	20.7 124.8 65	20.9 123.9 65. 13. 0.	21.5 122.8 75. 3440.	22.5 120.5 55. 198. 65.	23.5 118.1 35. 31160.
888786Z	20.9 123.7 70	21.0 123.7 70. 6. 0.		22.7 128.2 55. 22855.	23.5 117.7 35. 35455.
088712Z	21.0 123.5 90	26.9 123.8 90. 18. 8.		24.1 121.9 105. 113. 0.	26.2 120.8 60. 14725.
989718Z	21.1 123.4 118	21.0 123.4 95. 615.		23.7 121.2 105. 170. 5.	25.9 120.3 55. 18920.
868868Z	21.4 123.4 115	21.3 123.2 115. 13. 0.		24.8 121.9 188. 185. 5.	26.2 122.4 88. 188. 18.
088886Z	21.7 123.3 129	21.8 123.2 120. 8. 0.		25.5 122.3 165. 89. 15.	27.1 122.9 85. 63. 28.
888812Z	22.4 123.4 120	22.2 123.4 128. 12. 8.		26.5 122.8 100. 50. 15.	28.6 123.0 80. 49 28.
8888 18Z	22.9 123.5 125	22.9 123.4 128. 65.		27.2 122.6 90. 44. 15.	29.2 122.9 80. 60. 25.
8689882	23.8 123.8 120	23.9 123.9 120. 8. 8.		31.6 124.2 80. 237. 10.	33.8 120.2 70. 323. 20.
8889862	24.6 123.8 110	24.8 123.7 115. 13. 5.		32.6 122.1 80. 285. 15.	35.5 117.6 59. 448. 0.
	25.3 123.5 105	25.3 123.0 105. 16. 0.		30.0 124.7 75. 105. 15.	31.8 126.3 65. 120. 15.
	25.8 123.3 180	25.8 123.2 95. 55.		38.2 123.3 60. 66. 5.	32.2 125.2 45. 61. 0.
	26.3 122.9 95	26.4 122.8 98. 85.		30.5 123.4 60. 60. 10.	32.1 125.3 45. 124. 0.
	26.8 123.1 98	26.8 122.8 85. 165.		31.3 124.2 50. 61. 8.	32.7 126.3 40. 2045.
081812Z	27.2 123.3 85	27.3 123.3 00. 65.		31.1 125.3 45. 625.	33.4 124.6 30. 15915.
	27.4 123.4 75	27.7 123.4 75. 18. 8.		31.3 125.2 40. 785.	33.6 124.5 30. 19310.
8811882	27.7 123.5 78	27.8 123.3 70. 12. 0.		31.8 124.2 40. 1885.	33.8 123.5 25. 21115.
	20.0 123.5 65	28.8 123.2 65. 16. 8.		31.4 124.0 35. 20410.	0.0 0.0 00. 0.
881112Z	28.4 123.9 68	28.3 123.8 68. 8. 8.		31.4 124.7 38. 26915.	8.8 0.8 88. 8.
891118Z	28.9 124.0 55	28.8 124.2 55. 12. 8.		31.7 124.5 35. 3805.	0.0 0.8 00. 0.
	29.5 124.0 58	29.8 124.0 50, 18, 0,		32.8 122.8 25. 27815.	0.0 0.0 DD. D.
	30.3 124.0 50	30.2 124.0 50. 6. 0.		34.0 125.2 25. 20215.	0.0 0.0 00. 0.
	31.1 124.1 50	31.0 124.1 50. 6. 0.		35.5 124.9 25. 17610.	8.6 8.0 80. 6.
	32.1 124.0 45	32.2 124.2 45. 12. 0.	37.7 127.0 30. 21310.	0.0 0.0 00. 0.	0.0 0.0 0. 0. 0.
881388Z	33.5 123.5 45	33.2 123.8 40. 235.	38.8 126.7 30. 19710.	0.0 0.8 00. 0.	0.0 0.0 00. 0.
	34.7 123.0 45	34.9 123.1 48. 85.	40.0 126.6 29. 20311.	0.0 0.0 00. 0.	0.0 0.0 0. 0. 0.
881312Z	35.6 122.8 45	35.6 122.0 35. 1210.	0.0 0.0 00. 0.	8.0 B.0 G0. G.	0.0 0.0 00. 0.
	36.5 122.8 40	36.8 122.8 35. 185.	8.0 0.0 00. 0.	8.0 6.0 06. 0.	0.0 0.0 0. 0. 0.
081400Z	37.3 123.8 48	37.2 122.7 40. 16. 0.	0.0 B.0 BB. B.	0.0 0.0 0e. 6.	0.0 0.0 0. 0. 0.
081406Z	37.8 123.3 48	38.2 123.8 48. 28. 8.	0.6 8.6 88. 6.	8.6 6.8 66. 6.	8.6 6.8 64. 8.
8814122	38.4 124.3 35	30.5 124.0 35. 15. 0.	0.0 0.0 00. 0.	8.0 0.0 08. 6.	0.0 0.0 0. ··· 0.
	38.9 125.6 30	38.9 125.4 30. 9. 0.	6.0 8.0 8B. 0.	0.0 0.0 00. 0.	A.O O.O OO. O.
0014195	30.3 143.6 30	30.3 123.4 30. 3. 0.	0.0 0.0 00. 0.	0.0 0.0 0. TO. O.	0.0 0.0 00. 6.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	URNG	24~HR	48-HR	72-HR	<b>URNG</b>	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	14.	102.	172.	219.	14.	102.	172.	219.		
AVG RIGHT ANGLE ERROR	9.	41.	75.	141.	9.	41.	75.	141.		
AVG INTENSITY MAGNITUDE ERROR	2.	12.	25.	36.	2.	12.	25.	36.		
AVG INTENSITY BIAS	-2.	~8.	-18.	-27.	2.	-B.	-18.	-27.		
MIMBED OF FORFCOSTS	79	77	70	22	75	77	70	22		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1665. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

## TYPHOON CECIL FIX POSITIONS FOR CYCLONE NO. 12

FIX NO.	TIME (Z)	F1X POS1TION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	841744	19.6N 128.7E	PCN 5			PG (U
2	042125 058888	28.8N 127.6E 28.4N 127.8E	PCN 6 PCN 4			PG TW WT D9
	050600	20.6N 126.5E	PCN 4	T1.5/1.5	INIT OBS	PGTU
	0509 <del>00</del> 051200	28.5N 126.4E 21.6N 125.9E	PCN 6 PCN 6			PGTW PGTW
7	<b>05</b> 16 <b>00</b>	21.3N 125.3E	PCN 6			PGTW PGTW
		21.7N 124.9E 20.5N 124.6E	PCN 6		ULCC FIX	PGTW
10 11		28.6N 124.2E 28.7N 123.8E	PCH 4 PCH 4			PGTU PGTU
12	060600	20.2N 124.4E	PCH 4	T3.8/3.8+/D1.5/24HRS		PGT⊎
13 14	868617 868988	20.0N 124.5E 20.3N 124.5E	PCN 1 PCN 4	T3.5/3.5	INIT OBS	RPMK PGTW
15	<b>0</b> 612 <b>00</b>	20.3N 124.4E	PCN 1			PGTU
16 17	061600 061000	20.3N 124.3E 20.6N 124.2E	PCN 4 PCN 2			PG (W
18	061902	28.4H 124.4E	PCN 3			PÇ TW
19 26	062188 078888	20.7N 124.0E 20.7N 124.1E	PCN 4			PG TW PGTW
21	878388	20.9N 123.9E	PCN 6	74 5 /4 5 /81 5 /3 AUDO		PGTU PGTU
22 23		20.7N 124.0E 20.7N 123.8E	PCN 1 PCN 1	T4.5/4.5 /D1.5/24HRS T5.8/5.8+/D1.5/24HRS		RPIEC
		20.9N 123.8E 20.9N 123.7E	PCH 2 PCH 2			₽GTW PGTW
	071600	20.9N 123.5E	PCN 2			PGTW
27 28		21.1N 123.4E 21.6N 123.4E	PCH 2 PCH 2			PGTW PGTW
	872188	21.1N 123.4E	PCN 2			PGTU
30 31		21.3N 123.5E 21.6N 123.3E	PCN 2 PCN 2			PGTW PGTW
32	080553	21.5N 123.5E	PCN 1	T5.5/5.5-/D1.6/24HRS		PG TU
33 34		22.2N 123.5E 22.3N 123.5E	PCN 2 PCN 2			PG TW PG TW
35	001600	22.7N 123.5E	PCN 2			PGTW
36 37	861686 661636	22.9N 123.6E 22.9N 123.5E	PCN 2 PCN I			PGTW PGTW
38	882188	23.3N 123.8E	PCN 2			PGTW
39 40	898888 898388	23.8N 123.8E 24.4N 123.6E	PCN 2 PCN 2			PGTW PGTW
41		24.7N 123.5E	PCN 1	T6.0/6.0-/D0.5/24HRS		PGTU
42 43	090900 091200	25.2N 123.7E 25.5N 123.5E	PCN 2 PCN 2			PGTU PGTU
44 45	091600 091000	25.8N 123.1E 26.1N 123.1E	PCN 2 PCN 2			PGTW PGTW
46	892188	26.2N 123.0E	PCN 2			PGTU
47 48	100000	26.3N 123.1E 26.5N 123.1E	PCN 2 PCN 2		EYE DIA 18NM	PGTW PGTW
49	166528	26.7N 123.5E	PCN 1	T5.0/5.0	INIT OBS	RODN
50 51	100529 100900	26.6N 123.2E 27.0N 123.3E	PCN 1 PCN 4	T4.5/4.5 /W1.5/23HRS		PGTW PGTW
52	101200	27.3N 123.2E	PCN 4			PGTW
53 54		27.3N 123.2E 27.4N 123.4E	PCN 4 PCN 4			PGTU PGTU
55 56	162166 116666	27.6N 123.2E 27.7N 123.4E	PCH 4 PCN 4			PGTU PGTU
57	110300	27.8N 123.4E	PCH 4		ULCC FIX	PGTL
58 59	110517 110900	27.8N 123.5E 28.2N 123.9E	PCN 1 PCN 2	T3.5/4.0 /U1.8/24HRS		PGTU PGTU
68	111200	28.5N 124.2E	PCH 4			PGTU
61 62	111600	28.6N 124.2E 28.9N 124.1E	PCN 4 PCN 6			PGTW PGTW
63	120008	29.7N 123.7E	PCN 6		ULCC FIX	PGTW PGTW
65	120300	29.8N 124.8E 30.1N 124.8E	PCN 6 PCN 2	13.5/3.5-/S0.6/25HRS	ULCC FIX	PGTU
66	120900		PCH 2			PG TU PG TU
67 68	121200 121600	31.9N 124.2E	PCN 4 PCN 4			PGTW
69 70	121800	32.1N 123.8E	PCN 6 PCN 4			PGTW PGTW
71	122100 122100	32.6N 123.7E 29.6N 123.7E	PCN 6			PGTW
72 73	130000 130300	33.5H 123.4E 33.9H 123.6E	PCN 4 PCN 4			PGTU PGTU
74	130600	34.6N 122.9E	PCN 6	T2.5/3.8 /41.8/24#RS		PGTW
75 76	130900 131200	35.1N 122.9E 35.6N 122.8E	PCN 6 PCN 6			PGTU PGTU
77	131600	36. IN 122.8E	PCN 6			PGTU
78 79	131860 132166	36.4N 122.8E 36.7N 122.9E	PCN 6 PCN 6			Pi,TU PGT⊎
88	140000	37.3N 123.5E	PCN 6		IN CC ETY	PGTW
81 82	140300 140600	37.4H 124.2E 37.7H 123.7E	PCN 6 PCN 6	T2.8/2.5 /LB.5/24HRS	ULCC FIX ULCC 37.5N 124.5E	PGTW PGTW
93 84	140900 141200	37.9N 124.0E	PCN 6 PCN 6		ULCC 37.7N 127.1E	PG TU PG TU
85	141600	30.4H 125.4E 30.5H 125.7E	PCH 6			PGTW
96	141999	38.7N 126.1E	PCH 6			PG TW

				HIRC	RAPT PIRES				
FIX NO.	TIME (Z)	FIX POSITION			MRX-FLT-LVL-UND DIR/VEL/BRG/RNG		EYE ORIEN- DIAM/TATION	EYE TEMP (	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	858837 852181 968627 968839 962285 878687 978958 87258 897258 989782 999188 99983 99218	28. 3H 126. 9E 28. 4H 124. 4E 28. 1H 124. 5E 28. 2H 124. 6E 28. 6H 124. 6E 28. 6H 123. 9E 28. 8H 123. 9E 28. 9H 123. 9E 21. 2H 123. 5E 21. 3H 123. 4E 22. 1H 123. 4E 24. 6H 123. 6E 24. 9H 123. 6E 24. 9H 123. 6E 26. 1H 123. 6E 26. 2H 122. 9E	1506FT 7001B 3001 1506FT 7001B 2853 7001B 2823 7001B 2419 7001B 2409 7001B 2369 7001B 2518	992 25 116 76 994 33 928 98 986 35 918 38 9874 60 360 26 50 100 36 98 360 7 945 100 360 7 924 50 808 96 100 100 5 920 120 170 15 925 90 160 13 935 65 100 5	318 45 238 46 959 31 380 58 1 198 28 118 38 1 198 60 64 14 268 64 198 13 1 628 75 290 28 2 10 90 180 18 90 330 13 208 180 180 180 17 2 268 181 178 15 1 58 185 688 16	7 2 10 9 ELLIPTICAL 8 5 ELLIPTICAL 5 3 5 1 CIRCULAR 12 2 10 2 CONCENTRIC 5 2 CIRCULAR	23 18 030 10 14 20 15	+25 +24 +16 +11 +11 +25 +25 +18 +14 +11 +12 +15 +14 +15 +19 +12 +12 +19 +15 +12 +28 +14 +12 +18 +15 +12 +16 +16 +11 +18 +14 +14 +18 +15	1 2 3 3 4 4 5 5 6 6 7 7 8 9 10 10
- • • •					RADOB-CODE			RADAR	SITE
NO.	TIME (Z)	FIX POSITION	RADAR ACCRY	EYE EYE SHAPE DIAM	ASUAR TODEF	CONTENTS			WHU NO.
53 54 55 56 57 58 59 68 61 62 63	990538 990698 991998	21.3H 123.4E 21.4H 123.7E 21.5H 123.4E 21.8H 123.5E 21.7H 123.4E 21.8H 123.4E 21.1H 123.4E 22.1H 123.4E 22.1H 123.4E 22.1H 123.4E 22.1H 123.4E 22.1H 123.4E 22.1H 123.5E 22.4H 123.5E 22.3H 123.5E 22.4H 123.5E 22.4H 123.6E 22.5H 123.6E 22.5H 123.6E 22.7H 123.5E 22.5H 123.5E 22.7H 123.5E 22.7H 123.5E 22.7H 123.5E 22.7H 123.5E 22.7H 123.5E 22.7H 123.5E 23.7H 123.6E 22.7H 123.6E 22.7H 123.6E 22.7H 123.6E 22.7H 123.6E 22.7H 123.6E 22.7H 123.6E 23.7H 123.6E 23.7H 123.6E 23.7H 123.7E 23.9H 123.7E 23.9H 123.7E 23.9H 123.7E 23.9H 123.9E 23.7H 123.7E 24.7H 123.7E	LAND LAND LAND LAND LAND LAND LAND LAND		6/// 53084 10714 40000 10714 40000 10714 40000 10714 43314 10614 43508 10514 40605 10514 50000 10514 50000 10514 50000 10514 50000 10624 43304 11614 50205 20733 40508 20621 43308 11614 70205 20711 43408 20621 43508 11614 79105 10614 73506 10614 73506 10614 73506 10613 70206 11613 70206 11613 70206 11613 70206 11613 70206 11613 70206 11614 53611 10913 40307 11613 70308 11614 53612 10912 40112 10912 40112 10912 40112 10912 40112 10912 40112 10913 40307 11613 70308 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11614 53612 11613 70308 11614 73512 11613 70308 11614 73512 11613 70308 11614 73512 11613 73609 11614 73507 11613 73609 11613 73507 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10514 52307 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508 10513 70508		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5. IN 121.6E 4.3N 124.2E 4.8N 121.6E 4.8N 121.6E 4.8N 121.6E 4.3N 124.2E 4.8N 124.2E 4.8N 124.2E 4.8N 124.2E 4.9N 121.6E 4.3N 124.2E 4.8N 121.6E 4.3N 124.2E 4.8N 121.6E 4.3N 124.2E 4.8N 121.6E 4.3N 124.2E 4.8N 121.6E 4.3N 124.2E	46696 417918 46696 47918 46699 47918 46699 47918 46699 47918 46699 47918 46699 47918 46699 47918 46699 47918 46699 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47918 47927 46699 47918 47927

65	<del>0909</del> 30	25.1N 123.7E	LAND	10011 40507	24.0H 121.6E	466 <b>9</b> 5
66	691666	25.1N 123.6E	LAND	11012 53500	24.8N 125.3E	4. 92.
67	091000	25.2N 123.7E	LAND	11013 73509	24.3N 124.2E	47918
68	091000	25.2N 123.7E	LAND	10932 43511	24.6H 121.6E	46699
69	09 1 <del>00 0</del>	25.2H 123.5E	LAND	6//// 53589	24.6N 121.6E	46763
78	091036	25.2N 123.6E	LAND	18822 43116	24.6N 121.6E	46699
71	691166	25.3N 123.6E	LAND	11013 73407	24.3N 124.2E	47918
72	091100	25.2N 123.5E	LAND	11013 53211	24.8N 125.3E	47927
73	8912 <b>88</b>	25.3N 123.3E	LAND	6/// 53888	25.1N 121.6E	46696
74	891288	25.5N 123.5E	LAND	10823 43111	24.9H 121.6E	46699
75	<b>091200</b>	25.4N 123.5E	LAND	11834 73367	24. M 124.2E	47918
76	891288	25.3H 123.5E	LAND	11013 53306	24.8H 125.3E	47927
77	<b>891388</b>	25.5N 123.5E	LAND	11814 73388	24.3N 124.2E	47918
78	<b>891488</b>	25.6N 123.4E	LAND	10023 43605	24.0N 121.6E	4 <del>6€</del> 99
79	<b>0</b> 91400	25.6N 123.4E	LAND	218-14 73387	24.3H 124.2E	47918
88	<b>6</b> 914 <b>06</b>	25.5N 123.3E	LAND	11013 53211	24.BM 125.3E	47927
81	<b>0</b> 9 1 5 0 0	25.6N 123.4E	LAND	21013 73305	24.3H 124.2E	47918
82	<b>09</b> 15 <b>00</b>	25.6N 123.3E	LAND	10813 53505	24.8H 125.3E	47927
63	891688	25.7N 123.3E	LAND	5//43 73104	24.3H 124.2E	47019
84	89168 <b>8</b>	25.6H 123.1E	LAND	21863 52911	24.8N 125.3E	47927
95	<b>09</b> 1630	25.9N 123.1E	LAND	10913 43309	24.0H 121.6E	46699
86	<b>0</b> 917 <b>00</b>	25.9N 123.2E	LAND	6//// 5338G	25.IH 121.6E	46696
97	<b>69</b> 1700	25.9H 123.1E	LAND	10923 40000	24.0H 121.6E	46699
88	0917 <b>00</b>	25.8N 123.1E	LAND	6///3 73207	24.3H 124.2E	47918
89	091700	25.7N 123.1E	LAND	20844 53611	24.8N 125.3E	47927
90	<b>691766</b>	25.9N 123.1E	LAND	10923 40000	24.0H 121.6E	AF 763
91	<b>691886</b>	25.9N 123.1E	LAND	6///3 73207	24.3H 124.2E	47918
92	<b>6</b> 9 18 <b>06</b>	25.9N 123.1E	LAND	10073 53311	24.8N 125.3E	17 <b>92</b> 7

# SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	MERREST DATA (NM)	CONTENTS
1	868888	20.0N 124,1E	935	848	SHIP OBSERVATION
2	140000	37.5N 123.8E	835	626	UNO 54776
3	141886	38.9N 125.2E	838	848	

TYPHOON BOT BEST TRACK BATA

	BEST T	RACK		WARNI		RORS		24 H	DUR FI	DRECA!			48 H	OUR F	ERRO	RS		72 H		ERROR	5
HQ/DA/HR	POSIT W	IND	POSIT	MIND	DST	MIND	P09	IIT	MIND	DST	MIND	P05	IT	MIND	DST	MIND	POS	iIT	MIND	DST	MIND
000000Z	7.7 153.9	20	0.8 8.8	8.	-8.	В.	8.8	6.8	٠.	-4.	٥.	8.6	9.0	٠.	-8.	8.	8.8	0.0	8.	<b>-0.</b>	8.
2300000Z	8.1 152.4	25	8.8 8.8	8.	-8.	9.	8.8	8.8	8.	<b>-8</b> .	8.	8.8	5.8	8.	-8.	8.	8.8	8.8	8.	-8.	8.
666612Z	8.7 151.4	25	0.8 8.9	8.	-0.	0.	8.8	8.8	8.	-8.	0.	0.0	8.8	8.	-8.	0.	8.8	<b>8.9</b>	a.	-0.	8.
000618Z	9.7 149.6	30	6.8 8.8	Θ.	-8.	9.	8.6	8.8	₽.	-0.	e.	0.0	6.8	8.	-8.	8.	0.8	0.0	8.	<b>-8</b> .	8.
888988Z	18.4 148.8	38	18.1 149.9	30.	67.	ø.	11.0	146.1	46.	386.	-5.	13.8	141.4	65.	351.	8.	15.8	136.7	90.	293.	15.
888986Z	18.9 147.4	35	11.2 147.5	35.	19.	0.	13.0	143.2	50.	228.	0.	14.7	138.7	70.	256.	- i 0 .	15.0	133.8	90.	201.	35.
888912Z	18.8 144.5	40	10.8 144.8	48.	10.	€.	12.2	138.7	55.	48.		13.8	134.0	75.	50.	-5.	15.8	129.5	95.	99.	50.
666916Z	11.6 142.5	45	11.4 142.3	45.	17.	0.	12.8	136.4	65.	12.	5.	14.6	131.8	86.	55.	5.	17.0	127.4	169.	116.	50.
8818 <b>88</b> Z	12.6 140.9	45	12.8 148.7	45.	12.	8.	13.3	135.0	78.	23.	5.	13.9	130.7	88.	128.	5.	15.4	126.0	188.	248.	50.
08 1 <b>00</b> 62	12.2 139.4	58	12.8 139.8	50.	26.	9.	13.1	133.9	65.	51.	-15.	13.0	129.6	88.	203.	25.	15.9	124.8	95.	277.	48.
681 <b>0</b> 12Z	12.6 138.8	55	12.3 139.3	55.	25.	6.	13.1	133.5	70.	76.	-18.	13.0	129.7	85.	227.	40.	16.2	124.2	100.	279.	48.
<b>681618Z</b>	13.8 136.4	68	12.4 136.9	55.	46.	-5.	13.8	132.2	75.	81.	0.	15.0	128.8	85.	198.	35.	15.4	125.1	100.	336.	40.
9811 <b>66</b> 2	13.3 135.4	65	13.2 135.0	65.	24.	€.	15.2	130.3	85.	89.	10.	16.4	126.4	95.	184.	45.	16.8	122.0	105.	273.	<b>4</b> 5.
881186Z	13.8 134.4	88	13.3 134.2	88.	32.	0.		130.7	166.	64.	45.	16.8	126.9	110.	190.	55.		123.2		270.	55.
<b>88</b> 11122	14.4 133.4	80	14.2 133.6	80.	17.	0.		130.3	160.	53.	55.		127.0	185.	165.	45.		123.7	110.	188.	50.
881118Z	15.1 132.6	75	14.5 132.6	65.	36.	10.	16.5	129.2	105.	189.	55.	17.6	126.2	110.	219.	58.	18.6	123.4	110.	244.	50.
88 1 28 <b>8</b> Z	15.8 131.7	75	15.0 131.0	75.	48.	0.	18.2	127.8	85.	72.	35.	28.0	123.8	98.	26.	30.	24.8	121.2	t 00 .	125.	68.
<b>00 1 206</b> 2	16.7 130.8	55	16.0 130.5	75.	45.	20.	18.7	127.2	85.	87.	38.	21.7	124.7	98.	84.	30.	25.2	123.1	100.	263.	65.
<b>69</b> 1212Z	17.4 129.9	45	17.6 130.0	45.	13.	٥.	21.2	127.2	6 <del>8</del> .	<b>86</b> .	₩.		126.2	78.	256.	10.		126.1	75.	473.	45.
<b>881218</b> Z	18.3 128.9	50	18.5 129.2	50.	21.	₽.	21.6	126.9	60.	127.	ø.		126.1	78.	385.	16.	20.2	126.2	75.	520.	55.
881386Z	19.2 127.7	50	19.2 127.8	50.	6.	8.	23.2	125.2	65.	137.	5.	27.2	124.7	75.	363.	35.	8.8	0.0	0.	~8.	8.
88 1 386Z	20.1 126.8	55	20.2 126.8	55.	6.	₽.	24.8	124.8	65.	211.	5.	29.3	124.7	75.	464.	40.	8.0	6.0	0.	<b>-0</b> .	8.
<b>88</b> 1312Z	20.6 125.8	68	21.0 125.8	60.	24.	Ø.	24.8	123.5	70.	186.	10.	28.2	122.0	75.	344.	45.	0.0	0.0	0.	-8.	0.
<b>69</b> 1318Z	21.8 124.8	68	21.7 125.1	60.	45.	0.	24.8	122.8	75.	174.	15.	27.8	121.6	78.	288.	50.	6.0	0.0	8.	<b>-8</b> .	8.
881488Z	21.2 124.8	68	21.2 124.0	60.	8.	8.		120.8	65.	88.	25.	8.8	8.8	8.	-8.	8.	8.8	8.6	8.	-8.	8.
<b>66 1 466</b> Z	21.6 123.2	68	21.5 123.2	60.	6.	8.		119.7	50.	78.	15.	8.8	8.6	6.	-e.	₽.	8.8	8.8	8.	<b>-8</b> .	8.
<b>68</b> 1412Z	21.9 122.3	68	21.8 122.5	68.	13.	0.		119.1	48.	90.	10.	0.0	8.6	€.	<b>e</b> .	0.	8.8	8.0	€.	-8.	8.
<b>6</b> 81418Z	22.2 121.4	68	22.6 121.6	68.	16.	0.	24.0	117.8	48.	81.	20.	0.8	8.8	0.	-8.	0.	8.8	8.0	0.	-8.	Ð.
081500Z	23.4 119.5	40	23.4 119.6	40.	6.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	€.	-0.	0.	0.0	0.0	€.	-0.	€.
<b>0</b> 815 <b>0</b> 62	23.9 110.5	35	23.8 118.6	35.	8.	٥.	8.6	0.0	0.	-0.	0.	0.0	8.6	0.	-8.	0.	0.0	0.0	0.	-8.	ø.
661512Z	24.5 117.9	30	24.4 117.7	30.	12.	8.	8.6	0.0	8.	-8.	0.	0.0	6.8	€.	~0.	0.	0.0	0.0	0.	-0.	0.
0015182	25.2 117.1	20	8.8 6.8	€.	-0.	ø.	8.8	0.0	8.	-0.	٠.	8.6	8.0	θ.	-8.	0.	8.8	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35						
	URNG	24-HR	48-1根	72-HR	LIRNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	22.	188.	218.	262.	21.	109.	287.	229.			
AVG RIGHT ANGLE ERROR	17.	68.	172.	200.	17.	73.	157.	180.			
AVG INTENSITY MAGNITUDE ERROR	1.	16.	29.	47.	1.	16.	26.	46.			
AVG INTENSITY BIAS	1.	13.	27.	47.	1.	13.	25.	46.			
NUMBER OF FORECASTS	27	24	28	16	25	22	18 .	14			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2435. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 13. KNOTS

TYPHOON DOT FIX POSITIONS FOR CYCLONE NO. 13

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	871988	7.7N 156.7E	PCN 6			PGT⊌
2	872188	6.8N 153.5E	PCN 6			PGTU
3	000000	8.8N 153.2E	PCH 4	T1.8/1.8	INIT OBS	PGTU
4	000411	7.8H 152.6E	PCN 3			PGTW
5	000600	8.5N 152.8E	PCN 6		ULCC FIX	PGTW
6	000900	8.9N 151.7E	PCN 6		ULCC FIX	PGTU
* 7	861866	9.1H 148.4E	PCH 6			PGTW
* 8	002100	18.8N 147.6E	PCH 6			PGTW
,	890000	18.3H 149.9E	PCH 4	T2.8/2.8 /D1.9/24HRS		PGTW
10	896386	18.9H 149.3E	PCH 6			PGT⊎
11	898688	11.4H 147.7E	PCH 6		BASED ON EXTRAP	PGTW
12	090900	11.4N 146.1E	PCN 6		ULCC FIX	PG TU
13	<b>891286</b>	11.9H 144.9E	PCN 6			PGTW
14	99.1688	11.6N 142.7E	PCN 6			PGTW
15	<b>09</b> 1644	11.5N 142.9E	PCN 6			PGTW
16	891888	11.6N 142.4E	PCN 6			PGTW
17	892100	11.7N 141.5E	PCN 6			PGTW
10	100000	11.4H 148.7E	PCN 6	T2.5/2.5 /D0.5/24根\$		PGTU
19	100300	11.6H 140.8E	PCN 6		ULCC FIX	PGT⊌
20	100529	12.0H 139.4E	PCH 5			PGTU
21	100900	12.2N 138.9E	PCN 6			PGTW
22	101200	12.4H 138.6E	PCH 6			PGTW
23	101600	12.5N 136.6E	PCN 6			PGTW
24	18186)	12.7N 135.8E	PCN 6			PG TM

25	101017	17 M 176 7E	PCN 5		PGTU
25 26	101813	13.0N 136.3E 13.1N 135.8E	PCH 5		PGRU
27	110000	13.3N 135.6E	PCN 6	T3.5/3.5 /D1.8/24HRS	PGTU
28	110300	13.5N 135.2E	PCN 6	13.3/3.3 /D1.0/EWR3	PG FW
29	110500	13.8N 134.5E	PCN 1		PGTW
38	110900	14.1N 133.7E	PCN 4		Pr: flu
31	111200	14.2N 133.3E	PCN 6		PGTU
32	111688	14.4N 132.6E	PCN 6		PGTW
* 33	111800	14.1N 132.1E	PCN 6		PGIIJ
34	112100	14.9N 131.2E	PCN 6		PGTU
35	120000	15.2N 131.1E	PCN 6	T4.5/4.5-/D1.8/24HRS	PGTU
36	126366	15.9N 131.2E	PCN 6	1-10-110-0-110-0-1110	PGTVI
37	120600	16.7N 131.2E	PCN 6		PGTW
* 38	120647	16.3N 129.6E	PCN 5		Retak
39	120900	16.0N 131.3E	PCN 6		PG (W
40	121200	17.2N 129.8E	PCN 6		PG FW
41	121600	17.6N 129.4E	PCN 6		PGTM
42	121750	18.8N 128.9E	PCN 5		PRITU
43	122100	18.9N 128.5E	PCN 6		PGTS
44	130000	19.0N 127.7E	PCN 6		PGTU
45	130300	19.6N 127.5E	PCH 6	T3.0/3.5 /W1.5/27HRS	PG (W
46	130600	20.4N 126.8E	PCN 6		PG TU
47	130900	21.0N 126.5E	PCN 6		PGTW
48	131200	21.3N 126.3E	PCN 6		PGTW
49	131600	21.7N 125.5E	PCN 6		PGTW
50	131000	21.9N 125.1E	PCN 6		PHTW
51	132100	21.7N 124.3E	PCN 6		PG ru
52	140000	21.0N 124.0E	PCN 6		PG IW
53	140300	20.9N 123.5E	PCN 6		PGIW
54	140622	21.3N 123.0E	PCN 5	T2.0/3.0 /U1.0/27HRS	PGTW
55	140900	21.2N 122.6E	PCN 6		PSTM
56	141200	21.6N 122.6E	PCN 4		PG TU
57	141600	22.8N 121.7E	PCN 4		PGTW
58	141600	22.1N 121.4E	PCN 4		PGTW
59	141907	22.2N 121.1E	PCN 4		PGTW
60	142100 150000	22.5N 120.4E	PCN 4		PGTU
61	150300	23.1N 119.7E 24.RN 118.5E	PCN 6		PG (W Pri fW
62	150610			T1.0/2.0 /U1.0 24HRS	
63 64	150900	23.4N 119.1E 24.3N 110.6E	PCN 5 PCN 6	11.0/6.0 /W1.0/24NKD	PG TW PG TW
65	151200	24.3N 110.6E 24.4N 117.7E	PCN 6		PIGTU
			PCN 6		
66	151600	25.0N 116.6E	LUM P		PGTU

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP		-SFC-		MAX-						EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) DUT/ IN/ DP/SST	MSN NO.
		7 55 7 7 7 7 7					- ONL		2110	*	- United	KING	,		511711 &	<b>51</b> (11) (11) (10)	1,01/ 11/ 2/ 001	
* 1	000210	8.4N 153.2E	1500FT		1005		626		969	38	300	143	5	10			+23 +23 +20	1
2	890 i i 8	10.8N 148.5E	1500FT		1003	48	000	50	129	41	100	100	3	8			+23 +21 +21	2
3	<del>890</del> 322	10.9N 148.1E	7 <b>99</b> MB	3084	1003		330		130	52	030	10	3	4			+13 + 7	2
4	690715	10.0N 145.9E	700MB	3087		45	940	80	100	44	030	120	6	8				3
5	091022	9.9N 144.8E	7 <b>00</b> 119	3099	1006				120	41	360	120	10	25			+11 + 8	3
6	<b>0</b> 922 <b>09</b>	11.9N 141.5E	700118	3054	998		328		199	44	320	30	10	29			+12 +12 + 9	4
7	100653	12.6N 139.3E	7 <b>0011</b> 8	2982	989	68	360	10	210	64	969	55	5	8	•		+16 +11	5
8	100831	12.5N 138.8E	700MB	2982	987	55	330	15					5	В			+13 +12	5
9	101911	13.1N 136.3E	700MB	2900					338	33	230	10	7	3			+11 +15 +10	6
10	102151	13.0N 135.9E	796MB	2925	979	70	070	15	170	72	090	42	7	2	CIRCULAR	40	+12 +16 +18	6
11	110607	13.7N 134.5E	7 <b>90</b> MB	2847		90	968	14	090	72	340	27	2	2				7
12	110052	13.9N 134.0E	700HB	2844	971	55	200	11	330	61	280	11	3	2	ELL IPTICAL	10 08 020	+12 +16 <b>+18</b>	7
13	111926	14.8N 131.1E	760MB	2959					178	75	070	25	10	5				8
14	112219	15.5N 132.0E	700HB	2990	986	50	340	60	128	55	360	92	8	10			+13 +17	8
15	120901	17.2N 130.5E	700MB	3025		40	348	60	919	45	280	68	5	10			+12 +15 + 9	10
16	122819	18.6N 128.2E	700MB	3002		40	100	60	010	44	260	30	10	10				11
17	122282	18.8N 127.8E	700MB	2978		30	020	120	158	49	030	90	5	8			+18 +16 +11	11
19	130950	28.4N 126.1E	700MB	2977	986	75	100	49	120	81	030	45	5	8			+13 +10	12
19	131128	20.5N 125.BE	700MB	2984					699	78	340	40	10	10				12
29	131904	21.2N 124.7E	796MB	2962					110	75	340	20	8	Θ				13
21	132150	21.2N 124.4E	786MB	2980	986	50	350	20	110	55	350	94	5	8			+14 +18 + 6	13
22	140710	21.6N 123.0E	700HB	2992		50	989	30	179	46	990	60	5	3				14
23	141010	21.6N 122.8E	700MB	2977		65	010	30	110	48	010	75	5	5			+16 +17 + 8	14

RADAR FIXES

FIX NO.	TIME (Z)	F1X POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE RSWAR TDDFF	CONTENTS	RADAR POSITION	SITE UMO NO.
	898935	11.6N 145.9E 11.7N 145.2E 12.5N 143.8E	LAND	FAIR POOR POOR					13.6H 144.9E 13.6H 144.9E 13.6H 144.9E	91218

## SYNUPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
		22.8N 120.2E 23.4N 119.6E	949 949	010 015	WHD 46745, (	

TYPHOON ELLIS BEST TRACK DATA

	BEST TRACK	LIARN:	ING ERRORS	24 H	OUR FOREC	AST RORS	48 H	OUR FOR	ECAST PRORS	72 H	OUR FOREC	
MD/DA/NR	POSIT WIND	POSIT WIND	DST WIND	POSIT		TUIND	POSIT		DST WIND	POSIT	WIND DS	
881786Z	8.2 154.2 28	8.8 0.8 0.	-0. 0.	R.D 0.B	88		8.6 6.8		-a. e.	8.6 9.0	86	
891712Z	0.1 153.2 20	8.0 0.0 0.	-0. 0.	0.0 0.0	00		8.6 8.6	8.	- <b>8</b> . 8.	8.9 9.6	90	
8817182	B. 1 152.1 20	8.8 8.8 8.	-8. 8.	0.0 0.0	80		8.8 6.8		0. O.	0.9 9.0	90	
881888Z	8.8 151.1 25	8.8 8.8 8.	-B. B.	0.0 0.0	88		8.8 6.6		-0. 0.	0.6 9.6	06	
881886Z	8.1 150.0 25	8.8 8.8 8.	-0. B.	8.8 8.8	B8		0.0 0.0	e.	-8. 0.	0.8 9.8	า ฮ	
8818122	8.2 148.8 25	8.6 8.6 8.	-A. B.	8.8 8.8	00		6.6 0.6		-B. A.	0.0 0.0	90	
881818Z	8.5 147.4 30	8.8 148.2 25.	515.	9.8 146.2	49. 286		10.0 144.3	50.3	Ø629.	12.6 141.5	79. 326	25.
881988Z	8.8 146.1 38	9.1 146.1 38.	18. 8.	10.0 143.5	50. 98	5.	12.2 148.3	60. 1	2215.	12.8 136.7	79. 198	30.
881986Z	9.4 145.0 30	9.7 144.5 30.	35. 8.	11.2 141.1	50. 54		11.9 137.7		5015.	11.9 134.0	75. 313	30.
	18.2 143.9 35	18.2 144.2 35.	18. 8.	11.9 140.9	50. 55	15.	13.4 137.4	65. 1	A229.	14.2 133.9	88. 221	35.
	18.9 142.9 45	10.8 143.2 35.	1910.	12.5 139.8	55. 42	15.	13.7 135.6	70. 1	4325.	14.8 131.7	85. 295	35.
882888Z	11.5 142.0 55	11.6 142.8 58.	65.	13.2 139.1	60. 64	15.	14.5 134.2	75. 1	7425.	15.8 138.2		40.
<b>882886</b> Z	12.1 141.0 60	12.2 141.2 55.	135.	14.5 137.4	70. 59		15.4 133.8	<b>85.</b> 1	9520.	16.2 129.5		25.
<b>9626</b> 12Z	12.6 148.3 65	12.7 148.4 68.	85.	14.7 136.8	75. 72		15.9 133.6		4625.	17.4 131 2		
<b>0820</b> 10Z	13.2 139.7 70	13.3 139.4 60.	1910.	15.4 136.2	75. 65	20.	16.9 133.2		473A.	18.2 139.6	105. 202	10.
	13.8 139.8 75	13.0 139.0 65.	010.	15.2 136.5	75. 55		16.4 134.3	90. 1	71. ··35.	17.2 132.5	19'i. 343	10.
	14.3 138.4 88	14.1 138.3 70.	1310.	15.5 136.1	8 <b>8.</b> 72		16.7 133.9		1130.	17.5 132.1		
	15.0 138.0 85	14.9 137.7 78.	18 15.	17.8 135.2	98. 42		18.2 133.6		87 <b></b> 20.	19.8 139.8		
	15.6 137.3 95	15.0 137.3 75.	1220.	17.8 134.8	<b>95</b> . 41		19.8 132.4		19. <b>-10</b> .	21.9 130.3		
	16.1 136.7 100	15.0 136.0 95.	195.	17.2 135.1	125. 121				47. 15.	20.7 131.2		
	16.7 136.1 105	16.8 136.1 110.	6. 5.				20.6 132.2		86. 30.	22.7 131.0		
	17.4 135.8 115	17.4 135.8 128.	0. 5.				21.9 132.5		50. 35.	24.1 131.3		
	10.3 135.3 120	19.2 135.4 125.	0. 5.	20.9 134.1	140. 82		22.8 132.7		58. 35.	25.2 132.0		
	19.2 134.9 125	19.2 135.1 125.	11. 0.	21.7 133.6	135. 82		23.8 132.2		48. 38.	25.9 131.1		
	20.2 134.3 125	20.2 134.4 125.	6. 0.	22.7 132.8	139. 64		25.2 131.5		98. 30.	27.5 139.6		
	21.2 133.9 120	21.2 134.1 128.	11. 0.	24.5 132.2			27.0 130.9		32. 30.	29.2 130.1		
	22.1 133.4 115	22.1 133.4 120.	Ø. 5.	25.3 131.8	120. 0		27.9 130.6 32.4 130.6		12. 30. 1810.	39.2 129.5 39.8 133.6		
	22.9 132.9 115	23.0 132.9 120.	6. 5.	26.7 131.0	100. 30							
	23.7 132.4 110	23.7 132.4 115.	0. 5.	27.3 130.4	95. 42		34.1 130.8		6415.	0.8 0.0 8.8 9.9	00 00	
	24.5 132.1 105	24.4 132.1 105.	6. 0.	28.1 130.4	95. 42 98. 69		34.4 130.8 35.5 131.2		2310. 1810.	8.8 9.9 9.8 6.6	U0	
	25.3 131.8 100	25.4 131.7 188.	0. 0. 175.	29.2 130.2 31.2 129.4	90. 69 65. 157		30.2 132.3		1810. 7620.	0.8 8.0	00	
	26.1 131.2 100 26.7 130.8 95	26.2 130.9 95. 27.0 130.0 90.	175. 185.	31.2 129.4 32.8 129.6	65. 151		0.0 0.6	8.	-0. O.	0.6 A.A	90	
	27.4 138.5 98		85.	31.5 129.7	68. 91		0.0 0.0	0.	-0. 0. -0. 0.	8.6 9.8	B0	
	28.1 138.6 98	27.3 130.4 85. 28.2 130.4 80.	85. 121 <b>0</b> .	31.4 129.8	55. 106		9.0 9.0		-0. 0. -8. 8.	0.0 0.8	6e	
	28.8 130.6 95	28.2 130.4 80.	85.	33.2 138.4	50. 66		0.0 0.0		-0. 0. -0. 0.	9.8 0.8	0e	
	29.7 130.8 80	29.8 138.6 75.	125.	35.1 130.2	45. 95		0.0 0.0		-0. D.	0.0 0.0	A6	
	38.7 131.2 75	30.7 131.1 70.	55.	36.3 131.0	45. 139		0.0 0.6		~0. O.	8.8 8.8	9e	
	31.9 131.8 65	31.0 131.0 65.	6. <b>0</b> .	0.0 0.0	00		9.0 0.8	9.	-B. B.	0.0 0.0	96	
	33.6 132.1 60	32.7 132.0 60.	54. 0.	8.8 8.8	00		0.0 0.0		-B. B.	6.8 8.8	00	
	35.7 132.0 45	35.1 132.0 50.	36. 5.	0.0 0.0	00		9.8 8.8		-B. B.	8.6 6.6	06	
	38.5 131.9 40	38.7 131.8 48.	13. 0.	0.0 0.0	88		0.0 0.0		-8. 0.	8.8 0.8	Ae	
JUL , 126	ww. 3 13113 40	ww., 191.0 <b>40</b> ,	0.	J.6 9.6	JU		3.0 0.0		J. J.	3.0 0.0		. ••

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	14.	76.	171.	263.	12.	76.	171.	263.		
AVG RIGHT ANGLE ERROR	8.	42.	81.	153.	8.	42.	81.	153.		
AVG INTENSITY MAGNITUDE ERROR	5.	13.	23.	20.	5.	13.	23.	28.		
AVG INTENSITY BIAS	-3.	-4.	-5,	3.	-3.	-4.	-5.	3.		
NUMBER OF FORECASTS	36	32	26	22	33	32	26	22		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2648. NM

AVERPCS SPEED OF TROPICAL CYCLONE IS 11. KNOTS

# TYPHOON ELLIS FIX POSITIONS FOR CYCLOHE NO. 14

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	178484	9. IN 154.8E	PCN 5	T1.8/1.8		PGTW
ž	171688	7.7N 152.8E	PCN 6			PGTU
3	171649	7.5N 152.7E	PCN 5			PGTW
4	172188	7.1N 151.7E	PCN 6			PGTM
5	180000	7.5N 151.6E	PCN 6		BASED ON EXTRAP	PGTU
6 7	180300	8.0N 150.9E 8.1N 150.2E	PCN 6	T1.5/1.5 /D0.5/23HRS	BASED ON EXTRAP	PGTW PGTW
á	180900	8.1N 149.5E	PCN 6		ULCC FIX	PGTU
Š	181288	B.6N 149.4E	PCN 6		0000 717	PGTU
10	181688	8.3N 148.1E	PCN 6			PGTM
11	181637	8.2N 148.1E	PCN 5			PGTW
12	101800	8.2N 148.0E	PCN 6			PGTU
13	182100 190000	8.2N 147.6E	PCN 6			PGTU PGTU
14 15	190300	9.4N 145.4E 9.4N 144.9E	PCN 6	T2.8/2.8 /D8.5/24HRS		PGTU
16	190522	9.5N 144.4E	PCN 5	12.0/2.0 /D0.3/24m3		PGTU
17	198688	9.5N 144.3E	PCN 6			PGTW
10	190900	10.0N 144.2E	PCN 6			PGTW
19	191200	10.5N 144.1E	PCN 6			PGTU
20	191600	18.6H 143.1E	PCN 6			PGTU
21	191888	18.6N 142.7E	PCN 6			PGTJ
22 23	192166 200006	11.6N 142.2E 11.5N 142.4E	PCN 6 PCN 6			PGTW PGTW
24	200300	11.9N 141.7E	PCN 6	T3.5/3.5 /D1.5/24HRS		PGTW
25	200510	12.2N 141.1E	PCH 5	1310-010 - 2110- 2-410		PGTW
26	200680	12.3N 148.9E	PCN 2			PGTU
27	200900	12.5N 148.7E	PCN 6			PGTW
28	201200	12.8N 140.2E	PCN 6			PGTW
29	201680	13.3N 139.6E	PCN 6			PGTU PGTU
30 31	291998 202198	13.3H 139.2E 13.7H 139.3E	PCN 6 PCN 6			PGTW
32	210000	13.9N 139.0E	PCN 2			PGTM
33	210300	13.9N 138.7E	PCH 4	T4.5/4.5 /D1.8/24IRS		PGTU
34	218458	14.6N 138.5E	PCN 3	1-11-01-11-01-11-11-11-11-11-11-11-11-11		PGTW
35	210600	14.4N 139.6E	PCN 4			PGTU
36	210900	15.0N 138.1E	PCN 2			PGTW
37	211200	15.2H 137.9E	PCN 2		EYE DIA 20NM	PGTW
38 39	211600	15.6N 137.6E	PCN 2 PCN 1			PGTW PGTW
40	212180	15.8N 137.3E 15.8N 137.0E	PCN 2			PGTU
41	220000	16.6N 136.6E	PCN 2			PGTW
42	228388	16.6N 136.4E	PCN 2	T5.5/5.5 /D1.8/24HRS		PGTW
43	220445	16.5N 136.2E	PCN 1			PGTW
44	220900	17.2N 136.0E	PCN 2			PGTW
45	221200	17.5N 135.8E	PCN 2		CIE DIO TOUN	PGTW
46 47	221600 221730	18.8N 135.6E 18.3N 135.4E	PCN 2 PCN 1		EYE DIA 30NM EYE DIA 40NM	PGTW PGTW
49	222100	18.8N 135.2E	PCN 2		EYE DIA 35NM	PGTU
49	230000	19.2N 135.8E	PCN 2	T6.5/6.5 /D1.8/21HRS	EIE DIN GOM	PGTW
58	230300	19.7N 134.7E	PCN 2			PGTW
51	230615	28.3N 134.5E	PCN 1			PGTU
52	230900	20.8N 134.4E	PCN 2			PGTU
53	231200	21.3N 134.1E	PCN 2			PGTM
54 55	231688	21.8N 133.6E 22.3N 133.3E	PCN 2 PCN 2			PGTU PGTU
56	231900	22.2N 133.4E	PCN I			PGTU
57	231900	22.2N 133.5E	PCN I			P.PHK
58	232188	22.6N 133.0E	PCH 2			PGTW
59	240000	23.8N 132.8E	PCN 2	T6.8/6.5 /WB.5/24HRS		PGTW

68	240300	23.2N 132.6E	PCH 2			PGTW
61	240603	23.7N 132.5E	PCN 1			PGTU
62	240900	24.2N 132.2E	PCN 2			PGTU
63	241288	24.6N 132.2E	PCN 2			PGTU
64	241600	25.2N 131.9E	PCN 2			PGTU
65	241800	25.5N 131.9E	PCH 2			PGTW
66	241848	25.3N 132.6E	PCN 1			RPIK
67	258888	26.2N 131.1E	PCN 2	T5.6/5.5 /W1.8/24HRS	EYE DIA 18NM	PGTU
68	258388	26.6N 131.8E	PCN 4	15.65 5.15 15.15 15.5	ULCC FIX	PGTU
69	258551	26.9N 138.9E	PCN 1		55.5 Y 2.1	PGTU
78	258988	27.5H 138.7E	PCN 4			PGTW
71	251288	27.6N 130.4E	PCN 4			PGTU
72	251688	27.9N 138.6E	PCH 4			PGTU
73	251836	28.1N 138.7E	PCH 3			PGTU
74	252100	28.5N 139.8E	PEN 4			PGTW
75	260000	28.BN 138.5E	PCN 4	T4.0/4.5 /W1.0/24HRS		PGTU
76	268386	29.3N 138.6E	PCN 4	14.0/4.3 /81.0/2483		PGTU
77	268539	29.9N 131.1E	PCN 3			PGTU
78	268988	30.3N 130.9E	PCN 2			PGTU
	261288	30.7N 131.2E	PCN 4			PGTW
79	261688	31.5N 131.5E				PGTU
88			PCH 4			PGTU
81	261824	31.8N 131.5E	PCN 3			PGTU
82	262100	32.5N 132.3E	PCN 6			
83	270000	33.0N 131.9E	PCN 6	T3.0/3.5 /W1.0/24HPS		PGTU
84	270300	34.9N 132.0E	PCN 6			PGTU
85	270600	36.5N 132.4E	PCN 6			PGT⊎
* 86	270900	27.9H 132.4E	PCN 6			PGTW
87	2712 <b>88</b>	38.4N 131.8E	PCN 6			PG TU

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	70018 HGT	OBS MSLP	MAX- VEL/					-LVL- /BRG/		ACI NAV		EYE SHAPE	EYE ORIEH- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	188482	8.3N 150.6E	1586FT		1003	20	150	60					15	15			+23 +23	1
2	191100	10.2N 144.4E	700HB	3055	1002				898	53	<b>8</b> 50	60	10	Θ			+11 +10 +10	3
3	191852	11.1N 142.BE	780MB	2970					838	49	300	48	10	5				4
4	192124	11.2N 142.4E	788MB	2965	987	65	<b>050</b>	30	130	74	959	40	8	3			+18 +14	4
5	200600	12.2N 141.2E	700MB	2935		55	888	14	120	63	030	49	6	4				5
6	200058	12.2N 140.8E	7 <b>00HB</b>	2925	981	30	248	28	868	66	150	30	6	5			+14 +15 +18	5
7	281958	13.3N 139.4E	700MB	2876										12				6
₿	202053	13.3N 139.3E	700MB	2847	971		080	74	160		070	60	10	10			+12 +15	6
9	210722	14.5N 138.2E	700MB	2794	965	68	<b>0</b> 80	30	968	84	320	43	8	1				7
10	210903	14.6N 138.0E	700HB	2757		50	330	90	276		170	60	8	2	CIRCULAR	30	+14 +17 +10	7
11	211901	15.8N 137.1E	700HB	2689					178		100	30		89				8
12	212050	15.8N 136.9E	7001B	2659	950	100	<b>898</b>	20	330	98	250	30	10	8	CIRCULAR	40	+12 +16	8
13	220686	16.7N 136.2E	7 <b>00118</b>	2491		75	368	100	200		120		7	3	ELL IPTICAL	40 30 090	+12 +22 + 8	10
14	22 <del>0</del> 859	17.0H 136.0E	700MB	2445	926				278	97		20	6	5	CIRCULAR	38	+13 +21 + 7	10
15	222153	18.8H 135.2E	788MB	2331		75	300	8	150		620	22	3	2	CIRCULAR	30	+18 +25 + 5	11
16	238112	19.5N 134.0E	7 <b>00</b> MB	2366		115		15	310	112		20	3	1	CIRCULAR	30	+17 +24 + 8	11
17	238612	20.3N 134.3E	700MB	2391	920	100		15	218	112		38	5	2			+22 +15	12
10	230045	20.8N 134.3E	700HB	290 l		120	210	28	260		260	15	5		CIRCULAR	30	+15 +21 +13	12
19	24078 <del>8</del>	23.8N 132.2E	700MB	2536					210		130	30	5	5				14
20	240835	24.8H 132.2E	788MB	2538	937				290		220	25	5	5	CIRCULAR	48	+14 +15 +15	14
51	242211	25.8N 131.1E	788MB	2631			250	18	240		140	71	1	5			+17 +20 +15	15
22	258848	27.1N 130.5E	700MB	2615	946	65	130	120	220		130	198	8	15	C IRÇULAR	30	+15 +15	16
23	252151	28.7N 130.6E	700MB	2690					120		040	90	2		CIRCULAR	30	+17 +18 +15	17
24	260033	38.0H 130.8E	700MB	26 <del>88</del>		50	998	168	100	68	<b>9</b> 90	100	8	3			+17 +18	18

RADAR FIXES

FIX	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE D:AM	RADOB- ASUAR			CONTENTS	RADAR POSITION	SITE
110.	127	7031110	-		5.4.0					00.00		
1	242300	26.1N 131.1E	LAND				35/04				26.1N 127.7E	47937
2	250000	26.2N 131.0E	LAND				35//3				26.1H 127.7E	47937
3	250100	26.3N 131.1E					249/4				28.4H 129.5E	47 <b>98</b> 9 47937
4	250100	26.3N 131.1E	LAND				25//5 249/4				26.1N 127.7E 20.4N 129.5E	47989
5	250200	26.4N 131.1E 26.4N 131.1E	LAND				65/45				26.1N 127.7E	47937
6 7	250200 250300	26.5N 131.0E	LAND				22914				28.4N 129.5E	47909
ė	250308	26.5N 130.9E	LAND				20913				26. IN 127.7E	47937
š	258488	26.7N 131.8E	LAND				24914				28.4N 129.5E	47909
10	258488	26.7H 138.9E	LAND				55914				26.1N 127.7E	47937
11	250500	26.9N 131.8E	LAND				24914				28.4N 129.5E	47989
12	250500	26.9N 130.8E					65//7				26.1N 127.7E	47937
13	250600	27.8N 130.8E	LAND				22973 2 <b>0</b> 972				29.4N 129.5E 26.1N 127.7E	479 <del>0</del> 9 47937
14 15	258688 258788	26.9N 130.BE 27.1N 130.7E	LAND				22913				28.4N 129.5E	47909
16	250700	27.3N 130.8E	LAND				20913				26. IN 127.7E	47937
17	251000	27.2N 138.4E	LAND				22913				28.4N 129.5E	47909
18	251000	27.2N 138.5E					21913				26.1N 127.7E	47937
19	251200	27.2N 130.5E	LAND				22913				28.4H 129.5E	47909
28	251200	27.2N 138.4E					2///3				26.1N 127.7E	47937 47 <b>98</b> 9
21	251300	27.3N 130.4E	LAND				22913 35913				28.4N 129.5E 26.1N 127.7E	47937
22 23	251300 251400	27.3N 130.5E 27.4N 130.5E	LAND				22913				28.4H 129.5E	47989
24	251400	27.4N 130.5E	LAND				35//3				26.1N 127.7E	47937
25	251588	27.5N 130.6E	LAND				22913				28.4N 129.5E	47909
26	251500	27.5N 130.6E	LAND				35//3	70306			26.1N 127.7E	47937
27	251699	27.7N 130.6E	LAND				22913				28.4N 129.5E	47909
28	251600	27.BN 130.6E	LAND				5///3				26.1N 127.7E	47937
29	251700	27.9N 138.6E	LAND				22913				28.4N 129.5E 26.1N 127.7E	47 <b>98</b> 9 47 <b>98</b> 9
30 31	2518 <del>00</del> 2519 <b>00</b>	28.1N 130.5E 28.2N 130.5E	LAND LAND				22913 22813				26.1N 127.7E	47909
32	251900	28.2N 130.5E					54912				30.6N 131.8E	47869
33	268888	28.9N 130.6E					2291/				26.1N 127.7E	47909
34	261188	30.4N 131.1E					20542	68411			33.4N 130.3E	47886
35	261100	30.4N 131.1E	LAND				10472				30.6N 131.0E	47869
36	261300	30.7N 131.2E					20512				33.4H 138.3E	47806
37	261300	30.7N 131.3E					11432	50200			30.6N 131.0E 32.1N 131.5E	47869 47854
38 39	261355 2614 <b>00</b>	30.9N 131.3E 31.0N 131.3E		FAIR		30	12612	50116			30.6N 131.0C	47869
40	261400	30.9N 131.3E					26512				33.4N 138.3E	47886
41	261500	31.2N 131.4E					10512				39.6N 131.8E	47869
42	261500	31.2N 131.3E					20772	60125			33.4N 130.3E	47886
43	261555	31.3N 131.3E	LAND	COOD		30			MOVG	3525	32.1N 131.5E	47854
44	2616 <b>00</b>	31.4H 131.3E					10573				33.4N 130.3E	47806
45	261600	31.5N 131.4E	LAND	COOR		28	11512	20110	MOVG	7638	30.6N 131.8E 32.1N 131.5E	47869 47854
46 47	261655 2617 <b>00</b>	31.6N 131.3E 31.6N 131.4E	LAND	GOOD		26	18422	53611	LIDAC	3620	30.6H 131.0E	47869
48	261700	31.7N 131.3E					10573				33.4N 130.3E	47886
49	261755	31.8N 131.5E		POOR		5			MOVG	8338	32. IN 131.5E	47854
50	261800	31.9N 131.5E	LAND				255/2				34.3N 132.6E	47792
51	261800	31.9H 131.5E					10423				33.4N 130.3E	47886
52	261900	31.8N 131.6E					54542				30.6N 131.0E	47869 47869
53 54	2619 <b>00</b> 2619 <b>5</b> 5	31.9N 131.4E		FAIR		e	2////	,,,,,	MOVG	9726	33.3N 134.2E 32.1N 131.5E	47854
55	261988	32.8N 131.7E 32.1N 131.7E		FRIR		-	21443	66316	1 10 ₹6	<b>UJEJ</b>	33.4N 138.3E	47886
56	261988	32.1N 131.0E					10312				30.6N 131.0E	47869
57	261900	32.1N 131.5E					5////				33.3N 134.2E	47899
58	261900	32.1N 131.6E	LAND				25512	50111			34.3N 132.6E	47792
59	261955	32.3N 131.8E		FAIR		10			HOVG	0135	32.1N 131.5E	4785 .
60	278688	35.7N 132.8E					55//2				35.5N 133.1E	47791
61 62	278799	36.2N 131.8E					65//3				35.5N 133.1E 35.5N 133.1E	47791 47791
63	278888 278988	36.5N 131.8E 37.1N 131.8E					65//2 65//2				35.5N 133.1E	47791
64	271988	37.5N 131.8E					65//2				35.5H 133.1E	47791
	J. 1220	_:	<b>__</b>					-2				

# SYNOPTIC FIXES

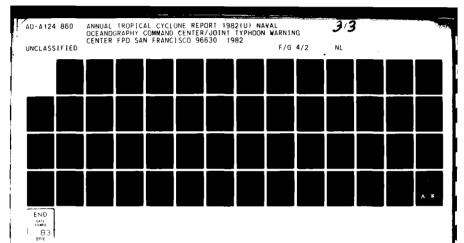
FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMENT
	262100	31.8N 131.6E 32.4N 132.8E 34.2N 132.8E	969 969 929	82 <del>8</del> 848 858	UPID 47835 UPID 47815 UPID 47755	

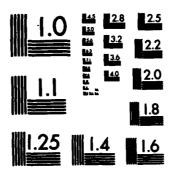
	BEST TRACK		24 F	IOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR	POSIT WIND	POSIT WIND DST	WIND POSIT	WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
082 <del>000</del> Z	11.3 124.8 20	0.0 0.0 00.	0. 0.0 0.0	00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0820 <del>06</del> Z	11.7 123.8 25	0.0 0.0 00.	0. 0.0 0.0	00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
982812Z	11.9 122.8 25	0.0 0.0 00.	0. 0.0 0.6	00. 0.	0.0 0.0 00. 0.	0.8 0.0 06. 0 <i>.</i>
082818Z	12.1 121.9 30	0.0 0.8 00.	0. 6.8 8.8		0.0 0.0 00. 0.	6.8 6.6 8. <del>-8</del> . 8.
082 100Z	12.1 121.0 30	12.2 120.2 25. 47.	-5. 12.5 117.4		13.3 114.2 <b>35.</b> 27248.	15.8 111.6 35. 45858.
082186Z	12.2 120.3 35		-18. 12.2 115.7		13.6 111.9 35. 48845.	15.8 188.2 38. 66968.
<b>6</b> 82112Z	12.3 119.7 35	12.7 118.9 30. 53.	-5. 13.1 115.7		13.8 112.1 45. 39040.	15.4 108.5 35. 64950.
0821182	12.0 119.3 40		-10. 12.8 115.6		13.3 112.8 45. 36340.	14.3 109.5 35. 68448.
082200Z	12.0 119.6 45		-15. 12.5 116.4		12.6 113.5 50. 34235.	13.2 110.3 35. 62130.
0022062 002212Z	12.2 119.5 55 12.4 119.3 65		-20. 12.8 118.1 -10. 13.2 117.6		13.3 115.3 55. 25535. 13.3 114.0 75. 30310.	14.0 112.2 58. 5055. 14.1 111.6 75. 560. 25.
082218Z	12.5 119.1 78		-10. 13.2 117.6 -10. 13.2 117.1		13.3 114.6 75. 340. 0.	13.9 112.2 70. 566. 20.
0022102 0023002	12.6 118.8 75	12.7 119.7 70. 0.	-5. 13.3 116.2		14.2 113.1 70. 448. 5.	15.1 109.8 55. 672. 10.
082306Z	12.6 118.7 80				14.9 114.2 70. 378. 15.	15.9 111.8 68. 646. 28.
0823122	12.8 118.7 85	12.8 118.8 80. 6.	-5. 13.2 117.2		13.9 114.9 70. 420. 20.	15.8 112.2 65. 666. 25.
082318Z	12.9 119.0 85	12.0 118.0 00. 13.	-5. 13.3 117.4		14.2 115.1 78. 428. 28.	15.5 112.5 65. 692. 30.
082400Z	13.4 119.3 85	13.3 119.5 80. 13.	-5. 14.9 119.8		16.1 117.6 108. 272. 55.	16.5 114.9 115. 606. 85.
882486Z	14.1 119.6 98	14.1 119.6 80. 0.	-18. 16.8 117.6		18.2 114.8 105. 391. 65.	10.6 111.6 115. 786. 98.
082412Z	15.0 119.7 85	14.8 119.8 80. 13.	-5. 17.∂ 119.€		18.7 116.7 85. 329. 45.	19.9 114.2 85. 682. 55.
<b>0</b> 82418Z	15.9 119.8 75	15.9 119.8 88. 0.	5. 18.8 118.9		19.9 116.2 88. 388. 45.	20.4 112.3 80. 856. 50.
082500Z	17.2 120.2 65	17.1 120.2 80. 6.	15. 20.2 119.1		20.7 115.8 75. 463. 45.	20.6 111.5 75. 999. 40.
002506Z	18.2 119.8 55	18.2 120.2 80. 23.	25. 20.5 118.5		21.8 116.3 60. 485. 35.	22.5 113.7 50. 936. 0.
082512Z	19.0 119.9 50	18.8 119.7 58. 17.	0. 21.6 118.6		23.2 116.0 40. 553. 10. 24.5 120.2 40. 405. 10.	0.0 0.0 d. −0. 0. 27.5 121.7 25. 585. −45.
092518Z 092600Z	19.4 120.2 58 19.7 128.5 45	19.5 120.0 55. 13. 19.8 120.4 55. 8.	5. 22.1 120.6 10. 22.5 123.1		24.5 120.2 40. 405. 10. 24.4 126.3 65. 168. 30.	27.5 121.7 25. 58545. 27.2 129.0 70. 249. 0.
082606Z	20.4 121.3 48	19.8 120.4 55. 8. 20.6 121.3 55. 12.	15. 22.5 124.4		24.8 126.9 70. 206. 20.	27.6 129.2 75. 254. 5.
8826122	21.2 121.9 48	21.1 122.1 40. 13.	8. 23.8 126.9		26.2 128.1 48. 22825.	29.8 129.9 50. 35228.
082618Z	21.5 122.9 35	21.7 123.0 35. 13.	8. 24.8 126.4		26.9 128.5 48. 24530.	30.7 130.2 50. 41510.
082700Z	21.8 124.8 38	21.8 124.0 35. 0.	5. 24.0 127.2		27.1 129.2 25. 23745.	6.6 8.6 60. 0.
002706Z	22.4 125.8 25	22.2 125.0 35. 12.	10. 0.0 0.0		0.0 0.0 00. 0.	0.6 0.0 00. 0.
082712Z	22.8 126.8 38	0.0 0.0 00.	0. 0.0 0.0	00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
<b>002710Z</b>	23.0 127.4 30	0.0 0.0 00.	0. 0.0 0.0		0.0 0.0 00. 0.	0.0 0.0 00. O.
082800Z	23.5 129.2 35	0.6 0.0 00.	0. 0.0 0.0		0.0 0.0 00. 0.	0.0 0.0 OO. O.
082806Z	24.1 130.6 50		-15. 26.9 135.7		30.2 139.6 50. 589. 5.	34.2 142.5 50. 887. 20.
082812Z	24.2   31.5 65	24.7 131.7 60. 32.	-5. 28.3 135.8		36.6 138.8 45. 893. 5.	0.0 0.0 00. 0.
882818Z	24.2 [31.9 70		-10. 27.6 135.4		33.0 137.9 55. 719. 15. 27.7 136.5 50. 389. 15.	0.0 0.0 00. 0. 33.3 139.1 35. 796. 10.
882988Z 882986Z	24.3 132.3 78	24.2 132.3 65. 6.	-5. 25.2 134.4		27.7 136.5 50. 389. 15. 28.2 136.8 50. 425. 20.	33.3 139.1 35.796. 10. 33.8 139.2 35.856. 15.
002900Z 002912Z	24.5 132.4 78 24.3 132.2 78	24 5 132.8 65. 22. 24.2 132.2 65. 6.	-5. 25.6 134.9 -5. 24.3 133.1		25.6 135.2 50. 273. 20.	29.7 138.2 30. 696. 10.
082918Z	24.0 132.1 60	24.2 132.2 65. 6.	5. 24.6 133.3		25.8 135.4 45. 316. 20.	8.8 0.8 60. 0.
003000Z	23.6 131.9 50	23.8 131.9 45. 12.	-5. 23.4 133.1		24.3 136.1 25. 366. 0.	0.8 0.0 00. 0.
083006Z	23.3 131.8 45	23.3 131.8 45. 8.	0. 22.6 132.3		0.0 0.0 00. 8.	0.0 6.0 00. 6.
0930122	23.0 131.8 40	22.9 131.0 40. 6.	0. 22.2 133.4		8.8 8.8 80. 0.	0.0 0.0 00. 0.
083018Z	23.0 132.0 48	22.8 132.1 40. 13.	0. 22.8 134.1	30. 199. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
08310 <del>0</del> Z	22.8 131.8 35	22.7 131.9 40. 8.	5. 22.1 132.3		0.0 0.0 00. 0.	0.0 6.0 00. 0.
083106Z	22.9 131.6 30	22.9 131.8 35. 11.	5. 22.6 131.5		0.0 0.0 00. 0.	0.0 0.0 00. 0.
0831122	23.0 131.1 30	22.9 131.2 30. 0.	0. 22.7 130.1		0.0 0.0 00. 0.	0.0 0.0 00. 0.
<b>083</b> 11 <b>0</b> Z	23.0 130.5 25	23.1 130.4 30. 8.	5. 0.0 0.0		0.0 0.0 00. 0.	0.0 0.0 00. 0.
0901002	23.0 129.6 25	22.9 128.3 25. 72.	0. 23.4 124.4		0.0 0.0 00. 0.	0.0 0.0 00. 0.
898186Z	22.9 128.7 28	23.1 128.8 25. 13.	5. 0.0 0.0		0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
090112Z 090118Z	22.8 127.8 28 23.0 126.8 25	23.0 120.1 25. 20. 22.9 127.2 25. 23.	5. 22.8 125.1 8. 8.8 8.8		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
0901102 090200Z	23.0 125.8 25	22.9 127.2 25. 23. 23.0 125.0 25. 6.	8. 0.0 0.0		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
090206Z	22.8 123.7 25	23.0 125.0 25. 6.	8. 8.8 8.8		8.6 8.8 B0. 0.	0.0 0.6 00. 0.
090212Z	22.5 123.4 38	22.4 123.2 25. 13.	-5. 0.0 0.0		0.8 0.8 80. 6.	8.0 0.0 00. 0.
898218Z	22.1 122.2 30	22.2 122.3 25. 8.	-5. 8.8 8.6		8.0 0.0 02. O.	0.0 0.0 00. 0.
090300Z	21.6 121.1 25	21.6 121.2 20. 6.	-5. 0.6 0.6		0.0 0.0 00. 0.	6.8 6.8 60. 6.
090306Z	20.9 119.8 20	0.0 0.0 00.	0. 0.0 0.0	00. 0.	8.0 0.0 80. 8.	0.0 0.0 00. 0.

	ALL	FORECAS	TS .		TYPHOONS UNILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	LIRNG	24-HF	48-HF	? 72-HR		
AVG FORECAST POSIT ERROR	18.	142.	384.	639.	17.	150.	376.	584.		
AVG RIGHT ANGLE ERROR	8.	89.	273.	445.	9.	109.	298.	422.		
AVG INTENSITY MAGNITUDE ERROR	6.	15.	26.	30.	7.	19.	28.	26.		
AVG INTENSITY BIAS	-2.	3.	5.	7.	-3.	2.	1.	-7.		
NUMBER OF FORECASTS	50	41	33	27	35	29	25	19		

DISTHNEE TRAVELED BY TROPICAL CYCLONE IS 2454. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS





MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

#### TYPHOONLEAVE FIX POSITIONS FOR CYCLONE NG. 15

FIX NO.	TIME (Z)	FIX FOSITION	ACCRY	DVORAK CODE	COIPENTS	SITE
* 1	200000 200300	11.2H 122.7E 11.3H 122.3E	PCH 6 PCH 6	T1.8/1.8	INIT OBS	PGTU PGTU
- 3	200600	11.6H 123.4E	PCN 6	11.001.0		PGTW
4	200652 200652	11.6N 123.7E 11.6N 123.8E	PCN 5	T1.5/1.5 T1.6/1.8	IHIT OBS INIT OBS	RP19K RODN
5 6	200032 200900	11.7N 123.6E	PCN 6	11.0/1.0	Inti Qua	PGTW
7	201200 201600	11.9H 122.7E 12.2H 121.8E	PCN 6 PCN 6			PGTW PGTW
* 9	201900	12.5H 120.7E	PCN 6			PGTW
* 16	201937 202100	11.8N 119.5E 12.5N 128.6E	PCH 5 PCH 6			RPHK PGTU
11 12	210000	12.1N 120.4E	PCN 6			PGTW
* 13 14	21 <b>0386</b> 21 <b>0680</b>	12.8N 119.6E 12.3N 119.9E	PCN 6	T2.8/2.8 /01.8/24RS		PGTW PGTW
* 15	218648	12.8H 119.4E	PCN 5	T2.8/2.8 /98.5/21HRS		RPMK
16 * 17	21 <b>0900</b> 2112 <b>00</b>	12.7N 119.7E 12.7N 118.6E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
18	211688	12.4H 119.6E	PCN 6		ULCC FIX	PGTW
19 28	2119 <b>00</b> 211925	12.4H 119.5E 11.8H 119.4E	PCN 6 PCN 5			PGTU RODH
21	212100	12.1N 119.1E	PCN 6		BRKS CONTINUITY	PGTU
22 23	22 <b>0000</b> 220300	12.1N 119.4E	PCN 6 PCN 6	T3.8/3.8 /91.8/24HRS		PGTU PGTU
24	220627	12.2N 119.6E	PCN 3			PGTU
25 26	228627 228988	12.1N 119.5E	PCH 3	T3.8/3.8+/D1.8/24HRS		RPHK PGTU
27	221266	12.6H 119.4E	PCN 2		EYE OPEN H	PGTW
28 29	2216 <b>00</b> 221 <b>000</b>	12.6N 119.2E 12.7N 119.8E	PCN 2		EYE DIA 28HM	PGTU PGTU
38	221912	12.6N 119.1E	PCN 3		ELE DOTA N	RPHK
31 32	222100 230000	12.7N 118.9E 12.7N 118.9E	PCH 2 PCH 2	T4.8/4.8 /D1.8/21HRS	EYE OPEN N	PGTU PGTU
33	230306	12.8N 118.6E	PCN 2			PGTU PGTU
34 35	238615 238615	12.7N 118.7E 12.5N 118.6E	PCN 1 PCN 1	T4.5/4.5 /D1.5/24HRS		RPMK
36	230615	12.4H 118.7E	PCH 1	T4.5/4.5+/01.5/24HRS	EYE DIA 20MM	RODN PGTW
37 38	230900 231200	12.7N 119.6E 12.9N 119.8E	PCN 2 PCN 2			PGTU
39	231600	12.9N 118.9E	PCN 2			PGTU RPHK
40 41	231751 231886	13.6N 118.8E 13.6N 118.9E	PCN 2 PCN 2			PGTU
42	231900	13.6N 119.1E	PCN 1 PCN 2			PGTU PGTU
43 44	232100 2 <b>4000</b> 0	13.1N 119.1E 13.3N 119.3E	PCH 2	T4.0/4.0 /58.0/24HRS		PGTW
45 46	240300 240603	13.7N 119.6E 14.1N 119.6E	PCN 2 PCN 1	T5.8/5.8 /D8.5/24HRS		PGTW RPIK
47	240603	14.2N 119.5E	PCN 1	1310/310 / <b>3</b> 010/ <b>2</b> 4m0		PGTU
46 49	240900 241200	14.6N 119.7E 15.2N 119.7E	PCN 2 PCN 2		EYE OPEN W	PGTU PGTU
50	241600	15.9N 119.6E	PCN 2		<del>-</del> <del>-</del>	PGTM
51 52	241888 241848	16.3N 119.4E 16.8N 119.6E	PCN 6 PCN 3			PGTU RPMK
53	242188	16.9N 119.4E	PCN 6			PGTU PGTU
54 55	250000 250300	17.1N 120.1E 17.6N 120.1E	PCN 6 PCN 6	13.5/4.0 /M0.5/24HRS		PGTW
56	250551	17.8N 119.9E	PCN 3	T3.5/4.5+/W1.5/24/RS		RPICK PGTU
57 58	250551 250900	18.2N 119.7E 18.6N 119.6E	PCN 3 PCN 6			PGTM
59	251200	19.8N 119.5E	PCN 6			PGTU PGTU
68 61	2516 <b>00</b> 251036	19.2N 119.8E 19.5N 128.8E	PCN 6 PCN 3			RPMC
62 63	251836 252188	19.5N 119.9E 19.4N 128.1E	PCN 5 PCN 6			PGTW PGTW
64	260000	19.7H 128.6E	PCN 4	T2.5/3.8 /U1.8/24RS		PGTW
65 66	2603 <b>0</b> 0 260539	20.0N 120.0E 20.2N 121.4E	PCN 4 PCN 3	T3.6/3.5 /48.5/24RS		PGTU RPIIK
67	260539	20.4N 121.4E	PCN 3	13.0/3.3 / 40.3/24463	BASED OH EXTRAP	PGTU
68 69	260900 261200	20.7N 121.5E 21.1N 121.6E	PCH 6			PGTW PGTW
78	261600	21.3N 122.2E	PCN 6			PGTU
71 72	261824 261824	21.6N 122.7E 21.4N 122.5E	PCN 3 PCN 6			RP11K PGTU
73	262100	21.5N 123.1E	PCH 6			PGTU
74 75	270000 270300	22.6H 123.8E 22.6H 124.5E	PCN 6	12.5/2.5 /S8.8/24RS		PGTU PGTU
76	278688	22.8N 125.7E	PCN 6			PGTW
77 78	271200 271800	23.6N 126.7E 22.6N 127.6E	PCN 6 PCN 4			PGTU Pu IU
79	271811	22.6H 127.2E	PCN 3		ULCC FIX	PGTU PGTU
98 18	272186 288688	23.2N 120.5E 23.6N 129.5E	PCN 6 PCN 4	T2.5/2.5+/80.0/24R\$	OCCC PIX	PGTU
82	286386	24.1N 130.2E 24.1N 130.4E	PCH 6 PCH 4			PGTU PGTU
83 84	200515 200600	24.2N 130.6E	PCH 4			PGTU

85	200900	24.3N 131.1E	PCN 2			PGTU
96	281288	24. IN 131.5E	PCN 2			PGTU
87	291688	24.5N 131.7E	PCN 2			PGTU
80	201900	24.4H 132.BE	PCN 6			PGTU
89	282186	24.4H 132.2E	PCH 6			PGTU
90	290000	24.4H 132.3E	PCN 4			PGTU
91	290300	24.6N 132.5E	PCN 6	T4.8/4.8-/D1.5/27HRS		PGTU
92	298583	24.6H 132.5E	PCN 3			PGTU
93	290600	24.5H 132.2E	PCN 4			PGTU
94	290900	24.6H 132.3E	PCH 4			PEŢU
25	291600	24.3N 132.3E	PCN 2			PGTU
96	291748	24.3N 132.3E	PCN 4		BASED ON EXTRAP	PGTU
97	292100	24.8N 132.8E	PCH 4		EXP LLCC	PGTU
90	300000	23.7N 131.9E	PCH 4			PETU
99	300300	23.5N 131.9E	PCN 4	T2.5/3.0 /J1.5/244RS		PGTU
100	300451	23.5N 131.8E	PCH 3			PGTU
101	300600	23.4H 131.BE	PCN 4			PGTU
162	300900	23.3N 131.7E	PCH 4			PGTU
183	301200	23.8N 131.8E	PCH 4		EXP LLCC	PETU
104	301600	22.9M 132.6E	PCH 4		EXP LLCC	PGTU
105	301736	23.8N 132.8E	PCH 3		EXP LLCC	PGTU
106	382188	23.0N 132.0E	PCN 4		EXP LLCC	PGTU PBTU
107	318388	22.6H 131.6E	PCN 4	TI 8.0 8 411 8.0400		PGTW
100	318628	22.9H 131.7E 23.8H 131.6E	PCN 3	T1.8/2.8 /U1.8/24RS		PGTU
189	318988	23.8N 131.5E	PCN 6			PGTU
110	311200	23.0N 131.3E	PCN 4			PETU
112	311688	23.1N 130.6E	PCN 6			PGTU
113	311800	23.1N 130.6E	PCN 4			PGTU
114	311965	23.6H 138.4E	PCN 3			RODN
115	312100	22.9N 130.6E	PCN 4			PGTM
116	010000	23.8N 129.7E	PCN 4			PGTU
117	010300	23.0N 129.2E	PCN 4	T1.8/1.8 /W1.9/24/RS		PGTU
110	010600	22.9H 129.9E	PCN 3			PGTU
119	010300	23.6N 128.6E	PCN 4			PGTU
120	811288	23.0H 125.9E	PCN 4			PGTU
121	611200	22.0H 127.0E	PCN 4			PGTU
122	011000	23.8H 127.1E	PCH 4			PG (U
123	011035	23.6H 126.5E	PCN 3			PGTU
124	626666	22.9H 125.0E	PCN 4			PGTU
125	626366	22.0H 125.1E	PCN 3	T1.8/1.8 /S8.8/24MS	EXP LLCC	PGTU
126	020556	22.5N 124.6E	PCN 3		EXP LLCC	PGTU
127	828988	22.6N 123.8E	PCN 6			PGTU
129	821200	22.5N 123.4E	PCN 6			PETU
129	821686	22.4H 122.6E	PCN 6			PGTU
130	621666	22.2M 122.3E	PCH 6			PGTU
131	821841	21.9N 122.2E	PCH 5			retu
132	822198	21.5H 121.7E	PCN 6			PGTU
133	030000	21.5N 121.1E	PCH 6		BASED ON EXTRAP	PGTW

FIX NO.	TIPE (Z)	F1X POSITION	FLT LVL	786HB HGT	08S MSLP	MAX-SFC- VEL/BRG/			-FLT- VEL/		-UND RNG	ACC NAV		EYE SHAPE	EYE DI			TEMP (I		MSN NO.
1	221032	12.3N 119.4E	7981B	2965	984	68 178	19	268	96	178	10	3	2	CIRCULAR	10		+1	12 + 8		1
2	221200	12.3N 119.2E	788HB	2938				386	55	588	28	3	2	CIRCULAR	15		+12 +3	净 + 9		1
3	222824	12.6H 119.8E	700HB	2841				140	ŧ	430	10	4	3				+14 +1	7 + 7		2
4	222259	12.7N 118.7E	788HB	2841	71	50 130	8	200	73	130	18	6	3	C IRCULAR	25		+11 +1	5 + 8		2
5	230750	12.6H 118.7E	7 <b>86</b> (5)	2746		65 278	5	010	185	270	10	5	2	ELL IPTICAL	25 15	969	+11 +			3
6	230953	12.0H 110.6E	788 <del>1</del> 8	2745	963	65 150	38	220		140		5	3	C IRCULAR	15		+12 +			3
7	232632	13.0H 119.3E	788HB	2746				938		320	10	10	3	CIRCULAR	25		+	4 +18		4
	248786	14.2N 119.7E	766HB	2739		86 616	10	100	95	616	18	2	1							5
9	248987	14.4H 119.7E	788HB	2743	963	80 850	8					2	1	ELL IPTICAL	20 15	340		8 + 9		5
10	250731	18.3H 119.8E	78 <b>0</b> 19	2998		40 838	8	248		178		4	3					5 + 9		7
11	252303	19.7H 128.5E	788HB	2992	987	78 146	15	240		140	15	15	2				+18 +1	8 + 8		
12	260718	20.7H 121.4E	70011	3035		48 898	30	160		996	25	10	5							9
13	261006	20.5H 121.6E	70019	3844	997	48 358	25	960		828	13	5	5					4 +18		
14	262237	21.6H 123.7E	790HB	3679	998	38 218	38	220		850	30	3	_1	CIRCULAR	25		+16 +1	7		10
15	278781	22.7N 125.2E	70019			15 270	38	350		278	38	20	20							11
16	201935	24.2H 132.BE	70010	2095			_	360		300	.5	5	3							12
17	202222	24.2N 132.1E	70010	2890	979	78 298	5	290		240	10	.5	5	CIRCULAR	12		+11 +			12
18	291842	24.6N 132.1E	70019	2941	982			830		310	30	10	3	CIRCULAR	13		+13 +	<b>?1</b>		14
19	291153	24. IN 132. IE	70019	2960				828		278		10	.3							14
20	292326	23.7M 132.6E	78819	3029		50 200	38	280		200	38	3	10				+11 +1			15
21	300753	23.2H 131.0E	1566FT		996	40 910	20	979	•	360	20		3						~~	16
22	300929	23.1M 131.0E	1500FT		997	48 248	15	828		249	10		•				T25 T	?7 +25	21	16
23	302020	23.0H 132.0E	70010	3060				260		140	50	Z	7				494 4	26 +24	70	17 17
24	302140 310730	22.0N 131.0E	1500FT		996	40 278	25	356		278 818	18		7				T24 T	.D 724	0	10
25		23.6N 131.5E	1500FT		999	35 990	15	138	21	210	185	19	-				+23 +2	M .25		16
26	318987	23.0H 131.4E	1500FT		373	30 150	13	130		850	3 <del>0</del>	15	3					27 +26	27	19
27	312143	23.0H 129.0E	1 <b>500</b> FT		997	25 690	•	930	21	220	3		3				723 T	.r 720	61	13

# RADAR FINES

	TIPE	FIX			EYE	EYE	RADOS-CODE		RADAR	SITE
MU.	(Z)	POSITION	RADAR		SHAPE	DIAM	ASUAR TODFF	COMENTS	POSITION	<b>WO NO.</b>
	*****						16571 52165	f	14.0H 120.2E	99426
2	232200 232300	13.3H 119.6					26511 56367		14.6H 120.2E	30426
3	242100	13.3H 119.6E					1151/ 50006		14.04 120.25	90426
3	240200	13.7N 119.4					1142/ 50107		14.8H 128.2E	99426
5	246300	13.6N 119.4					1948/ 78287	BEST TRACK 815 DEG 87 KTS	14.0H 129.2E	99426
* 6	240400	13.44 119.76					1081/ 43685	EYE 88 PCT CIR OPEN SE	16.3H 120.6E	98321
- ;	240400	13.9N 119.5					1141/ 99297	ETE BO FOT CIR OFEN DE	14.8H 128.2E	20426
* 8	246500	13.44 119.75					1881/ 43682	EYE 98 PCT CIR OPEN RE	16.3M 120.6E	98321
- 9	240600	14.1H 119.6					1141/ 00207	EIE 30 FCI CIR OFER TE	14.0H 128.2E	96426
* 18	248688	13.6N 119.7E					1199/ 43685		16.3H 120.6E	98321
* 11	248638	13.6N 119.7E					18883 43684		16.3H 120.GE	98321
12	240700	14.2N 119.6					1141/ 98287	BEST TRACK 816 DEG 87 KTS	14.0H 120.2E	98426
* 13	248788	13.7H 119.7E					18683 43685	EYE 100 PCT CIR	16.3H 120.6E	90321
* 14	240000	13.9N 119.0E					18783 48285	EYE 186 PCT CIR	16.3H 128.6E	98321
* 15	240900	14.1N 119.66					18623 43685	0.0 100 .0.	16.3M 120.6E	98321
* 16	240930	14.2N 119.00					11033 43606	EYE 90 PCT ELPTCL	16.3M 120.6E	90321
* 17	241130	14.6H 119.9E					1861/ 48186	EYE 100 PCT CIR	16.3N 120.6E	98321
18	241200	15.6H 119.0E					1141/ 00209		14.0N 128.2E	98426
* 19	241700	15.6N 119.6E					1831/ 43383		16.3N 128.6E	98321
<b>* 20</b>	241930	15.9H 119.06					1831/ 48285	EYE 188 PCT CIR DIA 11NM	16.3H 128.6E	96321
21	242030	16.1N 119.9E					1821/ 40306	EYE 100 PCT CIR DIA 9NM	16.3M 128.6E	98321
22	242835	16.0N 120.2E	LAND	POOR					15.2M 128.6E	98327
23	242166	16.3N 120.0E	LAND				1821/ 46268	EYE 188 PCT CIR DIA 9NM	16.3M 120.6E	98321
24	242138	16.2H 120.2E	LAND	FAIR	ELL IPTICAL			ELIP AXIS 26/18	15.2H 128.6E	98327
25	242208	16.7H 120.2E	LAHD				1822/ 48288	EYE 188 PCT CIR DIA SHM	16.3M 120.6E	98321
26	242230	16.8H 120.2E	LAND				1021/43600	EYE 188 OCT CIR DIA SWI	16.3N 128.6E	98321
27	258666	17.3N 128.3E					1831/ 48169	EYE 88 PCT CIR OPEN NNE	16.3H 120.6E	98321
28	250038	17.49 120.46					21985 ////	EYE ELLIPTICAL	18.3H 121.6E	98231
* 29	25003 <del>0</del>	17.6H 120.3E					4/// 43616		16.3H 120.6E	96321
* 30	256386	10.3H 120.2E			ELLIPTION		11/// 53687	EVE 188 OCT CIR DIA SMM EVE 88 PCT CIR OPEN NME EVE ELLIPTICAL	16.3M 120.6E	98321
* 31	250600	10.6N 120.16					1861/ 43485		16.3M 120.6E	98321
32	250900	18.6H 119.7E					29714 53683		18.3M 121.6E	90231
* 33	258988	10.0H 119.7E					115// 40000		16.3H 120.6E	98321
34	251130	18.6H 120.0E					10703 43600		18.3H 121.6E	96231 96321
35	251130	10.00 119.00					115// 40000		16.3M 120.GE 18.3M 121.GE	98231
36	251330	18.6N 120.1E					48483 32702		10.30 121.6E	98321
37	251330	19.1H 120.1E					1151/ 43607		16.3N 120.6E 18.3N 121.6E	98231
38	251460	18.9N 128.2E					19493 40295 11967 40108		16.3N 121.6E	98321
* 39	251400	19.3N 120.2E							22.GN 128.2E	46744
40	252200	19.64 120.4					2///1 53614		22.6N 120.2E	46744
41	261300	21.3N 121.9E					6//// 59999		22.07 120.2t	

# SYNOPTIC FIXES

FIX	TIME	FIX	INTENSITY	MERREST	CONTENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NPD	
	210000	11.2N 125.8E 12.1N 121.8E 14.8N 119.8E	826 638 606	918 875 838	uno 98555 uno 98538 uno 98426 cuel PT

# TYPHOCH GORDON

		BEST	TRACK			LIARN		RORS		24 H	DUR F	DRECA ERR			40 H	DUR F	DRECA: ERRO			72 H	DUR F	ORECA: ERROR	
HD/DR/HR	POS	17	HIND	80	RIT	MIM		WIND	POS	er T	LIND		MIND	POS	TIS	MIND		MIND	80	BIT	MIND		LIND
8827882		153.			153.8	30.	6.		17.8			-	-5.		149.3	79.		-15.		153.6		126.	
882786Z		152.			152.4	35.	6.	ă.	19.6	140.6	65.	118.	-5.	23.8	148.7	70.	75.			150.3		160.	
882712Z		151.			151.3	45.	31.	ă.	28.8	140.6	70.	125.	-5.	24.8	149.1	78.	43.	-25.	28.3			229.	-25.
8827192	17.8	151.			150.6	50.	39.	-5.	19.6	140.8	70.	123.	-18.		140.6	78.	132.	-30.	25.1			133.	-20
882869Z		158.			158.7	55.	8.	-10.		149.2	65	111.	-28.	23.2		75.	189.	-25.	26.8		85.	82.	
882886Z		150.			150.3	68.	25.	-18.		149.5	78	87.	-28.	24.7	149.4	80.	93.	-20.	27.4	149.9	85.	280.	ě.
992912Z	19.9	150.	75	28.8		78.	8.	-5.	24.8	150.6	an.	71.	-15.	27.2	151.8	90.	194.	-5.	29.6	152.4	95.	411.	18.
982918Z	21.8	158.	4 80	28.8	150.3	75.	13.	-5.	24.5	150.4	S.	87.	-15.	26.0	152.9	90.	387.	8.	20.3	157.6	98.	642.	5.
802906Z	22.2	158.	2 65	22.8	150.2	88.	12.	-5.	25.3	140.5	%.	33.	-!8.	27.2	146.2	95.	44.	10.	30.1	143.1	95.	200.	<b>5</b> .
8829 <b>8</b> 6Z	23.2	148.	9 90	23.2	150.2	85.	17.	-5.	25.9	147.8	95.	21.	-5.	20.2	144.6	90.	115.	5.	31.8	142.5	<b>50</b> .	290.	€.
<b>8829</b> 12Z		149.	3 95	24.2		100.	17.	5.		147.8		53.	30.		143.7		166.	28.	34.9	142.2		471.	5.
<b>0029</b> 10Z	24.5		100	24.9		100.	29.	8.	27.2		115.	76.	25.		143.2	95.	214.	10.	30.0	143.6	75.	643.	-10.
8838 <b>88</b> Z	25.8	148.	4 100	24.9	148.3		8.	₽.	27.1	145.6	110.	<b>69</b> .	25.		142.2	95.	237.	5.	49.4	141.2			
803006Z	25.6				147.9	90.	В.	-18.		145.3	80.	60.	-5.		141.9	79.	160.		35.6			400.	-15.
<b>0030</b> 122		147.0		26.2		98.	12.	-5.		144.7	88.	68.	-5.		141.2	78.	222.	-15.		140.4			
<b>0030</b> 10Z	26.4			26.7		85.	18.	-5.		145.1	?5.	72.	-10.		142.3	70.	162.	-15.	37.4			<b>55</b> 2.	
963196Z	26.7			26.9	146.7	65.	13.	0.	28.4	143.6	?5.	97.	-15.		140.2	78.	120.	-10.	30.8	136.5		197.	-10.
683186Z		146.			146.3	<b>85</b> .		●.		144.2	78.	73.	-20.		141.2	65.	90.	-10.		137.5		96.	-15.
<b>663</b> 112Z	27.8	145.0			145.0	98.	16.	5.		143.9	<b>95</b> .	73.	₽.	29.0	141.4	₩.	89.	5.	30.7	130.3		39.	9.
983118Z	27.8	145.		27.8		98.	11.	5.		142.0	85.	22.		20.8	140.2	<b></b>	42.	5.	31.3	138.2		130.	-5. 5.
8981862	27.8 27.8	144.		27.0	144.4	98.	5.	₽.	27.7 27.6	141.4	90. 96.	22.	10.		139.5	85.	70. 39.	10. 5.	33.2	139.2		176.	9. 9.
890106Z 890112Z		143.			143.9	98. 98.	8. 8.	e. 5.		141.2	95.	43.	15. 10.		139.7 139.7	75.	19.	3. 8.	32.6	139.2		263.	-15.
8981182		142.4			142.7	90.	17.	5. 5.	28.5	171.2	83.	49.	5.		139.7	78.	83.	-5.	34.0	139.9		203.	-28.
898288Z	27.G			27.6		88.	11.	9. 0.	28.9	138.9	65.	29.	-18.		136.6	60.	262.	-15.	20.9	134.5		813	-18.
8982862	27.6			27.6		75.	5.	8.	28.4	137.7	65.	181.	-10.		134.9	55.	458.	-15.	29.2			975.	
898212Z	27.8				140.5	75.	ĕ.				78.	91.	-5.		136.8	68.	501.	~10.	0.8	8.8		-8.	6.
898218Z		139.			139.9	75.	8.	·B.		137.3	65.	165.			134.7	55.	666.	-15.	8.8	8.6		-0.	8.
8983882	28.7			20.6		75.	12.	ē.	29.7	137.0	68.	227.	-15.	29.8		55.	766.	-10.	6.5	0.0		-0.	ě.
898386Z	29.2				139.7	78.	37.	-š.		136.2	68.	346.	-10.		133.8	50.	898.	-15.	0.0	0.1		-0.	ă.
8983122		139.			139.4	75.	12.	ě.		140.7	65.	195.	-5.	8.8	8.8	8.	-8.	Ď.	ě.ě	0.5		-0.	8.
898318Z	30.1	140		29.0		75.	28.	ě.		146.8	65.	303.	-5.	0.6	6.6	ē.	-8.	8.	8.0	8.4		-8.	ē.
898488Z	30.8	141.		31.0	141.2	75.	12.	ě.		145.7	50.	151.	-15.	8.8	9.6	ě.	-8.	Ĭ.	0.0	8.6		-0.	ě.
898486Z	31.8	142.0		32.8	142.6	78.	16.	ě.	39.7	148.2	45.	163.	-20.	0.8	6.8	ě.	-ē.	š.	8.0	8.6		-8.	ē.
8984122	32.9	144.		33.0		75.	26.	5.	8.8	8.0		-8.	ē.	0.8	6.8	ē.	-8.	8.	8.0	0.6		-ĕ.	ē.
8984182	34.3	146.3		34.3	146.4	78.	5.	ě.	8.0	0.0	ē.	-0.	ē.	0.8	0.0	8.	-8.	ě.	8.0	0.6		-8.	e.
898588Z	35.5	148.0	65	35.5	148.2	78.	10.	5.	8.8	0.0	e.	-0.	6.	8.8	6.8	8.	-8.	8.	8.8	9.6	0.	-8.	ŧ.
090506Z		149.	2 65		149.6	65.	19.	8.	0.0	0.0	ě.	-8.	ē.	0.0	0.0	ě.	-ē.	ě.	0.0	0.6	ı ë.	-0.	8.

	ALL	FORECAS	TS		TYPHO	ONS LIH	LE OVER	35 KTS
	URNG	24-HR	48-HR	72-HR	LIRNG	24-16	48-HR	72-HR
AVG FORECAST POSIT ERROR	15.	188.	214.	364.	15.	100.	214.	364.
AVG RIGHT ANGLE ERROR	11.	63.	181.	218.	11.	63.	101.	218.
AVG INTENSITY MAGNITUDE ERROR	3.	11.	12.	12.	3.	11.	12.	12.
AVG INTENSITY BIAS	-1.	-4.	-7.	-9.	-1.	-4.	-7.	-9.
NUMBER OF FORECASTS	38	34	30	26	37	34	30	26

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2014. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

# TWHOON CONTON

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	SVORAK COBE	COHENTS	SITE
1 2	251888 26888	9.0H 160.8E 10.5H 159.4E	PCH 6	T1.0/1.0	INIT ORS	PGTU
3	260600 261200	11.7H 199.6E 12.9H 196.1E	PCH 6			PGTU PGTU
5	261642	13.2H 154.8E	PCH 5			PGTU
7	262198 276668	13.9H 154.2E 14.8H 153.5E	PCN 6			PETU
9	27 <b>636</b> 0 27 <b>634</b> 5	15.5H 152.6E	PCN 6 PCN 5	12.5/2.5 /01,5/20HRS		PGTU
1 <b>0</b> 11	278600 278900	15.7H 152.2E 15.5H 151.9E	PCH 6 PCH 6	4.		PGTU PGTU
12 13	271200 271600	16.0H 151.5E 16.4H 151.1E	PCN 6 PCN 6			PGTU
14 15	271638 271888	16.2M 151.3E 16.7M 151.6E	PCH 5			PGTU PGTU
16 17	272100 200000	16.9H 151.6E	PCH 6			PGTU PGTU
18	290300 296600	19.2H 150.0E	PCN 2	T4.8/4.8 /91.5/24RS		PGT⊌
19 28	200900	19.4H 150.8E	PCH 2 PCH 5			PGTU
21 22	201290 201600	20.0H 150.5E 20.5H 150.5E	PCN 6			PGTU PGTU
23 24	281618 281888	20.5H 150.4E 21.6H 150.6E	PCN 6			PGTW PGTW
25 26	282166 29 <b>0000</b>	21.0H 150.5E 22.4H 150.3E	PCN 6 PCN 2			PGTU PGTU
27 28	298388 298583	22.7H 156.2E 23.1H 150.2E	PCN 2 PCN 1	T5.8/5.8-/91.8/24RS		PGTU PGTU
29 38	290600 290900	23.44 158.6E 23.54 149.8E	PCN 2 PCN 2			PGTW PGTW
31 32	291688 291748	24.6H 149.1E 24.7H 148.6E	PCN 4 PCN 4			PGTU
33	292100	24.8H 148.5E	PCN 2			PGTU
34 35	300000	25.9H 148.4E	PCH 4	13.5/4.5 /U1.5/24RS		PGTW
36 37	300451 300600	25.計 140.至 25.計 140.至	PCN 3 PCN 4			PGTU PGTU
39 39	300900 301200	26.8N 147.9E 26.3N 147.8E	PCN 4 PCN 2			PGTU PGTU
41	301600 301736	26.44 147.6E 26.44 147.3E	PCH 2 PCH 1			PGTU PGTU
42 43	302100 310000	26.8M 147.1E 26.7M 146.8E	PCN 2 PCN 2			PGTU PGTU
44	318388 318436	27.8H 146.6E 26.8H 146.7E	PCN 2 PCN 1	T4.8/4.8 /D8.5/24RS		PGTU PGTU
46	310600	27.1N 146.4E	PCN 2			PGTU
47	310900 311200	26.9H 146.8E 27.8H 145.7E	PCH 2 PCH 2			PGTU
49 50	31 1600 31 1800	25.0H 145.4E 27.0H 145.2E	PCN 2 PCN 2			PGTU
51 52	312100 010000	27.8H 144.6E 27.8H 144.6E	PCN 2 PCN 2			PGTU
53 54	010300 010426	26.9H 144.3E 27.8H 144.2E	PCH 2 PCH 1	T5.8/5.0-/01.8/24/RS		PGTU PGTU
55 56	010600 010500	27.2H 144.6E 26.9H 143.8E	PCH 2 PCH 2			PGTU
57 50	611290 811680	26.8M 143.3E 27.3M 142.8E	PCN 6 PCN 2			PGTU
59 68	011711 011900	27.4H 142.4E 27.7H 142.5E	PCH 2 PCH 2			PGTU
61	912100 920000	27.6H 142.1E 27.5H 141.7E	PCN 6 PCN 4		HLCC FIX	PG TU UT 29
63	828414	27.4H 141.6E	PCH 1	T4.8/4.5 /W1.8/25HRS	ULCC FIX	PGTU
64 65	020600 020900	27.5H 148.6E 27.6H 148.6E	PCH 4		ULCC FIX	PGTW
66 67	021200 021600	27.0H 140.5E 20.2H 140.6E	PCH 4 PCH 4			PGTU
6 <b>8</b> 69	021000 021041	28.44 139.8E 28.44 139.7E	PCH 4 PCH 3			PGTU
78 71	022100 030000	28.4H 139.6E 28.6H 139.5E	PCN 4 PCN 4			PETU PETU
72 73	030300 030544	28.9H 139.2E 29.1H 139.3E	PCH 2 PCH 1	T4.8/4.8 /S8.8/25HRS	EYE OPEN SU	PETU
74	030900 031200	29.4H 139.5E 29.5H 139.4E	PCN 2 PCN 4			PETU
75 76	031029	30.0H 140.6E	PCH 3		ULCC FIX	PGTW
77 78	032108 040000	30.5H 140.8E	PCH 4		ULCC FIX	PGTU
79 98	040300 040532	31.3N 142.6E 31.4N 142.6E	PCH 4	T3.8/4.8 /UI.8/24RS		PETU
01 62	040600 040300	31.4H 142.8E 32.3H 143.6E	PCH 4 PCH 6			PGTU
63		33.3H 144.5E	PCH 6			PETU

		33.6H 145.8E			 <b>₹</b>		CTU
85	841888	33.5H 146.5E	PCN 6			P	CTU
86	842188	34.0H 147.0E	PCN 6				CTU
87	850000	35.9H 147.9E	PCN 4		2.4	•	STU
88	050300	35.4H 148.4E	PCH 4	T3.8/3.8 /88.8/23HRS		P	STU
89	850688	37. IN 149.2E	PCN 4			P	CTU
90	858566	38.0H 149.5E	PCN 4			P	CTU

FIX NO.	TIPE (Z)	FIX POSITION	FLT LVL	78819 HGT	OBS MSLP	MAX-SFC VEL/BRG			-FLT-L VEL∕E			ACC HAV		EYE SHAPE		E ORI				erp (C) / BP/SST	MG.
1	262347	14.5N 153.9E	1586FT		1881	30 630	40	156	36 6		46	.2	4						+25		1
2	271826	16.2H 151.8E	70018	2998	991			330 380	34 2 45 1		26	15	3	CIRCULAR	18			+10			3
3	272335 200705	17.7H 158.7E 18.8H 158.6E	7881B 7881B	2894 2835	977 972	58 148 75 898	38 28	218		198	12 38	12	5					+ 9	413	TIE	- 3
- :	200763	19.4H 158.6E	78818	2887	312	12 636	20	168		130	25	10	3	CIRCULAR	25			+12	-10	412	- 7
	282812	21.4H 150.2E	7001B	2676	953	88 188		288	85 1		18	5	2	CIRCULAR	30			+14			
7	230644	23.3H 149.8E	70010	2629	946	100 190	28	188	99 1		30	5	4	CIRCULAR	18			+17			š
ė	290053	23.7N 149.7E	7881B	2612		80 320	68	840	71 3		30	18	4	CIRCULAR	20			+16			6
9	291986	24.7N 149.BE	78818	2607		79 278	98	388	73 2		31	5	5	C IRCULAR	40			+14			ž
18	300684	25.6N 147.9E	700fB	2616		58 139		258	79 1	158	35	5	5					• •			0
11	300032	25.7N 147.9E	700HB	2612	945	65 848	128	110	90 E	130	36	5	5	C IRCULAR	30			+13	+18	+16	ė
12	381988	26.4H 147.2E	70010	2617				190	98 6	100	57	5	3	ELL IPTICAL	45	25 3	18		+19		9
13	302043	26.6N 147.8E	788HB	2631	947	88 278	30		81 3		86	3	3	CIRCULAR	38			+16	+17	+15	9
14	318682	27.1N 146.2E	7001B	2624		65 178	65	200	76 1		68	10	5								10
15	318633	27.8H 146.1E	78818	2624	947	65 278	30	638	85 2		68	18	5	CIRCULAR	20			+14	+16	+15	10
16	311011	26.BN 145.8E	7001 <b>0</b>	2652				878	B2 3		90	2	3					_			11
17	312057	27.8H 144.7E	7001B	266 I	952			220	85 1		68	2	6	C IRCULAR	25			+15			11
18	616916	27.8N 143.8E	708HB	2657	949	65 300	120	858	68 3		70	2	5	CIRCULAR	20			+18	+18	+15	12
19	611851	27.5H 142.3E	70010	2729				130	59 8		120	3	3								13
20	012036	27.2H 141.9E	70019	2742	960	65 318		668	67 3		60	3	5	CIRCULAR	18			+12			13
51	828985	27.6N 148.8E	70010	2748	960	\$5 350	110	100	73 3		127		3	ELL IPTICAL	7	5 6	40	+14	+17	+15	14
22	821155	27.9H 140.5E	70018	2772				100	81 6		72	15	2	CONCENTRIC							14
23	821938	28.3N 139.3E	79818	2828				666	77		87	5	6								15
24	822286	20.5N 139.5E	7001B	2834		65 268	90	160	75 (		110	4	6	CIRCULAR	15 28			+15			15
25	838857	29.3₩ 139.4€	70010	2778	963	65 358	98	966 186	64 3 84 E		120	- 7	2	CIRCULAR	20			+16	Ŧ16	+14	16 16
26 27	631266 631431	29.3N 139.4E	78811)	2885	968			100	D-4 (	,,,,,	110	:	é	CIRCULAR	15			+14		417	17
29	831981	29.4H 139.8E 30.2H 140.4E	78819 78819	2002 2796	368			198	76 E	-	98	3	5	LIKCOLM	13			+14	+13	+13	17
29	032123	38.7N 148.7E	788HB	2787	964	88 328	68	330	75 2		45	2	ă					+17	417	A15	18
38	946012	30.8H 141.2E	76818	2773	20-	68 198	11	200	85 6		87	3	3					711	+11	¥13	18
31	846238	31.4H 142.8E	7001B	2885	965	30 320		168	61 6		78	5	ī					+15	410	414	18
32	848857	32.2H 143.7E	78819	2794	966	88 298		258	96 1		85	ĕ	18					+15			19
33	841285	32.9N 144.5E	786MB	2798	,,,,,	JJ 250	. 30	198	71		98		io							• • • •	19
34	841448	33.3H 145.1E	70018	2886				268	84		98		ia					+17	+16	+15	19
35	842123	35.1N 147.4E	78819	2849	973	88 898	120	158			188	ž	4					+12			20
36	650000	35.6H 147.8E	7881B	2848	-10	68 188		810	70 0		68	2	2								26
							-					-	-								

TROPICAL STORM HOPE BEST TRACK DATA

	BEST	TRACK			UARH I		RORS		24 H	OUR FO	DRECA!			40 H	DUR FO	RECA!			72 H		RECAS RRORS	
HD/DA/HR	POS1T	WIND	POS	1T	WIND	BET	WIND	POS	IT	MIND	DET	HIND	POS	1T	WIND	DST	LIND	POS	IT	UIND	DST	UIND
	16.2 118.		0.6	ີ.ຄ.ຄ			8.	8.0				0.	8.8	8.8	8.	-8.	8.	8.8	6.8	8.	-8.	8.
	16.5 118.		4.6	0.0		-1.	ě.	8.8	9.8		-ē.	Ď.	8.8	8.0	8.	-8.	8.	0.0	0.8	8.	-0.	0.
	16.6 117.			118.8	38.				116.0			-15.		115.4	50.	491.	-18.	8.8	0.0	e.	-8.	8.
*****	16.6 116.			117.8			-18.		116.4				18.6			458.	8.	8.8	8.0	٥.	-8.	ē.
	16.6 116.			116.8			-5.		114.2				8.8	6.8	<b>1</b>		6.	8.0	8.0	ě.	-0.	Š.
	16.5 114.				45.				113.6				6.8	0.8	ě.	= -	ě.	8.8	6.6	ā.	-ā.	ă.
	16.5 113.			113.6			= -		189.9				0.0	8.8	ă.	= -		6.6	8.8	ě.	-0.	ā.
							=-							8.8	6.		٠.	8.6	8.8	ă.	<u>.</u> .	Ĭ.
	16.4 112.			112.2		12.	٠.		188.2		134.	10.	0.0		= -		٠.			٠.	₹.	₽.
898688Z	16.2 111.	268	16.2	111.0	68.	12.	8.	6.8		6.	-6.	٠.	8.6	8.8	₩.	-8.	₽.	8.8	8.8	8.	-0.	₽.
<b>090686Z</b>	15.9 118.	1 68	16.0	189.6	68.	29.	8.	8.8	8.0	8.	-0.	0.	7.8	8.8	ı.	-0.	8.	0.0	8.8	0.	-0.	8.
<b>6986</b> 122	15.7 189.	68	15.8	189.0	a.	6.	8.	0.0	0.0	8.	-8.	e.	8.8	8.8		-8.	8.	8.0	8.6	٠.	-0.	8.
090618Z	15.6 107.		15.5	100.0	40.	13.	~10.	8.0	8.0	0.	-0.	8.	0.0	8.8	e.	-8.	8.	8.8	0.0	٥.	⊸•.	8.

	ALL	<b>FORECAS</b>	TS		TYPHO	DHS LIHIL	E OVER	35 KT\$
	URNG	24-HR	40-HR	72-HR	LIRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	19.	106.	426.	8.	₽.	₽.	8.	₽.
AVG RIGHT ANGLE ERROR	9.	79.	110.	8.	8.	€.	€.	€.
AVE INTENSITY MAGNITUDE ERROR	4.	11.	5.	●.	8.	8.	٥.	€.
AVE INTENSITY BIAS	-4.	-8.	-5.	0.	0.	٥.	8.	8.
NUMBER OF FORECASTS	10	6	2	•		8	8	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 638. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

18. KNOTS

TROPICAL STORM HOPE FIX POSITIONS FOR CYCLONE NO. 17

FIX NO.	TIPE (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMENTS	SITE
<b>*</b> 1	841688	15.5N 115.6E	PCN 6			PGTM
2	840000	16.4H 110.3E	PCH 6	T2.0/2.0	INIT OBS	PGTU
3	846388	16.5H 118.3E	PCN 6			PGT⊌
4	840600	16.7N 118.5E	PCN 4			PGTU
5	848714	16.7N 118.1E	PCN 5	T2.8/2.8	INIT 085	RP11K
6	848988	15.9N 117.5E	PCH 6			PGTW
* 7	841288	16.8N 116.4E	PCN 6			PGTU
* 8	841888	16.5N 116.9E	PCN 6			PGTU
. 9	842188	17.1N 116.6E	PCH 6			PGTU
10	050000	16.5N 115.3E	PCH 6	T3.8/3.8 /D1.8/24RS		PGTU
11	858388	16.5N 115.2E	PCN 6			PGTW
12	858688	16.3N 114.5E	PCH 6			PSTU
13	658782	16.3H 114.4E	PCN 5	T3.5/3.5+/D1.5/24RS		RPMK
14	050900	16.3H 114.2E	PCN 6			PGTU
15	051200	16.1H 113.1E	PCN 6			PGTU
16	851688	16.1N 111.9E	PCN 6			PGTU
17	951888	16.2N 111.6E	PCN 6			PGTU
16	852188	16.6H 111.9E	PCN 6			PGTU
19	968688	15.8N 110.8E	PCN 6			PGTU
20	060300	15.5N 110.2E	PCN 6	T3.5/3.5-/D8.5/27HRS		PGTU
21	060600	15.8H 189.8E	PCH 6			PGTU
22	060650	15.5H 118.2E	PCN 5	T4.8/4.8-/D8.5/24IRS		RPHK
23	060900	15.7H 189.5E	PCN 6			PGTU
24	<b>06 1 200</b>	15.7N 189.1E	PCN 6		ULCC FIX	PG N
25	961688	15.8N 188.3E	PCN 6		ULCC FIX	PGTU
26	<b>061800</b>	15.7N 187.9E	PCN 6		ULCC FIX	PGTW

FIX NO.		FIX POSITION	FLT LVL	78818 HGT		MRX-SFC- VEL/BRG.		PIR/				ŘCE NAV			EYE ORIEN- DIAM/TATION		TEMP IN/ DP.		MSN NO.
1	642357	16.5N 116.8E	78816	2986	994	45 868	10	168	47	<b>0</b> 58	12	5	5			+13 +	17 +18		
						•	ea dar	FIXE	3										
FIX NO.		FIX POSITION	RABAR	ACCRY	EYE SHAPE	DI		RADOB ASUMR					(	COMMENTS	,	RADA POSITI		SITE LIND N	i.
		16.9N 112.7E 17.1N 112.0E						5///3 5///3								5.8N 1 5.8N 1		59 <b>98</b> 59 <b>98</b>	
						511	IOPT!	C FIX	ES										

FIX TIME FIX POSITION ESTIMATE DATA (NPD COMMENTS

1 841288 16.8N 119.8E 838 838 HBDF SHIP OBSERVATION 841808 16.8N 117.1E 835 1808 HBDF SHIP OBSERVATION 851808 16.3N 112.3E 868 828 LPD 59981 4 866808 16.2N 111.2E 868 825 LPD 59985

# TYPHOON IRVING

		BEST	TRACK		URRH		NORS		24 H	JUR F	ORECA: ERR			48 H	OUR F	ORECA ERRO			72 H		ORECA!	
HD/DA/HR	POS	ıτ	LIND	P051T	LIND		HIND	POS	:IT	MIND		WIND.	POS	11	UIND		. MIND	POS	11	LIND		
090410Z	13.8			0.8 0.6		~€.	8.	0.8		8.	-8.	8.	8.8			-B.	B.	0.0		B.	-B.	8.
696366Z		132.		0.8 0.6		-0.	8.	6.0	8.0	8.	-ē.	ä.	8.8	8.6		-8.	ě.	6.6	8.8	3.	-8.	8.
090306Z	13.2			13.2 132.1		6.	8.	14.8	138.5	40.	124.	5.	15.8	127.8	55.	198.	ē.	16.3	124.5	65.	192.	5.
898512Z	13.7			13.6 131.7		18.	6.		138.0	45.	163.	š.		127.8		187.	8.	16.4	123.7	79.	192.	15.
090516Z	14.1			13.9 131.6		21.	5.		128.7	56.	117.	5.		125.7		156.	5.	15.9	122.2	79.	173.	28.
0906862	14.2			14.3 129.6		13.	6.		126.2	58.	165.	ě.		122.5		238.	18.	16.8	110.6	69.		10.
090606Z	13.7	128.		14.4 128.2		31.	5.		124.8	50.	193.	-5.		129.8		316.	-15.	18.4	117.8	55.	391.	5.
090612Z	13.2	128.	1 40	13.4 128.2		13.	18.		125.0	65.	63.	5.		121.8		117.	8.		118.2	55.	158.	5.
898618Z	13.2	127.	7 45	13.2 127.5		12.	18.		124.6	68.	99.	Ď.		120.8		136.	5.		117.2	68.	179.	10.
898786Z	12.9	127.	1 58	13.8 127.6	60.		10.		124.1	78.	64.	10.		121.2		78.	5.		118.4	60.	76.	10.
898796Z	12.9	126.	5 55	12.9 126.2	60.	19.	5.	13.1	123.2	60.	78.	8.	13.8	128.4	55.	82.	5.	14.3	117.3	68.	75.	10.
898712Z	12.9	126.	1 68	13.8 126.1	60.	6.	ě.		123.9	55.	13.	8.	13.7	120.0	58.	31.	ē.		117.8	60.	57.	5.
<b>898</b> 7182	13.8	125.	7 68	12.0 125.4	68.	21.	6.	13.0	122.5	50.	37.	ē.	14.1	119.5	55.	42.	5.		116.3	60.	26.	8.
<del>090000</del> Z	13.0	125.	2 68	13.1 125.4	68.	13.	8.	13.2	123.3	55.	58.	5.	13.7	120.9	50.	122.	Ö.	14.9	118.3	55.	141.	-16.
898886Z	13.1	124.	4 60	13.1 124.3	60.	6.	٠.	13.5	121.4	50.	29.	e.	14.6	118.0	55.	42.	5.	16.2	115.9	60.	51.	-5.
<b>696</b> 8122	13.2	123.	8 55	13.8 123.7	35.	13.	€.	13.8	120.5	50.	33.	ė.	15.2	117.8	55.	17.	6.	16.8	114.8	60.	68.	10.
<b>8988</b> 182	13.2			13.2 122.6	55.	18.	5.	14.2	119.0	50.	25.	€.	15.5	117.2	68.	34.	8.	17.3	114.0	69.	72.	-15.
898988Z		122.		13.4 122.4	50.	12.	8.	13.8	120.0	58.	81.	8.	14.2	117.5	55.	114.	-18.	14.7	113.8	68.	196.	20.
<b>090</b> 906Z	13.8	121.0		13.6 121.8	58.	12.	€.	14.6	119.4	58.	92.	8.	14.3	116.7	55.	184.	~18.	14.7	112.9	60.	136.	-30.
<b>090</b> 912Z	14.2			14.1 128.8		€.	€.	14.6	118.2	60.	54.	5.	14.9	114.8	68.	54.	-10.	15.4	110.5	60.	213.	-30.
<b>0909</b> 18Z	14.5			14.8 119.6		25.	8.		116.5	68.	44.	6.		113.2		77.			109.2	60.	241.	-30.
691666Z	14.9			15.8 119.8		13.	₽.		115.6	68.	45.	-5.		112.2		123.			108.5	55.	269.	
691666Z	15.1			15.9 117.7		35.	₽.		114.3	60.	60.	-5.		111.4	65.	178.		16.3	187.9	5#.	315.	-38.
891812Z	15.2			15.3 117.6		8.	Ð.		114.8	65.	54.	-5,		111.9	68.	109.			189.4	<b>5</b> 5.	209.	-20.
891818Z	15.2			15.5 116.8		19.	e.		114.2	68.	48.	-15.		111.2	55.	129.			188.2	50.	266.	-25.
891188Z	15.3			15.4 115.6			-5.		112.8	55.	87.	-25.		109.8	50.	206.			106.8	35.	338.	-35.
691186Z	15.5			15.8 115.2		21.	-5.		112.3	55.	98.	~35.		189.4		238.			106.9	35.	329.	35.
<b>89</b> 11122 <b>89</b> 11182	15.8			15.8 114.6		6.	-19.		112.6	55.	69.	~35.		110.2		168.			187.8	51.	262.	15.
	16.2			16.2 114.5			-10.		113.7	70.	40.	-20.		112.0	65.	41.	-18.		111.8	55.	48.	-10.
8912862 8912862	16.4	114.		16.7 114.2		19.	-15.		113.2	70.	66.	-15.		111.8	60.	75.			110.5	45.	199.	-15.
091212Z	17.8			16.9 113.9		13. 6.	0.		112.6	95.	35.	15.		111.7	88.	49.	10.		110.B	65.	98.	5.
<b>89</b> 12182	17.4			17.0 113.7 17.2 113.1		21.	8.		112.4	95.	24. 55.	20. 28.		111.3	88.	16. 36.	15.		110.8	65.	119.	5.
0913802	17.7			17.6 112.8		24.	8. 8.		111.7	95. 98.	45.	20. 18.		118.5	78.	36. 41.	.5.		110.2	60.	129. 179.	5. 5.
0913062	18.0			18.0 113.6		6.	ø.		112.8	75.	62.	10. 5.			78.		18.		110.0	50.		
<b>69</b> 13122	18.3			18.3 113.8			0.		112.1	65.	34.	3. 8.		111.6	65.	115.	5.	0.0	0.0	ø.	-6.	ē.
<b>69</b> 13182	18.7			18.9 112.4		11.	-5.		111.1	50.	54.			168.4	68. 36.	137. 83.	. O.	6.8	6.6	8.	-8.	٥.
8914882	19.8			19.1 112.2		6.	-5. 0.		111.1	65.	66.	~15. 5.	23.0	8.8	30. A.	-B.	-25. 8.	8.8	8.8	9.	-0. -0.	8, 8.
891486Z	19.4			19.3 111.9		6.	9.		116.9	66.	73.	a.	8.8	8.8	8.	-8.	8.	8.8	0.8 0.8	Ð. Ð.	-e.	8.
6914122	19.9			20.0 111.7		13.	8.		118.8	50.	121.	~18.	8.8	8.8	8.	-8.	B.	8.8	0.0	Ð.	-e.	B.
091418Z	20.1			20.3 111.3		16.	8.		118.3	48.	137.	~15.	8.8	8.8		-8.	8.	8.8	8.8	9.	~0.	8.
091500Z		116.		20.6 110.2		12.	Đ.		188.6	40.	181.	-13. -5.	0.0	8.8	6.	-8.	8.	0.0	0.6	ø.	~0.	e.
691586Z	26.9			20.8 189.5		8.	0.	8.8	0.0	- T	-8.	-3. B.	0.0	8.8	Ð.	-8.	Ø.	6.6	8.8	8.	-0.	0.
691512Z	21.3			21.5 109.8		12.	ø.	8.6	6.8	8.	-0.	e.	8.6	8.6		-e.	8.	8.8	8.8	9.	-0.	e.
091518Z	21.7			21.7 187.9		ē.	ě.	8.6	6.6		-6.	8.	6.8	8.8	ă.	-8.	ø.	0.0	8.8	8.	-0.	ø.
891686Z	21.8			21.8 107.8		ě.	ē.	0.6	6.6	ē.	-8.	ē.	8.8	8.8	ē.	-0.	ē.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECME			TYPHOG	NS UH	ile over	35 KTS
	LIRNG	24-HR	49-1病	72-HR	LIRNG	24-1#	1 48~HR	72-HR
AVG FORECAST POSIT ERROR	13.	73.	110.	172.	13.	73.	110.	172.
AVG RIGHT ANGLE ERROR	9.	42.	72.	126.	9.	42.	72.	126.
AVG INTENSITY MAGNITUDE ERROR	2,	8.	11.	15.	Ž.	8.	11.	15.
AVG INTENSITY BIAS	€.	-2.	-6.	~B.	-ē.	~2.	-6.	-8.
NUMBER OF FORECASTS	44	40	35	32	41	40	35	32

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1778. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

# TYPHOON IRVING FIX POSITIONS FOR CYCLONE NO. 18

	TIME	FIX			·	
NO.	(2)	POSITION	ACCRY	DVORAK CODE	CONSTRAITS	SITE
1 2	050000 050300	12.0H 132.6E 13.2H 132.6E	PCN 6 PCN 6			PGTU PGTU
3	858528 858688	13.5N 132.6E 13.4N 132.5E	PCN 3 PCN 4	T1.0/1.0	INIT COS	PG NJ PG NJ
5	050900	13.4H 132.2E	PCH 4			PGTU
ž	851288 851688	13.6H 131.7E 13.5H 130.8E	PCH 6			PGTU PGTU
* 8	851888 852188	12.8N 130.3E 14.8N 128.9E	PCN 6 PCN 6			PGTU PGTU
10 11	968888 968388	13.7N 128.7E 13.7N 128.4E	PCN 6	T2.5/2.5 /D1.5/21HRS		PGTU PGTU
12 13	868688 868658	13.5N 127.8E 13.2N 129.8E	PCN 6 PCN 5	T2.0/2.8	INIT ORS	PGTM RF18K
14 15	060900 061200	13.2N 127.7E 13.6N 127.9E	PCN 6 PCN 6		ULCC FIX	PGTU
16	061600	13.3H 127.6E	PCN 6		ULCC FIX	PGTU
17 18	061753 062100	13.3N 127.5E 13.2N 127.3E	PCN 5 PCN 6			PGTU
19 28	878888 878388	13.2H 127.8E 13.8H 126.6E	PCN 6	T3.5/3.5-/01.8/24RS		PGTU PGTU
21 22	878688 878637	13.1N 126.4E 13.8N 126.5E	PCN 4 PCN 5	T3.5/3.5 /D1.5/24RS		PG TU RP18K
23 24	878988 871288	13.6N 126.2E 12.6N 126.1E	PCN 6 PCN 6			PGTU
25 26	671666 671666	12.7N 125.4E	PCN 6		18 66 6 1v	PCTU
27	871922	12.5N 125.2E 13.1N 125.1E	PCN 5		ULCC FIX	PGTW ROOM
28 29	872186 888888	12.9N 125.1E 13.2N 124.6E	PCN 6		ULCC FIX	PGTU PGTU
30 31	000300 000626	13.1N 124.6E 13.2N 124.3E	PCH 6 PCH 5	T3.5/3.5 /S0.0/24RS		PGTU PSTU
32 33	000626 000900	13.1N 124.1E 13.1N 124.8E	PCN 3 PCN 6	T4.8/4.8-/08.5/24RS		RPISK PGTU
34 35	001200 001600	13.1N 123.7E 13.2N 122.9E	PCN 6		ULCC FIX ULCC FIX	PGTU
36 37	001000 001000 002100	13.3N 122.4E	PCN 6		ULCC FIX ULCC FIX	PGTM
38	090000	13.6N 122.1E 13.6N 122.4E	PCN 6		OLCE FIX	PGTU
39 48	090300 090613	13.9N 122.3E 14.3N 121.3E	PCN 6 PCN 5	T2.5/3.5+/¥1.8/24RS		PGTU
41 42	898613 898988	14.2N 128.4E 14.1N 128.3E	PCN 3			RPIK PGTU
43 44	090900 091200	14.2N 121.1E 14.6N 120.2E	PCN 4 PCN 6		ULCC FIX	RPHK PGTU
45 * 46	891680 891888	15.8N 119.8E 15.4N 119.3E	PCN 6 PCN 6		ULCC FIX	PGTW
47	091858	15.1N 119.7E	PCH 5		ULCC FIX	PGTW ROBH
* 49 49	091858 092100	15.5N 119.0E 14.9N 119.7E	PCN 5		ULCC FIX ULCC FIX BRKS CONTINUITY	PGTM PGTM
58 51	100000 100300	14.9N 119.8E 15.3N 118.6E		T3.5/3.5 /01.8/24/RS		PGTU PGTU
52 53	188681 188681	15.4H 118.8E 15.1H 117.6E	PCN 5 PCN 5	T3.5/3.5 /D0.5/24HRS		PGTU RPt <b>S</b> C
54 55	100900 101200	15.3N 117.3E 15.5N 116.8E	PCN 6		ULCC FIX	PGTU
56 57	181688	15.3N 116.7E 15.1N 116.6E	PCN 6 PCN 6			PGTW
58 59	101046	15.0N 116.5E	PCN 5			PGTM PGTM
68	102100 110000	15.2N 116.3E 15.5N 115.9E	PCH 6		ULCC FIX	PGTU PGTU
61 62	11 <b>0300</b> 11 <b>0600</b>	15.7N 115.7E 15.8N 115.4E	PCH 4 PCN 2	13.5/3.5 /S8.8/27HRS		PGTU PGTU
63 64	110900 111200	15.8H 115.3E 15.9H 115.1E	PCH 4 PCH 4			PGTU PGTU
65 66	111688	16.8N 114.8E 16.3N 114.6E	PCN 4 PCN 4			PSTU PGTU
67 68	112100	16.4N 114.3E 16.6N 114.1E	PCN 4		ULCC FIX	PG FM PG TU
69	120300	16.7N 113.9E	PCH 4	77 A G B A L T A MAG	ocat FIX	PG I'U
78 71	120600 120719	16.7N 113.9E 16.9N 113.9E	PCN 1	T5.6/5.8-/D1.5/244RS T5.6/5.8 /D1.5/25HRS		PGTM RODN
72 73	120900 121200	16.9N 113.7E	PCN 2 PCN 2			PHTM PG IM
74 75	1216 <b>88</b> 1218 <b>8</b> 8	17.1M 113.2E 17.3M 113.1E	PCN 2 PCN 2			PG IM PG IM
76 77	122100 130000	17.4H 113.8E 17.6H 113.8E	PCN 2 PCN 2			PGTW PGTW
70 79	138388	17.8N 113.1E 18.1N 112.9E	PCN 2	T4.8/4.5 /UL.8/21HRS		PGTW
86	130706	18.2N 113.1E	PCN 2 PCN 6	T4.5/5.8 /MB.5/24RS	18.50.514	PGTU R-INN
91 92	130900 131200	10.3H 112.8E 10.5H 112.5E	PCN 6		ULCC FIX	PGTW
93 94	131 <b>600</b> 131 <b>00</b> 0	18.6M 112.5E 18.6M 112.2E	PCH 6 PCH 6		•	PGTW PGTW

85	131951	18.7N 112.3E	PCH 1		RF19K
86	132188	18.9N 112.2E	PCN 6		PGT⊎
87	140006	19. IN 112. IE	PCN 4		PGTW
66	148388	19.2N 112.8E	PCH 2	T4.0/4.8-/S8.8/24HRS	PGTW
89	140686	19.7N 111.9E	PCN 2		PGTU
90	140655	19.8N 111.8E	PCN I	T4.5/4.5-/S8.8/24HRS	RODN
91	148966	19.8N 111.7E	PCH 4		PGTU
92	141200	20.6H 111.5E	PCN 6	ULCC F1X	PGT⊌
93	141600	28.2H 111.4E	PCN 6		PGTU
94	141988	20.2N 111.1E	PCN 6		PGTU
95	141939	20.2N 110.5E	PCN 1		RPMK
96	142188	20.2H 110.6E	PCN 2		PCTU
97	158688	20.2N 110.2E	PCN 4		PGTU
98	150300	20.6N 109.9E	PCN 2	T3.5/4.8-/U8.5/24HRS	PGTU
99	150688	28.8H 189.6E	PCH 2		PGT⊎
100	158643	28.9N 189.4€	PCN 1	T3.5/4.5-/U1.8/24IRS	RODN
161	158643	28.9N 189.1E	PCN 1	T4.8/4.8-	RPHK
162	158988	21.4H 189.2E	PCN 2		PGTU
163	151200	21.6N 108.8E	PCN 2		PGT⊌
184	151600	21.5N 100.0E	PCN 4		PGTU
185	151800	21.4H 187.5E	PCN 4		PGTU
106	151927	21.7N 187.6E	PCH 4		RPMK
187	152188	21.6N 167.2E	PCN 4		PST <b>U</b>
100	160000	21.8N 187.3E	PCN 6		PGT⊌
169	168631	22.6N 187.6E	PCN 3	T2.5/3.8-/U1.5/24RS	RODN
				AIRCRAFT FIXES	

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700HB HGT	08S MSLP	MAX-SI VEL/BI				-LVL- /BRG/		ACC NAV/		EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	858729	13.2N 132.0E	1586FT		999	35 2	48 5	2 236	23	258	48	5	3			+25 +22 34	1
* 2	652218	14.2h 129.9E	1586FT	3891	999	30 3	50 3	8 888	36	350	68	5	5			+14 +12 +11 32	2
3	868715	13.5N 128.4E	788HB	3854		58 3	90 2	7 100	35	300	27	10	3				3
4	868928	13.6N 128.4E	788HB	3840	1000	60 1	30 3	0 100	60	020	29	10	3			+11 + 8	3
5	878722	13.6H 126.4E	7881B	2974		45 3	50 3	290	65	140	25	5	3			+15 +14 +11	5
6	878947	13.6N 126.3E	788HB	2976		40 0	70 6	248	44	100	35	5	3			+17 +17 + 9	5
7	871928	13.1N 125.5E	786HB	2945				838	49	270	38	5	5				6
8	872285	13.1N 125.4E	788118	2958	963	55 B	98 3	5 868	70	318	30	3	2	CIRCULAR	20	+13 +17	6
9	992000	14.8N 119.4E	7001B	2990				868	59	310	Θ	5	2				7
18	892386	14.8N 119.2E	788HB	3812		65 3	58 1	0 120	66	360	28	10	1			+12 +19 + 7	7
11	100844	15.1N 117.8E	786HB	2946		48 3	50 6	070	58	358	30	3	3				8
12	161843	15.2N 117.7E	788HB	2946	<b>56</b> 1	28 2	28 9	<b>9 290</b>	53	228	20	2	3	CIRCULAR	15	+12 +19 +12	8
13	120623	16.8N 113.9E	700HB	2638	947	100 1	20 1	B 126	95	<b>0</b> 60	28	3	2	CIRCULAR	15	+17 +20 +12	10

# RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASUAR TODFF	COMMENTS	RADAR POSITION	SITE UMO NO.
1	871886	13.1N 125.7E	LAND				1892 / 43283		14.8N 124.3E	98447
ž	871988	13.1N 125.6E					18213 42985		14.0H 124.3E	98447
3	872888	13.2H 125.6E					10012 42804		14.6H 124.3E	98447
4	872188	13.2N 125.5E					18812 42888		14.8H 124.3E	98447
5	000600	13.3N 124.2E	LAND				25/88 4////		14.1H 123.0E	98440
6	082138	13.3H 122.6E	LAND				25/10 52706		14.1H 123.8E	98449
7	082280	13.4H 122.6E	LAND				20110 52904	EYE OPEN N	14.1H 123.0E	98440
8	696638	13.6N 122.9E	LAND				20021 58415	EYE OPEN NU	14.1H 123.0E	98443
•	090610	13.8N 121.6E	LAND				4111 11111		16.3H 120.6E	90321
10	898888	13.8H 121.4E	LAND				4/// 52906		16.3N 120.6E	98321
11	090630	14.2N 128.9E	LAND	FAIR					15.2H 120.5E	98327
12	696966	13.9N 121.3E	LAND				4/// 52900		16.3H 120.6E	98321
13	<b>09 1 000</b>	14.6N 121.2E		E001				HWG UNU 4 KTS	13.8H 120.1E	
14	891288	14.3N 121.6E		COOD				HVG UNU 4 KTS	13.9N 128.1E	
15	<b>69</b> 1315	14.4H 128.7E		C009	ELL IPTICAL			N TO S AXIS 37/20	16.6N 120.3E	
16	091 <b>400</b>	14.3H 120.5E		COOD	ELL IPTICAL			N TO S AXIS 24/14	16.6H 120.3E	
17	<b>89 1 588</b>	14.2N 120.4E					4/// 63868		16.3H 120.6E	90321
10	<b>091888</b>	15.4H 119.7E					1091/ 42702		16.3N 120.6E	98321
19	<b>092 1 30</b>	14.6N 119.2E					1072/ 43004	EYE 100 PCT CIR DIA 2011	16.3N 128.6E	98321
28	<b>892</b> 155	15.8N 119.2E		COOD	ELL IPT ICAL			N TO S AXIS 27/22	16.6H 120.3E	
21	892288	14.8N 119.1E					1072/ 42904	EYE 108 PCT CIR DIA 26NH	16.3N 120.6E	98321
22	092230	14.8N 119.1E					1872/ 42984	EYE 100 PCT CIR DIA 15HM	16.3H 120.6E	98321
23	092350	15.6H 119.8E		COOD	CIRCULAR	32			16.6H 120.3E	
24	100000	14.9H 118.8E					1092/ 42703	EYE 100 PCT CIR DIA 30NM	16.3H 120.6E	98321
25	100100	14.9N 118.5E					1871/ 42786		16.3N 128.6E	98321
26	108200	14.9N 118.3E					1091/ 42905		16.3H 120.6E	96321
27	100300	15.6H 118.3E					1091/ 42905		16.3H 128.6E	98321
26	100400	15.6N 118.2E					1092/ 42803	EYE 90 PCT CIR DIA 32NM	16.3M 120.6E	98321
29	188438	14.9N 118.0E					1092/ 42600	EYE 90 PCT CIR	16.3H 120.6E	98321
30	100500	14.98 117.95	LAND				1872/ 42784	EYE 78 PCT CIR OPEN E	16.3N 128.6E	98321

31 180608 15.0H 117.7E LAND 1877 43908 EYE 68 PCT CIR OPEN E 16.3H 128.6E 99321 180738 15.0H 117.7E LAND 1877 41785 16.3H 128.6E 99321 181838 15.0H 117.5E LAND 1877 41785 16.3H 128.6E 98321 181838 15.1H 117.2E LAND 1871 439085 16.5H 114.1E LAND 1871 439085 16.5H 114.1E LAND 1873 43906 16.5H 114.1E LAND 1873 43906 16.5H 112.3E 59981 18.6H 114.8E LAND 1873 43906 16.5H 112.3E 59981 18.6H 114.8E LAND 1873 43906 16.5H 112.3E 59981 18.6H 114.8E LAND 1873 43906 16.5H 112.3E 59981 18.6H 112.										
32 180738 15.0H 117.7E LAND 1071/ 40000 16.3H 120.6E 99321 33 100000 15.0H 117.5E LAND 1071/ 41705 16.3H 120.6E 99321 33 101030 15.1H 117.2E LAND 1071/ 43005 16.3H 120.6E 99321 1353 112350 16.4H 114.1E LAND 18063 52996 16.5H 114.1E LAND 18043 53006 16.6H 112.3E 59981 37 120250 16.5H 114.0E LAND 18043 53006 16.5H 112.3E 59981 39 120950 17.0H 11.7E LAND 180512 53485 16.6H 112.3E 59981 40 121150 17. 113.5E LAND 180512 53485 16.6H 112.3E 59981 40 121150 17. 113.5E LAND 180512 53485 16.6H 112.3E 59981 42 121350 17.3H 113.4E LAND 180512 53485 16.6H 112.3E 59981 42 121350 17.3H 113.4E LAND 180512 53485 16.6H 112.3E 59981 42 121350 17.3H 113.4E LAND 180512 53485 16.6H 112.3E 59981 44 121550 17.4H 113.4E LAND 180512 53485 16.6H 112.3E 59981 44 121550 17.5H 113.4E LAND 180512 53485 16.6H 112.3E 59981 45 121550 17.5H 113.4E LAND 180512 53485 16.6H 112.3E 59981 47 121550 17.5H 113.4E LAND 180512 53485 16.6H 112.3E 59981 49 12150 17.5H 113.4E LAND 180512 53485 16.6H 112.3E 59981 47 121950 17.5H 113.4E LAND 180512 53384 16.6H 112.3E 59981 49 122150 17.5H 113.4E LAND 180512 53384 16.6H 112.3E 59981 58 16.6H 112.3E 59981 58 16.6H 112.3E 59981 58 16.6H 112.3E 59981 59981 58 16.6H 112.3E 59981 58 16.6H 112.3E 59981 59981 59981 58 180650 16.5H 112.3E 59981 58 180650 16.5H 112.3E 59981 59981 58 180650 16.5H 112.3E 59981 58 1806	31	100600	15.8N 117.7E	LAND	1872/ 43884	EYE 68 PCT CIR I	DPEN E	16.38	120.6E	98321
33   180808   15.0H   17.5E   LAND   1877   41785   16.3H   129.6E   98321   34   181830   15.1H   17.2E   LAND   1871   43885   16.3H   129.6E   98321   35   112350   16.4H   114.1E   LAND   18683 \$2986   16.8H   112.3E   59981   36   120850   16.5H   114.1E   LAND   18732   43886   16.6H   112.3E   59981   37   120850   16.9H   11.4E   LAND   18732   53886   16.6H   112.3E   59981   38   120850   16.9H   11.4E   LAND   18512   53885   16.8H   112.3E   59981   18732   17.9H   17.7E   LAND   18512   53485   16.8H   112.3E   59981   18732   17.9H   17.7E   LAND   18512   53485   16.8H   112.3E   59981   141   121250   17.9H   13.5E   LAND   18512   53485   16.8H   112.3E   59981   141   121250   17.9H   13.4E   LAND   18512   53485   16.8H   112.3E   59981   141   121250   17.9H   13.4E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   17.9H   13.4E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   17.9H   13.4E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   17.9H   13.4E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   17.9H   13.3E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   17.9H   13.3E   LAND   18512   53485   16.8H   112.3E   59981   18.9H   112.3E   18.9H   112.3E   18.9H	32	100738	15.8N 117.7E	LAND						
34 181838 15.1N 117.2E LAND 1871.4 58985 16.3M 129.6E 98321 35 112338 16.4M 114.1E LAND 18683 52986 16.5M 114.1E LAND 18683 52986 16.5M 114.1E LAND 18732 43886 16.5M 112.3E 59981 37 128258 16.5M 114.1E LAND 18732 43886 16.5M 112.3E 59981 38 128958 17.5M 114.6E LAND 18512 533865 16.5M 112.3E 59981 39 128958 17.5M 11.5E LAND 18512 53485 16.6M 112.3E 59981 41 12138 17 113.5E LAND 18512 53485 16.5M 112.3E 59981 41 121258 17.3M 113.4E LAND 18512 53485 16.5M 112.3E 59981 42 121359 17.3M 113.4E LAND 18512 53485 16.6M 112.3E 59981 42 121359 17.3M 113.4E LAND 18512 53485 16.6M 112.3E 59981 44 121556 17.5M 113.4E LAND 18512 53485 16.6M 112.3E 59981 44 121558 17.5M 113.4E LAND 18512 53485 16.6M 112.3E 59981 44 121558 17.5M 113.3E LAND 18512 53485 16.6M 112.3E 59981 44 121559 17.5M 113.3E LAND 18512 53485 16.6M 112.3E 59981 46 121750 17.4M 113.3E LAND 18512 53485 16.6M 112.3E 59981 47 121850 17.5M 113.3E LAND 18512 53485 16.6M 112.3E 59981 47 121850 17.5M 113.3E LAND 18512 53384 16.6M 112.3E 59981 51 138050 16.6M 112.3E 59981 51 16.6M 112.3E 59981 5	33	188888	15.6N 117.5E	LAND	1877/ 41785					
35 112359 16.4H 114.1E LAND 18603 \$2986 16.9H 112.3E 59981 36 120850 16.5H 114.1E LAND 18732 438866 16.9H 112.3E 59981 37 120259 16.5H 114.0E LAND 18732 438866 16.9H 112.3E 59981 38 120650 16.0H 11.0E LAND 18512 53386 16.0H 112.3E 59981 39 120850 17.0H 11.7E LAND 18512 53485 16.0H 112.3E 59981 40 121150 17.7° 13.5E LAND 18512 53485 16.9H 112.3E 59981 11.1E 12.3E 17.9H 113.3E LAND 18512 53485 16.0H 112.3E 59981 11.1E 12.3E 17.9H 113.4E LAND 18512 53485 16.0H 112.3E 59981 43 121450 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 44 121550 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 44 121550 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 46 121750 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 46 121750 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 46 121750 17.0H 113.4E LAND 18512 53485 16.0H 112.3E 59981 46 121750 17.0H 113.3E LAND 18512 53485 16.0H 112.3E 59981 46 121750 17.0H 113.3E LAND 18512 53485 16.0H 112.3E 59981 47 121550 17.0H 113.3E LAND 18512 53485 16.0H 112.3E 59981 48 121950 17.5H 113.3E LAND 18512 53384 16.0H 112.3E 59981 50 12250 17.0H 113.1E LAND 18512 53384 16.0H 112.3E 59981 50 12250 17.0H 113.1E LAND 18512 53384 16.0H 112.3E 59981 50 12250 17.0H 113.1E LAND 18712 53382 16.0H 112.3E 59981 51 130850 17.7H 113.1E LAND 18712 53382 16.0H 112.3E 59981 51 130850 17.7H 113.1E LAND 18712 53382 16.0H 112.3E 59981 51 130850 17.7H 113.1E LAND 18712 53382 16.0H 112.3E 59981 51 130850 17.7H 113.1E LAND 18712 53382 16.0H 112.3E 59981 51 130850 18.3H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 130850 18.3H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 130850 18.3H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485 16.0H 112.3E 59981 51 131850 18.0H 112.0E LAND 30713 53485	34	101030	15.1N 117.2E	LAND						
36 120850 16.5H 114.1E LAND 10732 43986 16.8H 112.3E 59981 37 120250 16.5H 114.0E LAND 10413 53086 16.8H 112.3E 59981 38 120850 16.6H 112.3E 59981 19512 53596 16.8H 112.3E 59981 39 120850 16.6H 112.3E 59981 18512 53596 16.8H 112.3E 59981 18512 53495 16.8H 112.3E 59981 18512 53395 16.8H 112.3E 599981 18512 53395 18.5H 112.5E LAND 18512 55133595 16.8H 112.3E 599981 18512 5513355 16.8H 112.3E 599981 18512 5513	35	112350								
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49 122150 17.6N 113.1E LAND 11712 53384 16.6N 112.3E 59981 50 122250 17.6N 113.1E LAND 18712 53382 16.6N 112.3E 59981 51 130858 17.7N 113.1E LAND 18712 53382 16.6N 112.3E 59981 52 130859 18.6N 112.6E LAND 38762 53485 16.6N 112.3E 59981 53 130859 18.6N 112.6E LAND 38762 53485 16.6N 112.3E 59981 54 130850 18.3N 112.6E LAND 38713 53485 16.6N 112.3E 59981 55 131150 18.5N 112.6E LAND 38713 53485 16.6N 112.3E 59981 56 131250 18.6N 112.3E 59981 56 131250 18.6N 112.3E 59981 57 131450 18.6N 112.5E LAND 3773 53485 16.6N 112.3E 59981 56 131250 18.6N 112.5E LAND 3773 53485 16.6N 112.3E 59981 57 131450 18.7N 112.5E LAND 3773 53485 16.6N 112.3E 59981 57 131850 18.7N 112.5E LAND 3773 53485 16.6N 112.3E 59981 58 131850 19.0N 112.3E LAND 3773 53485 16.6N 112.3E 59981 59 131850 19.0N 112.3E LAND 3773 53485 16.6N 112.3E 59981 17.5N 112.5E LAND 3773 53485 16.6N 112.3E 59981	48									
50 122250 17.6N 113.1E LAND 10712 53302 16.9N 112.3E 59901 51 130050 17.7N 113.1E LAND 10712 53302 16.9N 112.3E 59901 52 130050 10.9N 112.0E LAND 30712 53405 16.9N 112.3E 59901 53 130050 10.1N 112.0E LAND 30713 53405 16.9N 112.3E 59901 54 130050 10.3N 112.0E LAND 30713 53405 16.9N 112.3E 59901 55 131150 18.5N 112.6E LAND 30713 53405 16.9N 112.3E 59901 56 131250 18.6N 112.6E LAND 37//3 53405 16.9N 112.3E 59901 57 131450 10.7N 112.5E LAND 37//3 53405 16.9N 112.3E 59901 58 131850 19.0N 112.3E LAND 37//3 53405 16.9N 112.3E 59901	49									
51 138658 17.7N 113.1E LAND 18712 53382 16.8N 112.3E 59981 51 138550 18.0N 112.3E 159981 52 138550 18.0N 112.3E 159981 53 138550 18.1N 112.8E LAND 38713 53485 16.8N 112.3E 59981 54 138659 18.3N 112.6E LAND 38713 53485 16.8N 112.3E 59981 55 13150 18.5N 112.6E LAND 38713 53485 16.8N 112.3E 59981 56 131250 18.6N 112.3E 59981 57 131450 18.5N 112.6E LAND 3773 53485 16.8N 112.3E 59981 57 131450 18.7N 112.5E LAND 3773 53485 16.8N 112.3E 59981 57 131450 18.7N 112.5E LAND 3773 53485 16.8N 112.3E 59981 58 131850 19.0N 112.3E LAND 3773 53485 16.8N 112.3E 59981										
52 138550 18.0N 112.8E LAND 38762 53465 16.9N 112.3E 59981 53 138650 18.1N 112.6E LAND 38713 53465 16.6N 112.3E 59981 54 138650 18.3N 112.6E LAND 38713 53465 16.6N 112.3E 59981 55 131150 18.5N 112.6E LAND 37/3 53465 16.9N 112.3E 59981 56 131250 18.6N 112.6E LAND 37/3 53465 16.9N 112.3E 59981 57 131450 18.7N 112.5E LAND 37/3 53465 16.6N 112.3E 59981 58 131850 19.0N 112.3E LAND 37/3 53465 16.6N 112.3E 59991	51	130050								
53 138659 18.1N 112.8E LAND 38713 53485 16.6N 112.3E 59981 54 138850 18.3N 112.8E LAND 38713 53485 16.6N 112.3E 59981 55 131150 18.5N 112.6E LAND 3773 53485 16.6N 112.3E 59981 56 131250 18.6N 112.6E LAND 3773 53485 16.6N 112.3E 59981 57 131450 18.7N 112.5E LAND 3773 53495 16.6N 112.3E 59981 58 131850 19.0N 112.3E LAND 3773 53495 16.6N 112.3E 59981 17.5N 112.5E 18.5N 112.5N 112.5E 18.5N 112.5N										
54     138050     18.3N 112.6E     LAND     30713 53405     16.8N 112.3E     59981       55     131150     18.5N 112.6E     LAND     3773 53405     16.8N 112.3E     59981       56     131250     18.6N 112.6E     LAND     3773 53405     16.8N 112.3E     59981       57     131450     18.7N 112.5E     LAND     3773 53405     16.8N 112.3E     59981       58     131850     19.8N 112.3E     LAND     5773 7777     16.8N 112.3E     59981	53	138658		LAND						
55     131150     18.5N 112.6E     LAND     3//3 53485     16.8N 112.3E     59901       56     131250     18.6N 112.6E     LAND     3//3 53485     16.8N 112.3E     59901       57     131450     18.7N 112.5E     LAND     3//3 53485     16.8N 112.3E     59901       58     131850     19.0N 112.3E     LAND     5//3 ////     16.8N 112.3E     59901	54	138858		LAND						
56 131259 18.6N 112.6E LAND 327/3 53485 16.6N 112.3E 59981 57 131450 18.7N 112.3E LAND 327/3 53485 16.6N 112.3E 59981 58 131850 19.0N 112.3E LAND 527/3 53485 16.6N 112.3E 59981	55	131158	18.5N 112.6E	LOND						
57 131450 18.7N 112.5E LAND 3//3 53405 16.8N 112.3E 59901 58 131850 19.0N 112.3E LAND 5//3 //// 16.8N 112.3E 59981	56	131250		I.AHD						
58 131858 19.8N 112.3E LAND 5//3 //// 16.8N 112.3E 59981	57									
	58	131850								
	59	132200	18.8N 112.3E	LAND	18512 53184					59758

## SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
1	881288	13.0N 123.7E	<b>e55</b>	815	UMD 98444	
2	061888	13.1N 123.8E	655	950	UMD 98440	
3	891288	14.8N 121.8E	050	825	MMD 98428	
4	891888	14.5N 120.2E	656	825	UMD 98426	
5	130000	17.8N 113.1E	385	875	UHD 59981	
6	142100	28.4N 118.7E	868	838	UMD 59758	
7	151800	21.7N 187.9E	<b>0</b> 55	045	WMD 59632	

TYPHOON JUDY BEST TRACK DATA

	BEST 1	TRACK		LIARN	ING ERROR:	3		24 H	OUR F	DRECA: ERR			48 H	OUR F	DRECA!			72 H		ORECAS ERRORS	
HD/DA/HR	POSIT L	IND	POSIT	MIND	DST LIII	ID III	POS	IT	UIND	DST	MIND	POS	TIE	UIND	DST	UIND	POS	IT	MIHD	DST	UIND
090500Z	12.1 147.3	20	6.0 6.1	8.	-e. (	). e		0.0	0.	-8.	ø.	0.0	0.0	0.	-ē.	0.	8.8	8.0	0.	-0.	e.
898586Z	12.6 146.2	25	6.0 6.0	B .	~8.	). E		9.6	8.	-8.	8.	0.0	8.8	8.	-8.	0.	8.6	0.0	0.	-8.	0.
<b>8985</b> 122	12.6 145.1	30	0.0 0.0	8.	-B. (	). E	1.0	8.8	8.	-8.	٨.	8.6	0.0	€.	-8.	8.	8.0	8.8	Э.	-0.	0.
<b>0905</b> 182	12.6 144.1	35	12.7 144.	2 25.	810	). 13	1.3	148.4	48.	113.	-10.	13.0	137.2	50.	197.	-15.	14.2	134.1	65.	301.	- 15.
090606Z	12.9 143.5	40	12.8 143.3	2 48.	19. (	1. 13	.2	139.1	56.	168.	€.	14.8	135.1	68.	256.	-18.	15.2	131.0	70.	427.	·15.
090606Z	13.2 143.1	40	13.1 143.	40.	6. (	). 13	.6	148.5	50.	84.	-5.	14.4	136.8	65.	228.	-18.		133.1	75.	452.	·15.
<b>090</b> 612Z	13.6 142.7	45	13.5 142.0	48.	8	5. 14	1.5	139.7	55.	78.	-5.	15.2	136.1	65.	246.	-10.	15.7	132.4	84.	461.	-5.
<b>8986</b> 18Z	14.8 142.2	50	13.8 142.2		12.	). 14	1.6	140.0	65.	144.	₽.		136.8	75.	315.	-5.	15.3	133.0	85.	535.	0.
898788Z	14.5 141.5	58	14.4 141.0					139.1	65.	109.	-5.			88.	266.	-5,	18.2	133.0	<b>9</b> 5.	393.	15.
898786Z	15.8 148.6	55	14.7 148.1	3 55.				130.0	78.	133.	-5.		134.8	85.	257.	-5.	19.2	130.7	188.	417.	20.
<b>0907</b> 12Z	15.8 139.7	68	15.7 140.0		10			136.8	75.	91.	8.		133.6	98.	218.	5.	21.0	130.8	110.	354.	35.
<b>098</b> 7182	16.7 138.8	65	16.7 139.3		23			135.7	98.	73.	0.	20.9	132.2	95.	215.	10.	22.7	129.5	115.	368.	40.
898888Z	17.3 137.9	79	17.4 137.0		810			133.0	85.	114.	θ.		131.0	116.	195.	30.	25.4	129.8	115.	313.	40.
090806Z	18.2 137.0	75	18.1 136.9		810			133.4	90.	112.	0.		130.0	115.	227.	35.	25.0	129.7	95.	353.	20.
898812Z	19.3 136.2	75	18.0 136.		31			133.1	95.	106.	10.		131.0	185.	211.	30.	26.0	129.6	95.	374.	20.
<del>0900</del> 182	20.4 135.5	86	20.5 135.3		13			133.3	95.	42.	18.	36.2		98.	224.	15.	33.3	142.9	80.	376.	5.
898988Z	21.4 134.7	85	21.8 134.9					133.3	105.	100.	25.		137.0	70.	388.	-5.	0.0	0.0	e.	-0.	0.
090906Z	22.4 133.9	90	22.5 133.0		8. (			133.4	98.	103.	18.		137.3	65.	379.	-10.	0.0	0.0	₽.	~€.	0.
<del>0909</del> 122	23.3 133.6	85	23.4 133.		13.			134.1	85.	169.	10.		139.2	68.	465.	-15.	0.0	6.0	9.	-0.	0.
<b>0909</b> 18Z	24.2 133.7	85	24.2 133.2					134.6		192.	-10.		141.3	48.	548.	-35.	9.0	0.0	₽.	-6.	0.
091800Z	24.8 133.8	80	24.8 133.1		8			134.7	65.		-10.		148.9	45.	403.	-30.	0.0	0.0	θ.	-8.	8.
<b>0910062</b>	25.4 134.1	88	25.7 133.0		24			135.0	68.	216.	-15.	39.2	143.0	40.	434.	-30.	8.6	9.0	a.	-8.	8.
891012Z	25.9 134.4	75	26.3 134.0			. 31		136.2	60.	187.	-15.	8.6	8.8	8.	-8.	8.	0.0	8.6	0.	~0.	₽.
891018Z	26.5 134.8	75	26.4 134.0		6.	. 38		137.6	70.	45.	~5.	8.6	8.8	₽.	-8.	0.	0.0	8.8	0.	-e.	Ð.
<b>8911882</b>	27.1 135.3	75	27.1 135.			. 31		138.5	78.	81.	-5.	0.0	0.0	8.	-8.	0.	0.0	0.6	ø.	-0.	0.
<b>89</b> 11862	27.8 135.9	75	27.9 135.0		. 0. (			139.2	60.	110.	-10.	0.0	8.0	₽.	-0.	0.	9.0	9.8	8.	-0.	٥.
<b>69</b> 1112Z	28.7 136.5	75	29.4 136.3					139.7	68.	234.	5.	6.6	6.8	8.	-8.	ø.	8.8	8.8	Ð.	~0.	₽.
<b>69</b> 1118Z	29.8 136.8	75	29.5 136.5		19		. 1	139.7	60.	264.	20.	8.0	0.0	0.	-0.	₽.	0.0	0.0	0.	-8.	ø.
891286Z	31.4 137.0	75	31.7 137.2	70.	21		.0	0.8	8.	-8.	Ð.	0.0	0.0	8.	-0.	0.	0.0	0.0	6.	-0.	ø.
<b>0912062</b>	33.6 137.3	78	33.5 137.	70.				0.0		-0.	0.	0.6	0.6	₽.	-6.	ø.	0.0	0.0	0.	-ø.	0.
<b>69</b> 1212Z	36.2 137.4	55	35.4 139.	60.				0.0	6.	-8.	Ð.	0.6	8.8	8.	<b>-0</b> .	₽.	8.8	0.0	0.	~0.	0.
<b>09</b> 1218Z	39.5 139.5	40	49.8 149.0	45.	30.	. E	.0	8.8	₽.	-8.	₽.	8.8	6.0	₽.	~8.	0.	0.0	9.0	9.	~€.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	URNG	24-HR	48-HR	72-14代	LIRNG	24-HF	48-HR	72-HR		
AVG FORECAST POSIT ERROR	19.	125.	298.	461.	(S.	125.	298.	401.		
AVG RIGHT ANGLE ERROR	15.	73.	126.	262.	15.	73.	126.	262.		
AVG INTENSITY MAGNITUDE ERROR	4.	8.	16.	15.	4,	8.	16.	19.		
AVG INTENSITY BIAS	-2.	-8.	-3.	11.	-2.	-0.	-3.	11.		
NUMBER OF FORETOSTS	20	25	19	17	20	25	19	13		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2133. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

# TYPHOON JUDY FIX POSITIONS FOR CYCLONE NO. 19

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1 2	050006 050300	12.1N 147.3E 12.3N 146.9E	PCN 6 PCN 6			PGTW PGTW
3	050520	12.5N 146.6E	PCN 5	T1.5/1.5	INIT OBS ULCC FIX	PGTU
5	858688 858988	12.6N 146.5E 12.8N 146.3E	PCN 6 PCN 6			PGTW PGTW
6	851288	12.7N 145.5E	PCN 6			PGTW
7	051600	12.3N 144.2E	PCH 6			PGTU
è	951999	12. IN 143.5E	PCN 6			PGTU
ğ	852188	13.1H 143.6E	PCN 6			PGTU
10	060000	13.4N 143.3E	PCN 6			PGTW
11	060300	13.3H 143.1E	PCH 6	T2.5/2.5 /D1.8/21HRS		PGTU
12	060508	13.1H 142.8E	PCN 5			PGTW
13	868688	13.3H 142.7E	PCH 6			PGTU
14	060900	13.4H 142.5E	PCH 6			PGTU
15	861286	13.5N 142.5E	PCN 6			PGTU
16 17	061600	13.3N 141.6E	PCH 6		ULCC FIX	PGTW
10	061753 062100	14.6N 141.9E	PCN 5 PCN 6		BRKS CONTINUITY	PGTU PGTU
19	878668	14.44 141.45	PCN 6			PGTU
20	070300	14.3H 141.1E	PCN 6	T3.5/3.5 /D1.8/24MRS		PGTU
21	078456	14.3N 140.9E	PCN 5			PGTU
22	070600	14.7N 148.7E	PCN 6			PGTU
* 23	878988	14.8H 148.5E	PCH 4			PGTU

24	671266	15.9N 139.9E	PCH 6		PGTW
25	871688	16.7N 139.2E	PCH 6		PGTW
26	871741	16.9N 138.7E	PCN 5	ULCC FIX	PRTW
27	871741	16.6N 138.6E	PCN 5	-,	RODH
28	872188	17.5N 138.6E	PCN 6	ULCC FIX	Pritu
29	868888	17.5N 137.7E	PCN 6		PGTW
30	000300	17.7N 137.4E	PCN 6	T4.5/4.5 /D1.8/24RS	PSTU
31	000444	17.9H 137.2E	PCN 5	1410-410-5110-6-4110	PGTU
32	888688	17.9H 137.2E	PCN 6		PGTU
33	888988	18.3N 137.2E	PCH 6		PGTW
34	881288	19.4H 136.3E	PCH 6	ULCC FIX	Le in
35	881688	19.7N 135.2E	PCN 6	ULCC FIX	POTU
36	881728	20.41 135.3E	PCN 6	ULCC FIX	PRIM
37	890000	21.9N 135.BE	PCN 6		PGTW
38	898388	21.9N 135.8E	PCN 6	75.8/5.8 /06.5/24RS	PGTU
39	898613	22.41 134.3E	PCN 5	1010-010-9010-0-4-40	PGTU
40	898900	22.9N 133.6E	PCN 4		Pigfu
41	891266	23.1N 133.6E	PCH 4		PGTW
42	091600	23.7N 133.5E	PCN 4		PG TU
43	891886	23.8N 133.4E	PCN 4		PGTW
44	091858	24. IN 133.5E	PCN 4		PGTU
45	891858	24. IN 133.6E	PCN 5		RODH
46	892188	24.4N 133.6E	PCH 4		PGTW
47	100000	24.8N 133.7E	PCN 4	EXP LLCF.	PGTU
48	100300	25.1N 133.8E	PCN 4	T5.8/5.6 /S8.6/24HRS	PSTU
49	100601	25.5N 134.8E	PCN 3	1012 014 2212 2 1111	FCTW
50	180300	25.7N 134.3E	PCN 4		PSTM
51	181266	26.8N 134.6E	PCN 4		PGTW
52	161686	26.3N 134.8E	PCN 4		PGTU
53	101000	26.1N 134.BE	PCN 4		PGTW
54	101046	26.0N 135.0E	PCH 3		PGTW
55	182188	26.4N 135.2E	PCN 4		PGTU
56	110000	26.9H 135.2E	PCN 4		PSTW
57	110300	27.4N 135.3E	PCN 4		PGTU
58	118549	27.7N 135.7E	PCN 3	T4.0/4.5 /U1.8/27HRS	PGTW
59	110900	28.0N 135.8E	PCN 4		PG TW
68	111200	28.3N 136.3E	PCN 4		PGTW
61	111600	29.2N 136.8E	PCN 4		PGTW
62	111886	29.8N 136.9E	PCN 6		PG Tu
63	111034	30.0N 137.1E	PCN 5		PGTW
64	112100	30.3N 137.6E	PCN 6		PGTW
65	120000	31.8N 137.5E	PCN 4	ULCC 31.3N 138.0E	PGTW
66	120300	32.3N 137.0E	PCN 4		POTW
<b>* 67</b>	121888	41.1N 142.1E	PCN 5		PGTU
* 68	121810	41.1H 142.1E	PCN 5		RODN

FIX NO.	TIME (Z)	FIX Position	FLT LVL	700MB HGT	OBS MSLP		-SFC- ⁄DRG/		MAX- DIR/			-UND ∕RNG			EYE SHAPE		ORIEH- TATION			EMP (		MSN NO.	
1	052239	12.8N 143.7E	1500FT		994	45	188	15	270	41	190	25	8	3					+24	+23	31	1	
ž	868836	13.3H 142.BE	788MB	3889			828	50	020		320		3	5				+12				2	
3	861187	13.6N 142.7E	700HB	3013					300		220		5	9					-			2	
4	861881	14.1N 142.2E	7881B	2985					110		000		9	5								3	
5	862188	14.3N 141.BE	700HB	2987		58	130	45	210		136		9	7				+12	+15	+ 9		3	
6	070623	15.2N 140.5E	7991B	2964		60	100	48	238	53	120	100	5	4								4	
7	878843	15.5N 140.2E	788H9			50	220	69	140	67	849	90	5	3				+12	+14	+10		4	
8	072059	17.1N 138.2E	70019	2986	978	45	100	30	220	46	120	88	9	10	ELL IPTICAL	40 20	1.49	+15	+15	+14		5	
9	980607	18.2N 136.8E	788HB	2832		70	100	90	188	84	166	75	18	5					+16	+12		7	
18	<del>0</del> 80902	18.7N 136.8E	788HB	2814	968	50	200	68	140	69	630	48	10	10	CIRCULAR	25		+12	+15	+14		7	
11	981885	20.6N 135.2E	799HB	2743					150	82	700	40	5	3								8	
12	082034	21.0N 135.0E	7001B	2786		78	218	15	300	80	190	20	5	3	ELL IPTICAL	40 30	090	+28	+19	+11		8	
13	<del>090</del> 600	22.5N 133.7E	7 <b>861</b> 6	2729			828	60	200	85	120	65	9	5								10	
14	<b>090940</b>	22.8H 133.6E	788HB	2738	959	55	300	75	260	67	200	68	5	5					+17			16	
15	<b>09</b> 2102	24.3N 133.8E	7 <b>0011</b> 0	2777	965		020	70	160		686		10	3				+15	+13	+13		11	
16	<b>0</b> 92316	24.7N 133.7E	760MB	2791		60	320	68	828	77	310	70	10	3								11	
17	101230	25.9N 134,4E	7861B	2793	967				136		658		15	18						+15		12	
18	101509	26.2N 134.4E	788119	2786					350		250		10	9						+15		12	
19	102207	26.8N 135.2E	7 <b>8618</b>	2797	966		220	98	300		210		10	2				+15	+16	+14		13	
28	102311	26.8N 135.2E	7 <b>0016</b>	2787			300	60	360		200		5	2								13	
21	110322	27.4H 135.3E	788HB	2800			300	96	228		130		5	5				+15	+16	+15		14	
22	118622	27.8N 135.9E	788MB	2798				120	140		630		5	5								14	
23	110010	28.8N 136.8E	700MB	27 <b>98</b>	966		240	98	238		248	88	5	5						+15		14	
24	112219	38.9N 136.7E	78/HB	2003	967			140	160		540		4	1						+12		16	
25	120203	32.1N 136.9E	7861B	2776	964		278	66	300		200		2	16						+13		16	
26	129791	34.0N 137.3E	7881B	2775	973	75	898	48	240	80	1.30	40	3	3				+ 8	+15	+11		17	

# RABAR FIXES

	TIPE (Z)	FIX POSITION	RADAR	ACCRY	FYE SHAPE	DIAM	RADOB-CODE AGUAR TODEF	CONTENTS	RABAR POSITION	SITE UMO NO.
1 2 3 4 5 6 7 8 9	851835 852835 868835 868835 868235 128888 128888 128888 128888 128888 128888 128888 128888 128888 128888 128888 128888 128888	13.8N 143.8E 13.6N 143.6E 13.5N 143.2E 13.6N 143.2E 13.6N 143.2E 13.6N 137.9E 34.3N 137.6E 34.4N 137.6E 34.9N 138.1E 35.3N 138.4E	LAND LAND LAND LAND LAND LAND LAND	PUOR POOR FAIR FAIR FAIR			6/// 5/// 6/// 4/// 227/5 53132 5//5 78124		13.6H 144.9E 13.6N 144.9E 13.6N 144.9E 13.6H 144.9E 13.6H 144.9E 34.6H 133.7E 35.2H 137.6E 35.3H 130.7E 35.3H 130.7E	91218 91218 91218 91218 91218 47773 47636 47639 47639

# SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
1	120600	33.9N 138.1E	968	865	UMD 47665	
2	120900	34.9N 138.4E	<b>8</b> 55	825	UND 47696	
3	121200	36.3N 138.3E	858	858	UND 47684	
4	121500	37.7N 138.8E	845	828	WHD 47684	
5	121900	39.5N 139.5E	040	825	UHD 47582	

TYPHOON KEN SEST TRACK DATA

	BEST TI	RACK		LIARN I	NG ERROR!	3		24 H	OUR FO	RECA!			48 H	OUR FO	RECA ERRO			72 H		ORECA EFFOR	
MO/DA/HR	POSIT W	THD	POSIT	MIND	DST WIE	ID.	POSI	T	LIND	DST	WIND	POSI	T	MIND	DST	WIND	PU	SIT	WIND	DST	MIND
091600Z	17.5 133.7	30	17.8 132.9	30.				29.9	40.	42.	-5.	19.2 1	26.4	45.	189.	-45.	19.5	121.3	55.	268.	-55.
091606Z	17.7 132.3	30	17.8 132.2	38.	8.			29.1	40.	51.	-18.		25.2	50.	148.	-50.		120.8	68.	386.	-40.
091612Z	17.8 131.8	35	17.8 131.8	35.	0.			29.5	45.	72.	-28.		26.6	58.	146.	-50.	17.2		68.	231.	-40.
0916182	18.1 131.1	40	17.9 131.0	35.	13			27.9	45.	95.	-48.		24.5	55.	187.	-45.	17.5	120.8	58.	269.	-50.
091700Z	18.3 130.5	45	18.6 138.8	40.	25			28.4	50.	78.	-48.		25.4		153.	-50.	18.5	122.0	65.	198.	-35.
891786Z	18.7 130.0	58	18.6 129.9	58.	8.			27.8	60.	49.	-40.		24.1	65.	95.	-35.	19.8	128.8	65.		-40.
<b>8917122</b>	19.1 129.6	65	18.9 129.5	50.	131			26.7	68.	29.	-40.		23.8	65.	82.	-35.	19.5	129.4	65.		-40.
0917182	19.2 129.1	85	19.8 128.8	80.	21			25.8	95.	80.	-5.			100.	144.		18.5	119.4	188.		0.
891888Z	19.5 128.3	98	19.6 128.5	98.		i. 20		25.8	100.	13.	-10.			115.	84.	15.	21.2	119.4	85.	297.	-10.
091006Z		100	20.0 127.8	95.	16			24.9	105.	33.	5.			115.	130.	10.	21.3	118.4	85.	358.	-5.
<b>891812</b> Z		100	20.2 126.9	108.				24.8	119.	8.	18.	21.1 1			95.	18.	21.1	128.1	90.	269.	5.
891818Z	20.3 126.6		29.2 126.3	100.				24.3		17.	18.				118.	18.	21.0	119.5	85.	386.	5.
8919882	20.6 125.9		28.8 126.8	105.	13			24.2		48.	10.		22.1	100.	151.	5.	22.1	119.8	88.	386.	5.
091906Z		188	20.8 125.3	105.				23.2	110.	56.	5.		20.5	98.	244.	e.	21.8	117.7	88.	447.	5.
091912Z	28.7 124.9		28.6 124.8	105.		. 21		23.0	105.	74.	ē.		21.0	98.	219.	5.	21.9	118.4	75.		8.
091918Z	20.7 124.6		20.8 124.2	105.		. 21		22.1		124.	5.		19.8	75.	200.	-5.	24.5		45.	587.	-38.
0920002	20.0 124.3		21.0 124.1	105.				22.3		155.	15.		21.9	90.	236.	15.	27.4	122.4	65.	331.	20.
892886Z	20.9 124.1		21.2 123.9	110.				23.5		98.	20.		22.2	95.	233.	20.	27.7		85.	387.	15.
0920122	21.0 124.3		21.0 124.0	110.					110.	87.	25.		23.7	90.	164.	15.	27.8	125.2	AA.	249.	10.
092018Z		100	21.0 124.0	110.	10. 10			23.6	110.	71.	30.		23.7	90.	183.	15.	27.8	125.2	86.	273.	5.
892188Z	21.1 124.7	95	21.0 124.8	98.	8			24.5	90.	46.	15.		24.4		175.	25.	25.8	124.8	85.	331.	5.
092106Z	21.2 124.8	98	21.2 124.6	90.	11.			24.5	90.	79.	15.		24.5		216.	28.	27.3		85.	360.	15.
0921122	21.4 124.9	85	21.8 124.8	98.				25.2	90.	56.	5.		25.1		222.	8.	28.8	125.8	68.	396.	-10.
8921182	21.8 124.8	80	21.6 124.3	85.		. 22		24.7	80.	148.	5.		24.2	70.	372.	-5.	26.8	123.4	68.	645.	-5.
892286Z	22.2 125.2	75	22.2 125.1	75.		). 23		25.5	70.	107.	5.	25.2 1		65.	355.	-15.	26.4	122.3	68.	756.	15.
092206Z	22.6 125.7	75	22.7 125.4	70.	18			26.2	50.	122.	-20.		25.4		332.	-35.	8.8	8.8		-0.	0.
092212Z	23.0 126.2	75	23.2 126.2	70.	12			27.6	55.	87.	-15.	27.8 1		45.	296.	-25.	0.0	0.0	ě.	-ē.	ē.
892218Z	23.6 126.9	75	23.5 126.6	70.	18			28.0	50.		-25.	28.2 1		40.	361.	-25.	0.0	0.0	ě.	-ē.	ē.
092300Z	24.2 127.4	65	24.1 127.5	65.	8. 6			30.1	50.	40.	-30.		32.1	40	319.	-5.	6.8	8.8	ě.	-0.	ē.
092306Z	24.8 128.4	78	24.7 128.2	65.	12			36.7	50.	180.	-20.	8.0	8.0		-8.	ĕ.	8.6	8.8	ě.	-ē.	ě.
<b>0923122</b>	25.7 129.2	70	25.9 129.5	70.	20. 6			33.5	50.	83.	-20.	0.0	8.0	6.	-0.	ē.	8.8	0.6	ě.	-0.	ě.
092318Z	26.8 130.2	75	26.8 130.2	65.	016			34.0	58.	81.	-15.	9.0	8.8	ě.	-0.	ě.	9.6	8.8	ě.	-ä.	e.
092400Z	27.7 130.6	80	20.0 130.5	78.	1916			33.4	45.	117.	ø.	8.0	8.8	e.	-8.	e.	8.8	0.0	ĕ.	-ē.	ě.
8924862	29.1 131.2	78	28.9 131.1	70.	13.			8.8	~J.	-B.	ø.	0.0	8.8	ø.	-B.	9.	0.8	0.0	ě.	-e.	8.
<b>0</b> 924122	31.2 132.1	78	30.0 132.2	79.		. 8		6.8	ě.	-0. -0.	Ð.	0.0	8.8	a.	~B.	Ð.	8.0	8.8	ă.	-8.	8.
8924182	33.3 132.5	65	33.6 132.8	79.		. 8		6.8	ě.	-0.	0.	0.0	0.0	ě.	-B.	ø.	8.6	9.0	e.	-0.	ě.
892588Z	35.5 132.5	45	35.7 132.7	45.	15.	. 8		6.0	ě.	-0.	R.	8.8	8.8	٥.	-8	6.	6.0	6.6		-8.	a.
0323 <del>00</del> 6	33.3 132.3	40	33.	45.	13.		. 0	0.0	٠.	-0.	٠.	0.0	0.0	٠.	-0.	٠.	0.0	0.0	٠.	٠.	٠.

	ALL FORECASTS				TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HK	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	15.	75.	201.	344.	14.	75.	201.	344.		
AVG RIGHT ANGLE ERROR	9.	49.	134.	263.	9.	49.	134.	263.		
AVG INTENSITY MAGNITUDE ERROR	4.	16.	20.	19.	4.	16.	28.	19.		
AVG INTENSITY BIAS	-1.	-5.	-9.	-10.	-1.	-5.	-9.	-10.		
NUMBER OF FORECASTS	37	33	29	25	35	33	29	25		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1647. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 8. KNOTS

#### TYPHOON KEN FIX POSITIONS FOR CYLLINE NO. 28

	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1 2	150600 151746	16.1N 134.4E 17.6N 134.6E		T1.8/1.0	INIT DOS BASED ON EXTRAP	PGTW PGTW
3	160000	17.4N 132.7E	PCN 6		BASED ON EXTRAP	PGTW
4 5		17.4H 132.3E 17.7H 132.6E	PCN 6	T2.8/2.8 /D1.8/21HRS	BASED DH EXTRAP	PG I W PGTU
6	160631		PCN 5	T1.5/1.5	INIT OBS	RPIK PG (W
8	161200	17.9N 132.5E	PCN 6		ULCC FIX	PGTW
10	161733	17.9N 131.1E 18.6N 131.6E	PCN 5		ULCC FIX ULCC FIX	PGTW PG (W
		17.9N 130.9E 17.9N 130.8E	PCN 6 PCN 6		ULCC FIX	PGTU PGTU
13	178888	19.2N 130.6E	PCN 6		BASED ON EXTRAP	PGTW
15	178618	18.6N 129.4E 18.6N 138.1E	PCN 5	T3.0/3.0 /D1.0/27HRS		PGT⊌ R^+1K
16 17	170900	18.8N 129.3E 18.9N 129.6E	PCN 6			PRTW PGTW
18	171600	18.9N 129.0E	PCN 6			PGTU PGTU
19 2 <del>8</del>	172188	19.2N 120.BE 19.5N 120.6E	PCN 2	T4.5/4.5 /D1.5/21HRS		PGYU
21 22	188388	19.7N 128.4E 19.8N 127.9E	PCN 2	T4.5/4.5 /D1.5/21HRS		PGTW PGTW
23 24	188688	28.6H 127.4E	PCN 1			PSTU PGTU
25	181288	20. IN 127.2E	PCN 2			PGTU
26 27	181688	20.1N 126.7E 20.1N 126.5E	PCN 4			PGTW PGTW
29	190000	28.5N 125.BE	PCN 2	T		PGTW
30	190554	28.5N 125.1E	PCN 1	T5.8/5.8 /D8.3/24#S T5.5/5.5	INIT OBS	PGTW RODN
		28.4N 125.2E 28.5N 125.8E				PGTW PGTW
33	191200	28.7N 124.8E	PCN 4			PGTW PGTW
35	191800		PCN 4			PGTW
36 37	191 <b>939</b> 1921 <b>88</b>		PCN 1 PCN 4			RODN PGTW
38	200000	28.BN 124.2E	PCN 2	T5.5/5.5 /08.5/24#RS		PGTU
40 40	200542	20.9N 124.1E	PCN 1	T6.8/6.8	INIT OBS	RPIK
41 42	200600 200900	21.8N 124 BE	PCN 2 PCN 2		•	PGTW PGTW
43	201200	21.6N	PCH 2			PGTU PGTU
45	201600	20.8N 124.3E	PCN 2	T5.5/5.5 /D8.5/244RS T6.8/6.8 T5.8/5.5+/48.5/244RS		PGTU
46 47	202100	21.1N 124.4E 20.9N 124.6E	PCN 2 PCN 4			PGTU PG TU
48	210300	21.2N 124.6E	PCH 4	T5.9/5.5+/W6.5/24HRS		PGTU PGTU
50	210900	21.8N 124.9E	PCN 4			PGTW
		21.7N 124.9E 21.6N 124.8E				PGTU PGTU
53	211888	21.6H 125.8E 21.6H 125.2E	PCN 4			PGTU PGTU
55	220000	22.1H 125.3E	PCN 4		ULCC FIX	PGTW
		22.4N 125.4E 22.5N 125.6E	PCN 4 PCN 3			PGTU PGTU
			PCH 4 PCH 3	T4.8/4.5 /U1.8/27HRS T4.5/4.5	INIT OBS	PGTU RPHK
68	220900	22.5H 125.7E 22.9H 125.7E 22.9H 126.8E 23.0H 126.1E 23.2H 126.3E 23.3H 126.5E 23.6H 127.3E 24.1H 127.3E 24.4H 127.3E	PCN 4			PGTU
61 <b>62</b>	221200 221600	23.2H 126.3E	PCN 4 PCN 4		EXP LLCC	PGTW PGTW
63 64	221883 222188	23.3N 126.5E	PCN 3			PGTW PGTW
65	238666	24.1N 127.3E	PCN 4			PGTIJ
	F-30-300	E-1111 1E0.0E	ren s			PGTU PGTU
68 69	238686 238648	24.9H 128.3E 24.8H 128.5E	PCH 4 PCH 3	T4.0/4.0-/\$0.0/24RS T4.5/4.5 /\$0.0/24RS		PG (U RPI1K
78	238900	25.4H 128.8E	PCH 4			PGTU PGTU
71 72	231200 231600	25.8H 129.3E 26.4H 129.9E	PCN 4		EXP LLCC	PGTW
	231751 232188	26.7N 138.1E 27.2N 138.5E	PCH 3 PCH 4		EXP LI.CC	PGTU PGTU
75	240000	27.7N 138.9E	PCH 4			PGTU PGTU
76 77	246366 246453		PCN 4 PCN 1	T4.8/4.8 /UB.5/22HRS		RPMK
78 79	240600 240900	29.0N 131.5E 30.0N 132.3E	PCN 4 PCN 4	T4.8/4.8-/98.8/24IRS		PGTU PGTU
88	241266	31.6N 132.5E	PCN 4 PCN 4			PGTU PGTU
81 82	2416 <b>00</b> 241730	32.9H 132.6E 33.2H 132.6E	PCH 3		ULCC FIX	PGTU
83 84	241938 242188	33.8N 134.2E 35.3N 132.4€	PCH 5 PCH 6	14.8/4.5 /AB.5/24RS		RPHK PGTU

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL		MRX-SFC-UND VEL/BRG/RNG	MRX-FLT-LVL-UND DIR/VEL/BRG/KNG			YE ORIEN- RM/TATION	EYE TEMP	
1234567891011213415167189120122234256272893832333	248184 248938	17.7H 132.7E 17.9H 132.2E 18.4H 139.8E 18.9H 139.9E 19.3H 129.9E 19.3H 129.9E 19.3H 129.7E 19.9H 127.4E 20.6H 125.2E 20.6H 124.4E 20.9H 124.4E 21.9H 124.4E 21.9H 124.4E 21.9H 124.4E 21.9H 124.8E 21.9H 124.8E 21.9H 124.8E 21.9H 125.2E 21.9H 125.2E 22.7H 125.0E 22.7H 125.0E 23.9H 127.5E 25.7H 129.1E 27.5H 130.3E 27.9H 130.3E 27.9H 130.3E 27.9H 130.3E 27.9H 130.3E	7:8019 7:8019	2566 938 2584 2632 2725 956 2662	35 650 65 35 628 35 45 348 11 59 278 18 59 278 18 100 268 18 100 240 7 100 010 18 100 360 12 65 360 12 65 360 68 56 266 98 66 360 28 66 360 28 67 220 78 55 360 83 68 100 120 78 240 120 88 218 68 55 218 68 55 361 28 88 218 68 55 361 28 88 218 68 578 228 52	868 29 349 45 128 35 636 128 248 36 159 15 638 46 310 58 128 88 10 10 658 92 886 8 668 84 360 18 268 99 146 68 656 95 166 26 356 86 260 48 650 67 316 28 356 86 260 48 650 67 316 28 356 86 260 48 650 67 316 28 356 86 260 56 260 69 160 26 260 69 160 26 260 69 160 26 260 69 260 56	8 5 18 2 2 2 1 1 3 2 5 2 3 1 2 2 3 1 2 2 3 1 2 2 3 1 2 9 10 6 10 4 7 7 5 10 10 10 10 3 3 7 7 7 3 3 5 5 10	CIRCULAR 25 CIRCULAR 25 CIRCULAR 16 CIRCULAR 16 CIRCULAR 35 CIRCULAR 35 CIRCULAR 48 CIRCULAR 48 CIRCULAR 15 CIRCULAR 15 CIRCULAR 15 CIRCULAR 15 CIRCULAR 25 CIRCULAR 27 CIRCULAR 27 CIRCULAR 37 CIRCULAR 37 CIRCULAR 37 CIRCULAR 38 CIRCULAR 37 CIRCULAR 37 CIRCULAR 37	8 150	+24 +25 +24 +18 +22 +22 +12 +16 +14 +13 +14 +11 +18 +14 +18 +11 +17 +18 +11 +18 +12 +16 +17 +14 +16 +16 +16 +14 +16 +17 +13 +14 +19 +14 +12 +15 +15 +11 +12 +12 +18 +18 +18 +11 +11 +18 +12 +18 +11 +11 +18 +11 +11 +18 +13 +15 +12 +13 +15 +12 +13 +14 +13 +11 +13 +12	344 455 66667777888999189112112112114114141414141414141414141414
	RADAR FIXES										
FIX NO.	TIME (Z)	FIX POSITION	RADAR AC	EYE CRY SHAPE	EYE DIAM	RADOB-CODE ASUAR TODFF	c	COPPENTS	I	RADAR POSITION	SITE UMO NO.
27 28 29 30 31	248188 248388 248488 248588 248688	20. 2N 124. 9E 20. 2N 124. 9E 20. 3N 124. 4E 21. 3N 124. 4E 21. 3N 124. 4E 22. 3N 125. 4E 23. 3N 126. 6E 23. 6N 126. 7: 1E 24. 1N 127. 4E 24. 1N 127. 4E 24. 1N 127. 4E 24. 1N 127. 9E 24. 6N 127. 9E 24. 6N 120. 4E 24. 9N 120. 4E 24. 9N 120. 4E 24. 9N 120. 4E 24. 9N 120. 4E 26. 9N 130. 4E 27. 1N 130. 7E 27. 4N 130. 5E 27. 4N 130. 5E 27. 6N 130. 6E 28. 6N 131. 6E 28. 6N 131. 2E 35. 6N 132. 4E	I.AND LAND LAND LAND LAND			359/4 78008 359/4 48000 15// 63586 354/3 4/// 353/3 50000 6/// 5/// //// //// 50488 6591/ 78508 6591/ 78508 6591/ 78508 21912 70613 21912 70612 20912 70612 21912 70613 21942 70612 65/// 50316 65/// 70216 65/// 70216 65/// 70216 65/// 70316 65/// 70316 65/// 30316 65/// 30316 65/// 30316 55/// 30316				8. 4N 122.0E 8. 4N 122.0E 9. 4N 122.0E 9. 4N 122.0E 9. 4N 122.0E 9. 4N 122.0E 6. 4N 127.0E 6. 2N 127.0E	98136 98136 98136 98136 98136 98136 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47939 47939 47939 47939 47909 47909 47909 47909 47909 47909 47909 47909 47909
	TIME (Z)	FIX POSITION		Y NEAREST DATA (NM)		CONTENTS					
2	241800	26.6N 138.1E 33.2N 132.5E 34.6N 132.6E	865 865 845	888 858 828	UMD 479 UMD 476 UMD 477		MO 47897				

TROPICAL STORM LOLA BEST TRACK DATA

BEST TRACK WARNING ERRORS						24 HOUR FORECAST ERRORS					48 HOUR FORECAST ERRORS					72 HOUR FORECAST						
						EK	(UKS				2,000	ALC:				FIGURE	RS .				RRORS	
HD/DA/HR	POSIT	MIND	PQ:	SIT	MIND	DST	MIND	PO	SIT	WIND	DST	MIND	POS	IIT	UIND	DST	WIND	POS	IT.	MIHD	DST	JIND
891588Z	22.8 168.	1 25	0.0	8.6	8.	-0.	0.	8.6	8.8	8.	-8.	8.	8.8	8.8		-8.	8.	8.0	8.6	8.	-e.	8.
8915862	22.7 166.	9 25	8.8	0.0	8.	-8.	8.	8.8	6.8	8.	-8.	Ä.	8.8	0.0		-0.	A.	8.8	8.6	8.	-8.	8.
6915122	23.3 165.	= ==	0.0	8.0	6.	-0.	ě.	0.0	8.8	Ä.	-0.		8.8	8.8	- 1	-8.		0.0	8.6		-0.	ě.
<b>69</b> 15182	24.0 164.		0.0	9.0	8.	-8.	ě.	0.6	4.6		-ē.	Ξ.	8.8	0.0	Ξ.	-8.	¥.	8.8	0.0	Ι.	-ā.	ē.
891600Z	24.5 163.		0.8	8.6	Ξ.	-8.	Ζ.	8.8	8.8		-ë.	٠.	8.0	8.8	- E-	-8.	٠.	8.8	8.6	۵.	-6.	-
					-0.		٠.					٠.				•••		= -=	= - =		-0.	٠.
<b>09</b> 16862	25.1 162.	3 35	25.2	162.3	30.	6.	-5.	28.5	158.2	45.	52.	~5.	33.2	159.1	55.	105.	10.	0.0	8.6	8.	-0.	Θ.
<b>69</b> 1612Z	25.6 161.	3 40	25.6	161.3	36.	e.	- i <b>6</b> .	28.6	158.2	45.	34.	-5.	33.2	159.1	55.	211.	18.	8.8	8.8	8.	-8.	8.
<b>69</b> 1618Z	26.2 168.	3 45	26.2	160.3	38.	8.	-15.	29.7	158.8	45.	48.	8.	34.5	168.8	58.	322.	5.	8.8	0.0	8.	-8.	8.
8917882	26.9 159.	5 45	27.5	159.3	35.	38.	-10.	33.7	168.2	50.	152.	5.	40.0	172.3	4	289.	ē.	0.0	8.8		-0.	٥.
8917862					45.	36.	-5.				198.	Ξ.			٠.		= -			Ξ.	=-	
							-3.	35.5				٠.	8.0	8.8		-6.	e.	6.8	0.0	٠.	- <b>e</b> .	٥.
<b>09</b> 1712Z	20.8 158.	8 50	20.6	159.2	50.	24.	●.	35.8	162.8	45.	93.	8.	6.8	8.8	٠.	-0.	e.	6.8	8.8	Ð.	-0.	8.
<b>6</b> 91718Z	29.9 158.	9 45	30.0	159.3	45.	22.	8.	35.8	166.6	45.	98.	8.	8.8	8.8	8.	-0.	0.	6.6	8.0	е.	-8.	8.
891888Z	31.2 159.	7 45	31.4	168.5	50.	43.	5.	36.2	170.3	40.	43.	Ä.	8.8	8.8	À.	-8.	ø.	0.0	8.8	a.	-8.	8.
891886Z	32.5 161.	a 45	32.2	161.2	45.	21.	<u> </u>	0.8	0.0	e.	-8.	Ι.	6.6	8.8	<u>.</u>		Ξ.	0.0	8.8		-a.	Ξ.
					:= :		٠.			Ξ.	_	Θ.			٠.	-0.	ø.			٠.		Ð.
<b>69</b> 1812Z	33.5 163.	3 45	33.7	163.1	45.	16.	8.	8.8	8.8	₽.	-8.	₽.	8.8	6.0	e.	-0.	Ð.	0.0	8.8	0.	-0.	8.
<b>69</b> 18182	34.3 166.	5 45	34.2	166.3	45.	12.	8.	8.8	8.8	8.	-8.	0.	8.0	8.8	a.	-0.	Ð.	0.0	8.8	A.	-0.	0.
691966Z	35.5 170.	1 40		178.0	4	30.	•	3.5	8.0		-8	Ξ.	8.6	8.8	- 1	-0.	Ξ.	8.8	0.0		.0.	ē.
22 1 200E	44.4 110.				⊸.	<del></del> .	٠.	9.0		•••	•••		0.0	3.0	٠.	~0.	o.	0.0	5.0	9.	٠.	٠.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS							
	<b>URNG</b>	24-1根	48-1根	72-1歳	LIRNG	24-HR	48-HR	72-HR				
AVG FORECAST POSIT ERROR	21.	88.	232.	8.	0.	Θ.	0.	₿.				
AVG RIGHT ANGLE ERROR	14.	68.	152.	8.	Ð.	8.	8.	8.				
AVG INTENSITY MAGNITUDE ERROR	4.	2.	6.	0.	0.	ø.	8.	0.				
AVG INTENSITY BIRS	-3,	-1.	6.	8.	e.	Θ.	8.	€.				
NUMBER OF FORECASTS	12	8	4	8	8	ē	8					

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1424. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 15. KNOTS

TROPICAL STORM LOLA FIX POSITIONS FOR CYCLOHE NO. 21

### SATELLITE FIXES

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COPPENTS	SITE
1	150318	22.5N 167.9E	PCN 6	T1.5/1.5	INIT UBS ULCC FIX	KGWC
Ž	151603	24. IN 164.5E	PCN 6		ULCC FIX	KGWC
3	151684	24.1N 164.3E	PCN 6			PGTW
4	152188	24.4H 163.9E	PCN 6		ULCC FIX	PGIW
5	160000	24.2H 163.4E	PCN 6	T2.0/2.0	INIT OBS	PGTW
6	160300	24.8N 162.8E	PCN 6			PGTW
7	160600	25.2N 162.3E	PCN 6			PGTU
8	160900	25.0H 161.7E	PCN 6			PGŢU
. 9	161600	26.0H 161.0E	PCN 6			PGTW
10	161800	26.2N 160.8E	PCN 6			PGTW
11	162100	26.8N 159.8E	PCN 6			PGTU
12	170000	26.8N 159.5E	PCN 6	T3.8/3.8 /D1.8/24/RS		PGTU
13 14	178436 178688	27.8N 158.9E 27.8N 158.9E	PCN 6			PGTU PGTU
15	178900	28.1N 159.4E	PCN 6			PGTU
16	171280	28.7N 159.1E	PCN 6		ULCC FIX	PGTU
17	171600	29.5N 159.2E	PCN 6		OCCC PIA	PGTW
18	171900	30.3N 159.6E	PCN 6			PGTU
19	172166	38.8H 159.9E	PCN 6			PGTU
20	100000	38.9H 159.4E	PCH 4	T3.8/3.8 /S8.8/24HRS		PGTW
21	188424	31.9N 168.6E	PCN 3			PGTW
22	188688	32.4N 161.2E	PCN 4			PGTU
23	188988	32.8N 162.2E	PCN 6			PGTU
24	181288	33.3N 162.9E	PCN 6			PG TU
25	181600	33.5N 165.5E	PCN 6			PGTW
26	191999	34.1N 166.3E	PCN 6			PGTU
27	182100	34.5N 168.1E	PCN 6			PGTW
28	190000	36.8N 178.9E	PCN 6	T2.8/2.5 /U1.8/24HRS		PR IW

HOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND HOT USED FOR BEST TRACK PURPOSES.

### TROPICAL DEPRESSION 22 BEST TRACK DATA

BEST TRACK	WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
	POSIT WIND DST WIND 18.2 139.5 30. 27. 8.		POSIT WIND DET WIND 0.8 0.8 60. 0.	POSIT WIND DST WIND 8.8 8.8 66. 6.
092110Z' 20.7 137.6 30	18.9 139.5 38. 67. 8. 21.8 138.5 38. 43. 8.	D.D D.O DD. D.	0.0 0.0 U0. 0. 0.0 0.6 00. 0.	6.6 B.6 G6. G. 6.6 B.6 G6. G.
	21.4 136.6 38, 16, 9, 22.3 135.9 28, 21, -5.		0.6 0.0 00. 0, 0.6 0.0 00. 0,	6.8 8.6 68. 6. 9.8 8.8 88. 8.

	ALL	FORECAS	115		TYPHO	35 KTS		
	LIRNG	24-HR	43-HR	72-HR	URNG	24-HR	40-HR	72-HR
AVG FORECAST POSIT ERROR	35.	155.	8.	0.	8.	٥.	8.	Ð.
AVG RIGHT ANGLE ERROR	21.	83.	0.	e.	ē.	ā.	e.	ö.
AVC INTENSITY MAGNITUDE ERROR	1.	15.	Ø.	8.	8.	ě.	0.	6.
AVG INTENSITY BIRS	-1.	15.	6.	ě.	ð.	ä.	8.	Đ.
HUMBER OF FORECASTS	5	1	ě.	Ď.	¥.	Ξ.	Ξ.	Ĭ.

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 282. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TROPICAL DEPRESSION TD22
FIX POSITIONS FOR CYCLONE NO. 22

### SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1 2 3 4 5 6 * 7 * 8	210000 210300 210600 210900 211200 211600 211000 212100 220000 220300	17.4N 139.8E 18.1N 139.0E 18.4N 140.8E 18.6N 140.8E 19.5N 139.4E 21.2N 130.0E 21.2N 139.5E 21.4N 139.7E 21.2N 137.0E 21.2N 137.0E	PCN 6 PCN 4 PCN 4 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6	T1.8/1.8  T1.6/1.6 /50.6/24#S	INIT OBS	PETU PETU PETU PETU PETU PETU PETU PETU

### AIRCRAFT FIXES

FIX NO.	TIME (2)	FIX POSITION			MAX-FLT-LVI-UND ACCRY EYE DIR/VEL/BRG/RIG NAV/MET SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ EH/ DP/SST	HSN NO.
1 2		16.7N 148.5E 21.1N 136.9E			828 22 288 58 12 12 250 18 368 18 12 5		+27 +25 25 +25 +25 +25 27	1 2

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

SUPER TYPHOUN HAC REST TRACK DATA

The second section of the second section is a second secon

	BEST TRACK	LIARN	ING ERRORS	24 11	OUR FO	RECAST ERRORS	48 F	RECAST ERRORS	72	72 HOUR FORECAST ERRORS				
HD/DA/HR	POSIT WIND	POSIT WIND	DST WIND	POSIT	MIND	DST WIND	POSIT	MIND	DST WIR	IN POSIT	MIND	DST WIND		
188186Z	11.6 151.6 26	8.6 8.6 8.	-B. B.	6.6 6.6	8.	-0. 0.	8.8 8.8		-0.			-0. 0.		
1881862	11.9 151.8 20	8.0 8.0 8.	-6. 8.	6.6 6.6	Ä.	-0. 0.	0.0 0.6		-0.		0 0.	-0. 0.		
1001122	12.6 158.2 25	12.6 150.2 25.	36. 8.	13.3 147.3	35.	6718.	14.8 144.3		844			11378.		
1861182	12.0 149.4 30	12.4 149.1 30.	30. 6.	13.0 145.6	45.	275.	13.4 142.6		593			12365.		
1802002	12.1 148.5 30	11.9 148.5 38.	12. 6.	12.2 146.3	45.	11015.	12.7 144.		2114			32175.		
188286Z	12.5 147.5 48	12.4 147.5 40.	6. 0.	13.4 143.8	50.	820.	14.9 141.8		7850		6 70.	17465.		
188212Z	12.6 146.4 45	12.8 146.5 48.	135.	13.8 143.2	55.	1830.	15.5 141.1		6561			9150.		
1802182	12.6 145.4 58	12.9 145.4 45.	105.	14.3 142.4	65.	1325.	16.0 140.0	90.	604		1 115.	4418.		
100300Z	13.1 144.5 60	12.8 144.7 55.	215.	13.2 141.6	75.	7925.	13.8 138.2		13945			26510.		
100306Z	13.3 143.7 70	13.3 143.7 70.	8. 8.	14.0 139.0	110.	76. 0.	14.6 135.7		16310	. 15.2 131	6 140.	346. 20.		
1003122	13.7 142.9 65	13.7 142.8 85.	6. 0.	14.8 139.2		5510.	15.8 135.3		120.		5 130.	310. 0.		
100318Z	14.2 142.2 98	14.1 142.2 98.	6. 0.	15.8 138.6	120.	2410.	17.3 134.6	130.	93. 5	5. 19.1 131	2 130.	263. 5.		
1004002	14.5 141.4 100	14.5 141.2 90.	12. ~10.	16.8 137.9	100.	2440.	17.3 134.5	110.	116	5. 19.3 131	3 120.	281. 0.		
199496Z	15.0 140.6 110	14.9 148.7 95.	815.	16.5 137.8	185.	1330.	17.9 134.8	115.	109	5. 19.3 131	3 125.	352. 10.		
100412Z	15.3 140.0 125	15.5 140.0 125.	12. 0.	17.8 138.8	130.	120. 0.	19.9 138.2	115.	16115	5. 22.0 138	0 100.	18915.		
100418Z	15.7 139.0 130	16.2 139.0 130.	30. O.	19.4 137.6	135.	116. 10.	22.2 137.2	115.	12210	3. 24.7 137		d8. −15.		
100500Z	16.1 138.3 140	16.2 138.2 140.	9. 0.	17.9 135.6	120.	48. 5.	20.2 133.8	119.	14010	3. 22.4 1 <b>3</b> 2.	9 104.	4911 <b>8.</b>		
1005062	16.6 137.6 135	16.6 137.7 148.	6. 5.	10.3 135.1	115.	815.	20.7 133.5	105.	20016			5025.		
1 <b>00</b> 512Z	17.2 136.8 130	17.2 136.9 135.	6. 5.	19.1 134.4		9615.	21.7 133.1		22816			5975.		
100510Z	17.9 136.3 125	17.8 135.9 125.	24. 0.	20.2 133.8	105.	10326.	22.5 132.5		30019		4 98.	√355.		
1006002	18.6 136.0 115	19.7 135.8 115.	13. 0.	21.8 134.2		6820.	26.5 134.1	<b>85.</b>	19029		2 65.	26028.		
1 <b>00606</b> Z	19.6 135.5 120	19.4 135.4 115.	135.	22.2 134.2		11415.	25.3 133.9		36129		4 65.	42215.		
1 <b>006</b> 12Z	20.4 135.4 130	20.6 135.3 120.	13. ~10.	25.8 135.2		8718.	31.8 139.2		43 10		0 0.	-0. 0.		
1006182	21.2 135.3 125	21.2 135.1 120.	115.	25.9 135.2		82i0.	32.0 139.5		169		0 0.	-0. 0.		
100700Z	22.0 135.4 120	21.9 135.2 120.	13. 0.	26.2 136.8	100.	11710.	32.8 142.3			5. 9.0 0	0 0.	-0. 0.		
1 <b>00</b> 706Z	23.5 135.7 115	23.3 135.8 115.	13. 0.	30.9 149.4	95.	12310.	36.2 157.2		53220			-0. 8.		
	24.5 135.9 115	24.6 136.0 115.	8. 8.	31.8 141.6	90.	83LO.	0.0 0.8	0.	-0. (			-0. 0.		
	26.1 136.7 110	26.0 136.8 110.	B. Ø.	33.7 145.2	80.	14115.	8.0 8.9	0.	-0. 6			-0. 0.		
	27.7 137.4 110	27.7 137.3 110.	5. 8.	35.2 149.2		2405,	9.0 9.6			. 0.0 0.		-0. 0.		
	29.8 138.4 105	29.6 138.8 105.	24. B.	36.0 153.0	78.	36710.	0.0 0.0			. 0.0 8		-6. 6.		
	31.6 140.0 100	31.8 139.7 100.	19. 0.	0.9 0.0	ø.	-0. 0.	0.0 0.0			. 0.0 0.		-0. 6.		
1008 19Z	33.4 142.4 95	33.8 142.3 90.	255.	0.6 0.0	₽.	-0. 0.	0.0 0.0	. <b>e</b> .		9.0 0		-0. 0.		
100900Z	34.5 144.4 85	34.7 144.0 85.	23. 0.	8.8 8.8	0.	-0. 0.	0.0 6.0	0.		0.0 0		- <del>0</del> . 8.		
1 <b>00</b> 906Z	35.4 146.3 80	35 2 146.3 88.	12. Ø.	0.0 0.0	Θ.	-0. 0.	0.0 0.8	0.	-0. (	9. 9.0 0.	0 0.	-0. B.		

	ALL	FORECAS	TS		TYPHO	ONS WHI	35 K 18		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	14.	90.	162.	294.	13.	90.	162.	294.	
AVG RIGHT ANGLE ERROR	13.	63.	164.	149.	12,	63.	184.	149.	
AVG INTENSITY MAGNITUDE ERROR	2.	14.	21.	24.	3.	14.	21.	24.	
AVG INTENSITY BIAS	-2.	-13.	-20.	-20.	-2,	-13.	-20.	-20.	
NUMBER OF FORECASTS	32	28	24	28	29	28	24	20	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2287, NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNO

SUPER TYPHOON MAC FIX POSITIONS FOR CYCLONE NO. 23

### SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMPENTS	SITE
1	818888	12.5N 152.8E	PCN 6	T1.0/1.0	INIT ORS	PG TU
2	010300	12.4H 151.5E	PCN 6			PGTW
3	010510	12.6N 151.0E	PCN 5			PGTU
4	010600	12.5N 150.0E	PCN 6			PGTW
5	01 <del>0900</del>	12.7N 151.0E	PCN 6		ULAC FIX	PGTU
6	0112 <del>00</del>	12.7N 150.1E	PCN 6			PGTW
7	011600	12.2N 149.1E	PCN 6			PGTU
8	011800	12.8H 148.7E	PCN 6			PGTW
9	012100	12.0N 148.4E	PCN 6			PGTU
10	62 <del>66</del> 66	11.8N 148.6E	PCN 6	T2.0/2.0 /D1.0/24HRS		PGTW
11	828388	12.2N 148.8E	PCN 6		BASED ON EXTRAP	PGTW
12	628458	12.8N 147.6E	PCH 5			PG TU
13	020600	12.6N 147.4E	PCN 6			PGTW
14	82 <del>8988</del>	12.9N 146.8E	PCH 6		BASED ON EXTRAP	PGTW
15	621266	12.9N 146.2E	PCN 6			PG TU
16	<b>0</b> 216 <b>00</b>	12.6N 145.3E	PCN 6			PGTW
17	621743	12.6N 145.6E	PCN 5			PG NJ
18	<b>821888</b>	12.6N 145.5E	PCN 6			PGTU
19	022100	12.9N 144.9E	PCN 6			PGTU
20	03 <del>0000</del>	13.1N 144.7E	PCN 6	T4.8/4.8+/D2.8/24#RS		PGTW
21	636366	13.3N 144.2E	PCH 4			PGTU
22	030446	13.4N 143.9E	PCN 4			PGTW
23	838688	13.4N 143.0E	PCN 2			PGTW
24	030900	13.6N 143.4E	PCN 2			PGT⊔

25	031200	13.6N 143.8E	PCN 4			PGTW
26	931699	14.1N 142.3E	PCN 4			PGTW
27	031731	14.3N 142.0E	PCN 3			PG (U
28	831888	14.3N 142.BE	PCH 4			PGTU
29	832188	14.3N 141.7E	PCN 4			PGTW
30	848666	14.5N 141.5E	PEN 2	T5.8/5.8 /D1.8/24#RS		PGTW
31	040300	14.8N 141.1E	PCN 2		EYE DIN 28HM	PGTU
32	648434	15.8N 140.7E	PCN 1		EYE DIA ZONM	PGTU
33	040600	15.1H 148.6E	PCN 2			PGTW
34	648966	15.2N 140.3E	PCN 2		EYE DIA 20MI	PGTU
35	841200	15.5N 148.BE	PCH 2			PGTW
36	641686	15.7N 139.2E	PCN 2			PGTU
37	841719	16.1N 139.1E	PCH 1			PGTU
38	841900	15.8N 139.1E	PCN 2			PGTU
30	842188	16.0N 139.7E	PCH 2			PGTU
48	658888	16.3N 138.4E	PCN 2	T6.0/6.0 /D1.0/24HRS		PGTW
41	858300			10.070.0 701.0724W3		PGTW
	<b>050</b> 684	16.5N 130.0E	PCN 2			PGTM
42	<b>05090</b> 0	16.7H 137.8E	PCN 1		EVE DIG IEUM	PGTW
43		17. IN 137.2E	PCN 2		EYE DIA 15MM	
44	<b>651266</b>	17.4N 137.0E	PCH 2			PGTU
45	<b>85</b> 16 <b>00</b>	17.6H 136.1E	PCN 4			PCTU
46	051000	17.8H 136.0E	PCH 4			PSTU
47	852100	18.3N 136.0E	PCN 4			PSTW
49	969999	18.5N 136.1E	PCN 2	T5.0/6.0 /U1.0/24R5		PGTU
49	868408	19.2N 135.7E	PCH 2			PGTU
58	868552	19.6N 135.7E	PCH 2			PGTU
51	060900	20.0N 135.6E	PCN 2			PGTW
52	861288	20.4N 135.4E	PCN 2			PG TW
53	961699	20.8N 135.2E	PCN 2			PGTW
54	661866	21.1N 135.1E	PCN 2			PGTW
55	862188	21.4H 135.3E	PCH 2			PGTW
56	870000	21.8H 135.5E	PCN 2	T6.0/6.0-/D1.0/244RS		PGTW
57	878480	22.8N 135.7E	PCN 2			PGTW
58	070540	23.4H 135.8E	PCN 1			PGTW
59	87 <del>8900</del>	27.9N 135.9E	PCN 2			PGTW
68	0712 <del>08</del>	24.5N 136.1E	PCH 2			PGTW
61	<b>6</b> 716 <b>00</b>	25.5N 136.5E	PCH 2			PGTW
62	871609	26.8N 136.6E	PCN 2			PGTW
63	<b>6</b> 721 <del>88</del>	26.9N 137.8E	PEN 2			PGTW
64	999999	27.6N 137.5E	PCN 2	T5.0/5.0 /W1.0/24HRS		PGT⊎
65	<b>0</b> 90400	28.9N 138.2E	PCN 2			PGTU
66	<b>888</b> 527	29.7N 138.5E	PCN 1			PGTW
67	<del>080</del> 900	30.7N 139.4E	PCH 6			PGTW
68	081200	31.4N 140.0E	PCN 4			PGTW
69	<b>9</b> 816 <b>99</b>	33.2N 142.1E	PCN 6		ULCC FIX	PGTW
* 70	081912	34.0N 143.7E	PCN 5		ULCC FIX	PGTW
71	092100	33.9N 143.4E	PCN 4			PGTW
72	090000	34. IN 144. IE	PCN 4	T3.5/4.5 /W1.5/24HRS	ULCC FIX	PGTW
73	090400	35.1N 145.6E	PCN 4			PGTW

### AIRCRAFT FIXES

	TIME	FIX	FLT	700HB	OBS		SFC-				-LVL				EYE SHAPE			RIEN- ATION			EMP (		MSN NO.
HO.	(Z)	POSITION	LVL	HGT	MSLP	VEL	/BRG/	KMG	D I K	VEL.	/BKG	KING	NAV	THE I	SHAPE	אוע	1121	HIIUN	UU 14	111/	, tiles	7571	MU.
1	612284	11.9N 148.8E	1500FT		1000	30	858	20	120	36	030	24	7	2					+24	+23	+23	30	1
2	929139	12.2H 148.3E	1500FT		1000	25	290	20	298		220	14	7	5					+24	+24	+23	30	1
3	<b>02060</b> 1	12.4H 147.5E	1588FT		993	45	145	20	228		140	20		19									2
4	82 <del>898</del> 2	12.5N 146.9E	7 <b>00</b> 118	3050	1002				170		879	15		5						+13	+11		2
5	021505	12.7N 145.8E	786MB	2980					160		<b>09</b> 0	10	5	_					+16	+14			3
6	8218 <b>88</b>	12.6N 145.4E	7 <b>0011</b> 0	2929					199		090	5	5	1	ELLIFTICAL								3
7	022005	12.8H 145.2E	7 <b>00</b> mB	2928	981		290	98	928		<b>0</b> 20	10	5	2	ELL IPTICAL			150		+16			3
8	<b>030133</b>	13.2N 144.4E	7 <b>00118</b>	2810	966		030	5	140		648	7	5	2	ELI. IPTICAL	15	10	120	+12	+15			4
9	639666	13.3N 143.7E	7 <b>90</b> MB	2751			948	10	160		040	9	4	3						+17			5
16	030620	13.5N 143.4E	78 <b>0HB</b>	2700	955	60	150	30	689		350	11	5	2	ELL IPTICAL	18	8	<b>0</b> 90	+14	+18	+13		5
11	031211	13.8N 142.8E	7 <b>86HB</b>	2692					100		070	12	8	1									7
12	031436	13.9N 142.6E	788118	2688	954				200		139	19	5	1	C IRCULAR	8				+15			7
13	<b>0320</b> 15	14.2N 141.8E	7 <b>00118</b>	26 <b>90</b>	954		360	16	350		260	35	15	2	CIRCULAR	30				+15			8
14	640656	15.6N 139.9E	7 <b>86</b> 118	233 i	989	180	330	6	188		989	18	25	1	CTRCULAR	15			+11	+29	+ 1		9
15	<b>84</b> 1156	15.2N 140.BE	7001B	2291						112		10	15	1									9
16	842187	15.9H 138.6E	7 <b>0011</b> 8	2173	895	196	360	7	110		939	8	5	1	CIRCULAR	12				+24	+10		10
17	851889	17.1N 137.1E	700HB	2273	968				130		020	15	5	2	CONCENTRIC	67	40		+10	+21			11
10	<b>0</b> 512 <b>49</b>	17.4N 136.7E	7 <b>00HB</b>	2350					218		130	25	8	2									11
19	051924	18.0N 136.3E	7 <b>00H</b> 0	2372					230		110	28	10	5									12
20	<b>0</b> 52219	19.3N 136.0E	7 <b>0011</b> 0	2303	926		626	16	130		<b>858</b>	35	10	18	CONCENTRIC	12	25		+11	+17	+16		13
21	060704	19.8N 135.6E	700HB	2396		60	858	10	190	145		25	10	3									15
22	060931	20.1N 135.5E	7 <b>8019</b>	2332	914				278		188	25	15	5	C IRCULAR	25			+12	+28	+12		15
23	061913	21.2N 135.3E	7 <b>9811</b> 9	2314					199		030	10	5	5									16
24	062145	21.6N 135.3E	7 <b>86118</b>	2346	918	50	846	96	300	100	200	38	5	5	CIRCULAR	25				+17			16
25	070937	24.0M 135.0E	7 <b>0011</b> 0	2421	924				190		110	25	10	2	CIRCULAR	30			+13	+17	+15		19
26	871214	24.6N 135.9E	70 <b>0HB</b>	2441					100	63	<b>920</b>	30	10	2									18
27	071835	26.2N 136.7E	7 <b>00HB</b>	2467					280		169	19	7	3									19
28	872112	26.8N 136.8E	7 <b>00</b> 118	2500	932	98	100	60	198		100	30	7	4	ELL IPTICAL	30	20	146	+14	+17	+16		19
29	888627	29.8N 138.4E	700MB	2545		198	250	5	286	90	999	30	5	1									28
30	000053	30.7N 139.1E	780HB	2566	945				149	87	020	58	5	5						+22			20
31	982935	33.8N 143.0E	700HB	2733	959	88	898	120	210	100	130	199	3	5					+19	+20	+12		21
32	662332	34.4H 144.ZE	798(1B	2763					038	82	289	110	10	4									21

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE	RADOB-CODE ASUAR TDDFF	CONTENTS	RADAR POSITION	SITE
						• • • • • • • • • • • • • • • • • • • •				
1	828635	12.7N 147.3E	LAND	FAIR					13.6N 144.9E	91218
ż	020735	12.7N 147.3E	LAND	GOOD					13.6N 144.9E	91218
3	929835	12.7N 147.2E		GOOD					13.6H 144.9E	91218
4	020935	12.8N 147.1E	LAND	POOR					13.6N 144.9E	91218
5	021035	12,7N 146.7E	LAND	FAIR					13.6N 144.9E	91218
6	021135	12.7N 146.6E	LAHD	GOOD					13.6H 144.9E	91218
7	021235	12.8N 146.3E	LAND	GOOD					13.6N 144.9E	91218
8	021335	12.8N 146.2E	LAND	GOOD					13.6N 144.9E	91218
9	021435	12.8H 146.1E	LAND	GOOD					13.6H 144.9E	91218
10	021540	12.8N 145.8E	LAND	GOOD					13.6N 144.9E	91218
11	021640	12.8N 145.7E	LAND	FAIR					13.6H 144.9E	91218
12	0217 <b>35</b>	12.8N 145.7E		HAIR	CIRCULAR	25			13.6N L44.9E	91218
13	021835	12.8N 145.4E	LAHD	GOOD	CIRCULAR	25			13.6N 144.9E	91218
14	<b>0</b> 21935	12.8N 145.3E		FAIR					13.6N 144.9E	91218
15	022648	12.9H 145.1E		COOD	CIRCULAR	18			13.6N 144.9E	91213
16	022148	12.8N 144.8E		G00D	CIRCULAR	16			13.6N 144.9E	91218
17	<b>9</b> 22235	12.8N 144.6E		GOOD	ELL IPTICAL			FLIP AXIS 18/4	13.6N 144.9E	91718
10	030035	13.1N 144.5E		GOOD	CIRCULAR	11			13.6H 144.9E	91218
19	<b>030135</b>	13.1H 144.3E		GOOD	CIRCULAR	18			13.6N 144.9E	91218
20	030235	13.2H 144.2E		GDOD	C IRCULAR	9			13.6N 144.9E	91218
21	030335	13.2N 144.BE		GOOD	CIRCULAR	10			13.6N 144.9E	91218
22	<b>03043</b> 5	13.2N 143.9E		FAIR		14			13.6N 144.9E	91218
23	030535	13.3N 143.8E	LAND	FAIR		16			13.6H 144.9E	91216
24	838638	13.4N 143.8E		FAIR		11			13.6N 144.9E	91218
25	02883 <b>0</b>	13.5H 143.4E		POOR		13		OPEN N-SE	13.6H 144.9E	91218
26	031030	13.6N 143.2E		FAIR		7			13.6N 144.9E	91218
27	03113 <del>0</del>	13.6N 143.0E		FAIR		5			13.6N 144.9E	91218
28	031235	13,7H 142,8E		FAIR		6			13.6N 144.9E	91218
29	031335	13.8N 142.8E		FAIR		8		OPEN NE	13.6H 144.9E	91218
30	031435	13.8N 142.7E		GOOD		7		DPEN N	13.6H 144.9E	91218
31	031535	13.9H 142.2E		FAIR					13.6H 144.9F	91218
32	031E35	14. IN 142.2E		POOR					13.6H 144.9E	91218
33	000900	30.4H 138.9E					65/// /////		35.39 138.75	47639
34	081300	31.6N 141.2E					65/// 50749		35.3N 138.7E	47639
35	<b>082000</b>	34.2N 143.0E	LAND				35/// 50422		35.3N 130.7E	47639

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

	BEST TRACK	UARN ING ERRO		OUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
HD/DA/HR	POSIT WIND	POSIT WIND DST		WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
1010062	16.1 146.2 15	8.0 8.0 80.	0. 0.6 0.6		8.8 8S. A.	8.8 8.8 08. 0.
1010122	16.0 144.5 20	0.0 0.0 00.	0. 0.0 0.0	00. 0.	0.0 0.0 06. 6.	8.6 6.6 86. 8.
1818182	15.8 142.9 25	0.0 0.0 00.	0. 0.0 0.0	60. 0.	0.0 8.0 80. 8.	8.0 8.0 80. 8.
1811882	15.9 141.3 30	16.1 141.2 25. 13.	-5. 18.7 136.2		22.2 133.3 45. 38220.	27.9 133.9 55. 78045.
1011062	16.2 139.9 35	16.2 139.9 35. 8.	8. 17.8 135.2		21.6 132.2 55. 33715.	26.8 133.8 55. 76368.
1811122	16.2 138.5 48	16.3 138.5 40. 6.	6. 18.2 133.8		21.3 131.5 55. 32120.	26.8 133.0 55. 82758.
1011182	16.8 137.8 45	16.4 136.4 45. 42.	0. 18.3 132.2		21.2 130.3 55. 31625.	26.8 133.0 55. 87725.
101200Z	15.9 135.7 40	16.0 135.7 40. 6.	0. 16.2 130.8	58. 2115.	17.8 126.1 60. 6340.	19.4 120.4 50. 1215.
1812962	15.9 134.2 45	15.6 134.2 45. 18.	8. 15.7 129.3	55. 6815.	17.3 124.6 65. 7750.	19.2 120.0 55. 1425.
1012122	15.9 132.9 55	15.9 132.9 55. 6.	0. 16.3 127.1	75. 71. 8.	18.3 122.2 78. 6835.	28.1 117.2 68. 1745.
1812182	16.2 131.7 60	16.0 131.4 60. 21.	B. 16.9 125.7	75. 685.	18.8 120.8 68. 8428.	28.2 115.7 58. 18828.
1813862	16.4 138.5 65	16.5 130.4 65. 8.	0. 18.6 126.4		20.9 124.2 100. 326. 45.	23.1 123.1 110. 602. 35.
1813862	16.7 129.3 70	17.6 129.4 78. 19.	0. 19.2 125.8	98. 16225.	21.3 123.0 100. 304. 40.	24.3 123.0 110. 702. 35.
1813122	17.1 128.8 75	17.1 120.2 75. 11.	0. 18.8 124.2		21.2 120.8 85. 311. 20.	24.4 118.8 60. 56528.
101316Z	17.4 126.6 80	17.3 126.7 90. 9.	0. 19.2 121.9	85. 122. 5.	22.3 119.2 75. 355. S.	26.2 117.7 45. 65635.
161406Z	17.7 125.0 100	17.9 125.0 100. 12.	6. 26.6 128.4		23.8 117.3 78. 3945.	25.9 115.9 35. 60540.
1014062	17.6 123.5 115	10.2 123.3 115. 30.	8. 20.5 119.7	80. 204. 20.	23.8 116.9 70. 4615.	0.0 0.0 00. 0.
1814122	17.3 122.2 185	17.3 122.2 105. 0.	0. 16.3 117.0	65. 61. 8.	16.3 112.8 70. 6210.	17.0 107.9 00. 70. 5.
101419Z	17.4 128.9 88	17.5 120.0 80. 8.	0. 17.2 116.1	75. 8. 5.	19.0 111.2 85. 49. 5.	28.9 186.6 55. 7428.
101500Z	17.5 119.7 55	17.5 119.7 70. 0.	15. 17.7 114.8	85. 48. 10.	19.6 110.6 70. 775.	28.2 186.6 58. 9825.
101506Z	17.3 110.5 68	17.7 118.3 78. 27.	10. 17.6 113.4	90. 42. 15.	18.1 109.3 65. 3910.	19.9 105.5 45. 5725.
101512Z	17.2 117.3 65	17.3 117.2 65. 8.	0. 18.3 112.2	80. 79. 8.	20.5 108.2 55. 13420.	0.0 0.0 DO. D.
1815182	17.1 116.2 78	17.5 115.0 70. 33.	0. 19.0 118.8	80. 97. 0,	20.3 106.2 40. 9835.	6.0 0.0 0. <del>-0</del> . 6.
101500Z	16.9 114.7 75	17.0 114.0 70. 8.	-5. 16.8 189.9	65. 4210.	16.4 185.8 30. 15645.	0.0 0.0 00. 0.
1016062	16.9 113.3 75	16.8 113.2 75. 8.	0. 16.3 108.0	55. 9920.	0.0 0.0 0. <del>-</del> 0. 0.	0.0 0.0 00. O.
1016122	17.0 112.0 00	17.0 112.0 80. 0.	0. 17.7 187.4	60. 4315.	0.0 0.0 0 <b>0.</b> 0.	0.0 <b>6.0 6.</b> -0. 6.
101618Z	17.2 111.0 80	17.2 111.0 75. 0.	-5. 10.8 106.8	45. 630.	8.0 6.6 68. A.	0.6 <del>0</del> .8 80. 8.
1017 <del>0</del> 0Z	17.5 109.9 75	17.7 109.7 75. 17.	0. 19.2 105.7	45. 2!30.	9.9 9.9 90. 9.	8.0 0.0 0O. O.
101706Z	17.8 188.7 75	17.7 100.9 75. 13.	0. 10.8 104.9	30. 2140.	0.0 0.0 00. 0.	6.0 0.0 0. <del>-8</del> . 6.
1817122	18.3 187.8 75	18.2 107.7 88. 8.	5, 0.0 0.0	00. 0.	0.0 0.0 00. 0.	0.6 0.8 89. 8.
1617182	18.8 106.9 75	18.9 106.8 70. 0.	-5. 0.0 0.0	08. B.	0.0 0.8 00. 0.	0.0 <b>0.0 0</b> 0. 0.
101800Z	19.0 106.0 75	19.1 186.8 78. 6.	-5. 0.0 0.0	0. ~0. 0.	0.0 0.0 0. <del>-0</del> . 0.	0.0 0.0 O0. O.
101006Z	19.0 105.2 70	<b>6.0 6.0 60.</b>	0. 0.0 0.0	00. 0.	D.O 0.0 DD. D.	0.0 0.0 <b>0</b> 0. 0.

	ALL	FORECAS	iTS		TYPHOONS WHILE OVER 35						
	LIRNG	24-HR	48~HR	72-HR	WRNG	24-H	R 48-HR	72-HR			
AVG FORECAST POSIT ERROR	12.	86.	213.	438.	12.	86.	213.	430.			
AVG RIGHT ANGLE ERROR	10.	74.	175.	333.	10.	74.	175.	333.			
AVG INTENSITY MAGNITUDE ERROR	2.	12.	23.	27.	2.	12.	23.	27.			
AVG INTENSITY BIAS	Ð.	-6.	-12.	-18.	0.	-6.	-12.	-10.			
NUMBER OF FORECASTS	29	26	21	17	2B	26	21	17			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2488. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 13. KNOTS

TYPHOUN NANCY FIX POSITIONS FOR CYCLONE NO. 24

### SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMENTS	SITE
1	100503	16.1N 147.8E	PCN 3	T1.5/1.5	INIT OBS	PGTW
2	100900	16.3N 145.8E	PCN 6			PGTU
3	101200	16.1N 144.5E	PCN 6		ULAC FIX	PGTW
4	101600	15.8H 143.5E	PCN 6		ULAC FIX	PGTW
5	181988	15.7N 142.6E	PCH 6		ULAC FIX	rg tu
6	102100	15.9H 141.6E	PCN 6		ULAC FIX	PGTU
7	110000	15.9H 141.4E	PCH 4			PCTIJ
	110400	16.0N 139.8E	PCN 6	T2.5/2.5 /D1.0/23HRS		<b>ଧୀ</b> ନସ
9	118451	16.0N 139.6E	PCN 3			PGTW
10	110600	15.9N 140.1E	PCH 4			PG TU
11	110900	16.2N 139.2E	PCN 6			PGTU
12	111200	15.8N 138.8E	PCH 6		ULAC FIX	PGTW
13	111688	16.1N 137.3E	PCH 6		ULAC FIX	Pt-TW
14	111736	16.3N 136.6E	PCN 6		ULAC FIX	PGIW
15	112100	16.3N 136.1E	PCN 6		ULAC FIX	PGTU
16	120006	15.8N 135.5E	PCN 4			PG III
17	120400	15.8N 134.7E	PCN 4	13.8/3.0 /D0.5/24RS		PGTW
10	128621	15.9H 134.2E	PCN 3			PGH
19	120900	16.0N 133.9E	PCN 4			PRIM
20	121200	16.8H 132.8E	PCH 4			PG I W
21	121588	16.2N 131.0E	PCH 4			PIs DI
22	121966	16.3N 131.5E	PCN 4			PGTU
23	122106	16.4H 131.1E	PCN 4			PGTU

24	138666	16.4N 138.6E	PCH 4		ULCC FIX	Pictri
25	130300	16.6N 138.8E	PCN 2	T4.5/4.5~/D1.5/23HRS		FGTM
26	138689	16.8N 129.2E	PCH 1			PGTM
27	138689	16.9N 129.3E	PCN 1	T4.5/4.5	INIT OBS EYE DIA 6NM	RFIK
28	130900	17.1N 128.8E	PCH 2			PGTW
29	131200	17.2N 128.1E	PCH 4			PSTU
30	131600	17.4N 126.9E	PCN 2			PGTW
31	131854	17.6N 126.5E	PCH 1			FGRU
32	132100	17.6N 125.7E	PCH 2			PGHI
33	140000	17.7N 124.9E	PCN 2			ECIA
34	140300	17.8N 124.2E	PCN 2	T5.5/5.5 /D1.8/2/HRS		PGTU
35	148556	17.7N 123.4E	PCN 1			PGIU
36	140556	17.7N 123.4E	PCN 1	T6.0/6.0~/D1.5/24HRS		RFI11C
37	140900	17.7N 123.8E	PCN 2			FCTU
39	141200	17.7N 122.3E	PCN 2			FGTU
39	141688	17.7N 121.2E	PEN 6			PG FIJ
48	141888	17.7N 120.9E	PCN 6			PIFFIJ
41	141841	17.8N 128.5E	PCH 5			PG (W
42	142188	17.6N 120.0E	PCN 6		ULCC FIX	PGTW
43	150000	17.5N 119.6E	PCN 6	T4.5/5.8+/U1.8/21HRS	ULAC FIX	PGTH
44	156388	17.4N 119.1E	PCN 2	14.5, 5.6., 6.1.6, 2.1.8,5	02.10 7 17	PGTW
45	158688	17.5N 118.5E	PCN 2			PGTW
46	150726	17.4N 118.1E	PCN 5	T4.8/4.5+/W2.8/25HRS		REHK
	150720	17.4N 117.8E		14.8/4.3*/W2.0/23fik3		PGTW
47			PCN 2			
48	151200	17.7N 117.1E	PCH 4			PGTH
49	151688	17.7N 116.1E	PCN 6			PGTW
50	1518 <b>66</b>	17.6N 115.6E	PCN 6			PGTU
51	151829	17.2N 116.0E	PCN 5			RPMK
52	152 1 <del>68</del>	17.1N 115.2E	PCN 6			PG (1-J
53	160000	17.0N 114.4E	PCN 4			PGTU
54	160300	16.9N 113.8E	PCH 2	T5.0/5.0 /D0.5/27HRS		PG FU
55	160600	16.9N 113.4E	PCN 2			FGTW
56	160714	17.6N 113.8E	PCH 1	T4.5/4.5-/D8.5/24HRS		RPM/:
57	160900	17.8N 112.7E	PCN 2		EYE DIA 25NI1	PGTW
58	161200	17.8N 112.1E	PCN 2			PGTM
59	161688	17.2N 111.3E	PCN 2			PGTW
60	161800	17.3N 110.9E	PCN 2			PGTW
61	161959	17.4N 118.7E	PCN 1		EYE DIA 36NM	RITIK
62	162188	17.5N 118.4E	PCN 2		CIE DIA SONI	PGTU
63	179000	17.6N 109.9E	PCN 2			PGTU
64	170300	17.6N 189.4E	PCN 2	TE E & E - 400 E 44 MC		
65				T5.5/5.5-/D0.5/24HRS		PGTW
	178680	17.9h 108.9E	PCN 2	TE 9 6 9 09 5 0 4 100	ENE NIO AMUM	PGTW
66	170702	10.0N 108.3E	PCN 1	T5.0/5.0-/D0.5/24HRS	EAL DIN 18HM	RPHK
67	170900	18. IN 188. IE	PCN 2			PGTU
68	171200	18.4N 107.8E	PCN 2			PG (W
69	171600	18.7N 107.2E	PCN 2			PGŢIJ
70	171800	18.9N 106.9E	PCN 2			PGTW
71	171947	19.0N 106.7E	PCN 1			RP1 K
72	172100	19.0N 106.5E	PCN 2			PG NJ
73	180000	18.8N 106.0E	PCN 2			PG TW
74	180300	18.9N 185.7E	PCN 4	T4.0/5.0-/W1.5/24HRS		PGIW
75	180600	18.9N 105.2E	PCN 4			PGTW
76	180900	19.8N 105.8E	PCN 6		ULCC FIX	FGTW
77	181200	18.8N 104.7E	PCN 6		ULAC FIX	PGTW
78	181600	18.8N 185.8E	PCN 6			PGTW
79	181888	18.8N 184.9E	PCN 6			PGTU
98	200000	18.8N 104.3E	PCN 6			PGTU

### AIRCRAFT FIXES

FIX NO.	TIME (Z)	F1X POSITION	FLT LVL	700MB 0BS HGT MSLP	MAX-SF VEL/BR		MAX-FLT-LVL DIR/VEL/BRG				EYE SHAPE	EYE ORTEN:	EYE TEMP OUT/ IH/ DP	
1 2 3 4 5 6 7	110135 110543 110750 112114 112350 120613 120023	15.9N 141.2E 16.2N 140.1E 16.2N 139.4E 15.9N 136.2E 15.9N 135.7E 15.9N 134.2E 15.9N 133.8E	1500FT 1500FT 1500FT 1500FT 1500FT 700MB 700MB	1066 999 998 3032 999 998 2982 988 2930 985	25 36 40 36 25 25 40 01 35 27 50 30 55 27	0 10 8 48 9 20 8 38 6 18	228 28 138 118 52 838 348 21 258 168 58 918 848 55 38 850 38 388 160 63 838	98 98 28 48 98	5 10 10 8	5 1 2 10 4 3			+23 +23 +22 +31 +31 +24 +24 +22 + 9 +13 + 9	27 2 3 3 4 4
8 9 10 11 12	122005 122217 130615 130858 132158	16.2N 131.2E 16.3N 130.9E 16.6N 129.5E 16.8N 129.8E 17.7N 125.4E	708118 700118 700118 700118 700118	2868 975 2867 2838 2798 978 2616 946	50 09 80 04 75 35 100 14	9 12 9 20 9 5	060 73 360 130 76 060 190 78 140 020 73 350 100 117 040	27 40 50 10	5 15 15 15	2 3	C IRCULAR C IRCULAR C IRCULAR	18 26 12	+12 +17 +18 +14 +13 +14 +17 +18	5 5 6 <i>6</i> 7
13 14 15 16 17 18	140015 140701 140941 150725 151005 152123	17.8N 125.0E 17.6N 123.4E 17.5N 122.8E 17.2N 118.3E 17.0N 117.8E 17.1N 115.4E	70018 70018 70018 70018 70018 70018	2627 2547 2497 933 2955 2936 985 2852 973	65 84 68 34 55 36	9 5 9 13 9 30 9 65 9 60	150 45 040 040 63 350 110 82 360	15 18 30 40 20	10 5 5 5	1 2 5 5 3	CIRCULAR CIRCULAR CIRCULAR	2 <del>6</del> 35 50	+12 +21 + 9 +11 +15 + 8 +12 +12 +12	7 8 9 9 18
19	160023	16.9N 114.7E	7 <del>00118</del>	2849	70 98		068 79 368 R FIXES	75	18	5				10
FIX NO.	TIME (Z)	FIX POSITION	RADAR A	EY CCRY SHA		YE IAM	RADOB-CODE ASWAR TDDFF			(	COMMENTS		RADAR POSITION	SITE WMO NO.
1 2 3 4 5 6 7 8 9 10 11 12 13 14	140400 140600 140630 141300 141330 141500 141500 150300 150300 150300 150400 151200 151430	19.8h 124.8E 17.8h 123.6E 18.4h 123.6E 17.7h 122.0E 17.6h 121.9E 17.6h 121.9E 17.6h 121.6E 17.6h 119.7E 17.6h 119.7E 17.8h 118.8E 17.8h 118.9E 17.7h 118.7E 17.7h 118.7E 17.7h 116.7E	LAND LAND LAND LAND LAND LAND LAND LAND				//// 22982 //// 42618 4/// //// 11852 42513 11194 42518 12334 42718 10634 //// 129// 42718 129// 42708 129// 42705 1091/ 42710	ΕY	E 198	9 PC	ELPTCL 65/5 T ELLIPTICAL ELLIPTICAL	0 KMS	18.3N 121.6E 18.3H 121.6E 18.3H 121.6E 18.3N 121.6E 18.3N 121.6E 18.3N 121.6E 18.3N 121.6E 16.3N 120.6E 16.3H 120.6E 16.3H 120.6E 16.3H 120.6E 16.3H 120.6E	98231 98231 98231 98231 98231 98231 98231 98321 98321 98321 98321 98321 98321
					S	YNOPT	IC FIXES							
	TIME (Z)	FIX POSITION	INTENSI'		1)		CONTENTS							

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

UMO 98233 UMO 59981

1 141500 17.3N 121.8E 090 020 2 160900 17.0N 112.7E 000 030

### TROPICAL DEPRESSION 25 BEST TRACK DATA

	BEST TRAC	K	WARN ING		24 1	IOUR FO		48 (	HOUR FO		72 HOUR	FORECAST
				ERRORS			ERRORS '			ERRORS		ERRORS
HD/DA/HR POS	IT UIND	POSIT	MIND D	GHIW TE	POSIT	WIND	DST WIND	POSIT	WIND	DST WIND	POSIT WIN	D DST WIND
1815862 18.3	137.8 28	18.8 137.6	25. 1	8. 5.	19.8 134.8	30.	133. 15.	8.8 8.8	8 0.	-0. 0.	8.0 0.0 6	8. 8.
1815122 18.9	136.9 20	18.9 136.6	25.	8. 5.	0.0 0.0	0.	-0. 0.	8.8 8.6	8.	-0. 0.	0.0 0.0 0	0. 0.
1015102 19.0	136.1 26	18.9 135.2	28. 7	4. B.	0.0 0.8	8.	-8. 0.	0.8 0.0	8 6.	-0. 6.	6.6 6.6 6	0. 0.
1016862 28.5	135.4 15	19.5 135.2	28. 6	1. 5,	6.0 8.0	0.	-0. 8.	0.8 8.0	8 8.	-0. 0.	8.8 8.8	0. 0.
1016062 21.0	135.0 15	21.2 134.5	15. 1	3. 0.	0.0 0.0	8.	-0. O.	0.0 0.0	9 0.	-0. O.	0.0 6.0 6	8. 8.

	PLL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	LIRNG	24-HR	48-HR	72-HR	LIRHG	24~HR	40-HR	72-HR		
AVG FORECAST POSIT ERROR	35.	133.	8.	8.	0.	Θ.	0.	9.		
AVG RIGHT ANGLE ERROR	33.	119.	8.	8.	8.	0.	е.	8.		
AVE INTENSITY MACHITUDE ERROR	3.	15.	€.	6.	a.	ø.	8.	9.		
AVG INTENSITY BIAS	3.	15.	0.	0.	e.	0.	0.	٥.		
HUMBER OF FORECASTS	5	1			8	6	9	0		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 228. NH

AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

TROPICAL DEPRESSION TD25
FIX POSITIONS FOR CYCLONE NO. 25

### SATELLITE FIXES

FIX HO.	TIPE (Z)	FIX POSITION	ACCRY	DVORRK CODE	COPPENTS	SITE
1	140000	17.1N 143.7E	PCN 6	T1.5/1.5	INIT OBS	PGTW
2	148388	17.5N 142.9E	PCN 6			PGTU
3	148688	17.9H 142.6E	PCN 6		ULAC FIX	PGTW
4	148988	18.1N 141.3E	PCN 6		ULAC FIX	PGT⊌
5	141200	17.6N 148.4E	PCN 6		ULCC FIX	PGTW
6	141600	18.2N 139.4E	PCH 6			PGT₩
7	141800	17.7N 139.8E	PCH 6		ULAC FIX	PGTW
8	142100	18.1N 138.1E	PCN 6		ULAC FIX	PGTU
9	158888	17.8H 138.8E	PCN 6	T2.8/2.8 /D0.5/24HRS		PGTU
18	158388	17.9H 138.2E	PCN 6			PGTW
11	150544	18.7N 137.9E	PCN 6			PGTU
12	150600	18.7N 137.9E	PCH 4			PGTU
13	150900	18.9N 137.4E	PCN 6			PGTU
14	168888	20.6N 135.3E	PCN 4	T1.8/1.5 /W1.8/24/RS		PGTU
15	168532	28.9N 135.6E	PCN 3			PGTW

### AIRCRAFT FIXES

FIX NO.	TIME (Z)	F1X POSITION				MAX-FLT-LVL-WHD ACCRY DIR/VEL/BRG/RNG NAV/TET	EYE SHAPE		MSN NO.
1	142336	17.8N 138.9E	1500FT	1006	20 030 60	219 26 149 58 5 2		+24 +25 +25 38	1

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

	BEST 1	TRACK	:		UARN:		ORS		24 H	OUR FO	DRECAS ERRO			48 HO	UR F	ORCCA! ERRGI			72 HC		DRECAS ERRORS	
MB/DA/HR	POSIT L	THD	P09	TIE	WIND	DST	MIND	PO	TI	MIND	DST	MIND	POS	IT.	UIND	DST	MIND	POS	IT	MIND	DST	UIND
1814002	10.9 161.8	20	8.0	0.0	8.	-0.	Ð.	0.0	6.0	Ø.	-0.	0.	0.0	0.0	e.	··0.	0.	8.8	0.0	0.	-8.	₽.
101406Z	11.0 160.8	20	0.0	0.0	e.	-0.	e.	8.0	0.0	٨.	-8.	0.	0.0	8.8	8.	-8.	8.	8.6	0.6	0.	-0.	8.
1014122	11.8 159.7	20	0.0	0.8	0.	-0.	e.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	ø.	6.6	0.0	0.	-0.	0.
1014182	11.7 150.2	25	0.0	0.0	ã.	-0.	ø.	0.0	8.0	0.	-0.	ø.	8.8	9.0	0.	-8.	e.	0.0	0.0	8.	-0.	0.
101500Z	11.7 156.7	25	8.0	8.6	e.	-0.	ø.	0.0	8.0	ø.	-0.	ä.	8.0	8.8	0.	-0.	ø.	8.8	0.0	8.	<b>-0</b> .	8.
101506Z	12.0 155.3	25	0.0	8.0	a.	-8.	8.	0.8	8.0	ø.	-0.	ē.	0.0	8.0	ø.	-8.	ē.	8.0	0.0	0.	-0.	e.
1815122	12.8 154.1	38	0.0	0.0	ē.	-0.	ø.	8.8	0.0	ø.	-0.	ñ.	0.0	8.8	ø.	-8.	e.	0.0	0.0	ø.	-0.	0.
1015182	13.7 153.1	30	11.8	152.9	30.	115.	ē.		147.4	45.	192.	5.		142.7	68.	258.	5.		137.9	78.	373.	ø.
1016002	14.6 152.1	35	13.8	151.6	35.	56.	ø.		145.5	55.	159.	18.		141.2	75.	235.	15.		136.8	95.	386.	20.
101606Z	15.0 150.9	35		150.2	48.	42.	5.		144.2	60.	180.	15.		139.8	88.	283.	26.		135.2	188.	462.	28.
1016122	15.0 149.6	48		149.5	45.	13.	5.		144.6	60.	128.	10.		139.7	75.		10.		136.2	95.	402.	10.
181618Z	15.7 148.8	49		148.4	45.	26.	5.		144.0	65.	121.	10.		140.1	80.	217.	10.			188.	369.	10.
1017002	16.2 147.9	45		147.8	45.	19.	ä.		144.2	65.	87.	5.		140.9		164.	10.		138.7		290.	5.
1017062	16.4 147.2	45		146.8	55.	26.	10.		143.1	78.	93.	10.		148.2	98.	186.	10.		137.8			5.
101712Z	16.7 146.5	50		146.5	55.	6.	5.		143.4	65.	46.	0.		148.6	90.	282.	5.		138.3			18.
1017182	16.9 146.0	55		146.3	68.	17.	5.		144.5	75.	42.	5.		142.8			16.		148.9			15.
1018002	17.1 145.3	68		145.7	68.	24.	ē.		143.5	75.	48.	ē.		141.7		233.	8.		142.2			15.
101806Z	17.2 144.7	68		144.4	60.	18.	8.		148.9	BØ.	178.	0.		138.3			0.		136.3			20.
1018122	17.6 144.2	65		144.1	60.	19.	-5.		141.0	80.	232.	-5.			100.		-5.		136.2			30.
1018122	18.2 143.8	78		144.1	65.	49.	-5. -5.	••••	141.0	85.	270.	-5.		137.8			-5.		136.2			40.
1019102	19.0 143.6	75		143.6	75.		-3. 0.		142.5		119.	-10.		142.6	98.	403.	-10.		146.3		488.	20.
101906Z	19.9 143.4	80		143.7	PØ.	13.	Ø.		142.4			-10.		143.2	85.	467.	-5.		147.6		478.	20.
		85				16.	0. 0.			100.		-10.		145.B	80.	350.	-3. 8.		149.8		437.	5.
1019122	21.0 143.3			143.2	85.	6.						-3. -10.		148.4	75.	288.	5.		151.8	68.	482.	5. 5.
101918Z	22.0 143.4	90		143.4	85.	12.	-5.		144.4													
102000Z	23.3 143.9	95			100.	10.	5.			100.	163.	0.		149.7	80.	353.	15.		154.5	65.	797.	10.
1020062		100		144.6	95.	12.	-5.		147.1	60.	200.	-10.		152.1	60.	682.	8.	8.6	0.0	8.	-0.	0.
1020122	25.8 145.9			146.0	95.		-10.		150.4	75.	106.	-5.	0.0	0.0	0.	-0.	8.	8.0	0.0	ø.	-0.	0.
102019Z	27.3 147.1			147.5	90.		-15.		152.7	70.	102.	θ.	0.0	0.0	θ.	-6.	0.	0.0	0.0	0.	-0.	0.
102100Z	28.8 148.9				105.	5.	5.		155.2	60.	186.	-5.	9.0	0.0	ø.	-0.	ø.	0.0	0.0	9.	-0.	Θ.
102106Z	29.9 150.9	98		151.2	90.	17.	0.	0.0	0.0	0.	-0.	0.	0.0	6.0	0.	-0.	0.	0.0	0.0	0.	<b>-0</b> .	θ.
1 <b>0</b> 2112Z	30.7 152.4	80		152.7	85.	17.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	8.
1 <b>0</b> 2119Z	31.0 154.0	70		154.0	70.	12.	0.	0.6	0.0	0.	-0.	0.	0.0	9.0	0.	-0.	ø.	0.0	0.6	٨.	- <b>e</b> .	0.
1 <b>0</b> 2200Z	30.7 155.3	65		155.5	50.		-15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-Ø.	0.
102206Z	29.8 156.7	60	0.0	0.0	ø.	-0.	0.	0.0	8.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.
1022122	29.8 157.7	60	0.0	0.0	0	~0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	8.0	0.0	0.	-8.	0.
1 <b>0</b> 2210Z	27.8 158.3	55	0.0	0.0	ø.	-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	0.
1 <b>02300</b> Z	26.9 159.2	55	0.0	0.0	0.	-0.	Ø.	8.8	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	<b>-0</b> .	0.
102306Z	26.2 160.2	55	0.0	0.0	0.	-0.	ð.	0.0	0.0	0.	-0.	0.	0.0	0.6	0.	-8.	0.	8.8	0.0	θ.	-0.	0.
1023122	25.9 161.4	55	0.0	0.0	0.	-0.	0.	0.0	0.0	Ð.	-0.	0.	9.0	0.0	0.	-0.	0.	0.0	0.8	0.	-8.	8.
102318Z	25.7 162.5	50	8.8	8.6	0.	-0.	Ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.8	e.	-0.	e.
1 <b>02400</b> Z	25.5 163.6	50	6.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	6.	-0.	0.	9.9	0.0	0.	<b>-e</b> .	e.
182 <b>40</b> 6Z	25.4 164.4	50		164.7	50.	20.	ø.	25.8	169.2	60.	100.	10.		173.6	50.	418.	10.	6.6	8.0	8.	-0.	0.
1024122	25.4 165.3	50		165.8	50.	28.	0.		178.2	50.	145.	8.	9.6	8.6	9.	-0.	0.	8.8	0.0	٥.	-8.	ø.
1 <b>0</b> 2418Z	25.5 166.2	58	25.5	166.1	50.	5.	8.	26.2	169.1	58.	126.	5.		172.2	45.		18.	8.8	8.8	8.	-8.	8.
102500Z	25.7 166.9	50	25.5	167.1	50.	16.	9.	26.1	170.3	45.	227.	0.		174.5	45.	515.	15.	0.0	0.0	Ð.	~0.	0.
1 <b>02506</b> Z	26.2 167.4	50	26. l	167.8	45.	22.	-5.	27.3	178.6	40.	255.	0.		174.2	35.	50S.	5.	0.0	0.0	0.	-0.	Θ.
1025122	26.8 167.5	50	26.6	160.5	45.	55.	-5.	28.5	171.E	40.	322.	5.		175.9	35.		10.	0.0	0.8	8.	-8.	0.
1 <b>6</b> 2518Z	27.3 167.1	45	27.5	167.5	45.	24.	8.	29.8	167.8	45.	135.	10.	0.0	0.0	0.	-0.	0.	8.6	0.0	0.	-0.	0.
1026002	27.8 166.5	45	28.0	167.3	45.	44.	ø.	30.2	167.8	40.	147.	10.	0.0	0.0	0.	-0.	Ø.	8.0	8.0	€.	-8.	0.
102606Z	29.2 166.1	40	28.3	166.4	45.	17.	5.	30.6	165.2	35.	15.	5.	0.0	0.0	0.	-0.	0.	8.8	0.0	8.	-0.	0.
1826122	28.7 165.7	35		166.2	45.	27.	10.		165.2	Ø.	29.	-25.	0.0	0.0	0.	-0.	ø.	0.0	0.0	8.	-0.	0.
182618Z	29.2 165.3	35		165.2	40.	8.	5.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-Ð.	ø.	0.0	0.0	0.	-0.	0.
1027002	29.8 165.0	30		164.8	35.	21.	5.	0.0	0.0	ē.	-0.	ø.	0.0	0.0	e.	-0.	ø.	0.0	0.0	ø.	-0.	e.
1027062	30.6 164.9	30		164.2	35.	43.	5.	0.0	0.0	ø.	-0.	e.	0.0	8.8	9.	-0.	ø.	0.0	8.0	8.	-0.	0.
1027122	31.4 165.5	25		165.3	35.	18.	10.	0.0	0.0	ø.	-0.	e.	8.0	0.0	ø.	-0.	ē.	0.0	0.0	0.	-0.	e.
1027192	32.3 166.7	25	0.0	0.0	ð.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	Θ.	-0.	8.
102800Z	33.3 167.3	20	0.0	0.0	ø.	-0.	8.	0.0	0.0	ě.	-8.	ø.	0.0	0.0	ø.	-8.	ē.	8.8	8.8	e.	-e.	e.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	WRNG	24-HR	48-HR	72-HR	LIRNG	48-HR	72-HR			
AVG FORECAST POSIT ERROR	24.	146.	362.	558.	21.	154.	339.	550.		
AVG RIGHT ANGLE ERROR	19.	103.	236.	285.	16.	106.	212.	285.		
AVG INTENSITY MAGNITUDE ERROR	4.	6.	8.	14.	4.	6.	8.	14.		
AVG INTENSITY BIAS	1.	î.	6.	14.	0.	1.	5.	14.		
NUMBER OF FORECASTS	46	32	24	18	36	29	21	18		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 3684. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

## TYPHOON OLEN FIX POSITIONS FOR CYCLONE NO. 26

### SATELLITE FIXES

	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CUITENTS	SITE
	140000	9.4N 161.5E		T1.0/1.0	INIT OBS	PGTW
2	148414	10.3N 160.9E 10.6N 160.9E	PCN 6			PGTU PGTU
4	140908	10.8N 168.2E	PCN 6		ULAC FIX	PGIW
5	141200	11.5N 160.0E	PCN 6			PGTW
7	141659	12.2N 159.3E	PCN 5			PGTU PGTU
8	141888	11.6N 158.4E	PCN 6			PGTU
18	142166	11.7N 157.4E	PCN 6	T2.0/2.0 /D1.0/24HRS	ULAC FIX	PGTU PGTU
ii	158482	11.8N 155.5E	PCN 5	1810/210 / 9110/2418.0	ULAC FIX	PGTW
12	158688	12.2N 155.3E	PCN 6		ULAC FIX ULAC FIX	PG TW BG TW
* 14	151200	12.3N 154.9E	PCN 6		OLNE FIX	PGTW
		11.6N 153.4E 11.5N 152.7E				PGTW PGTW
		13.3N 151.7E			BASED ON EXTRAP	PGTIJ
* 19	160000	14.7N 151.0E	PCN 6	T2.5/2.5 /D0.5/24HRS		PGTU
19 28	168688	14.6N 150.6E	PCN 6			PGTW PGTW
21	160900	14.6H 149.7E	PCN 6			PGTU
22	161200	14.6N 149.5E	PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
24	161999	15.2N 148.5E	PCN 6		ULCC FIX	PGTU
25 36	162100	16.0N 148.8E	PCN 6	T7 8 /7 8 /08 5 /2 4UDC		PGTW PGTW
27	170300	16.1N 147.5E	PCN 4	13.0/3.0 /20.3/24083		PGTU
28	170520	16.4N 147.3E	PCN 3			PGTU
38	171200	16.4N 146.8E	PCN 6	13.0/3.0 /D0.5/24HRS		PG TW PG TW
31	171688	16.9N 146.4E	PCN 6		04555 BU EVENAG	PuTM
32 33	172100	17.5N 146.8E 17.5N 145.8E	PCN 6		BASED ON EXTRAP BASED ON EXTRAP	PGTW PGTW
34	180000	17.4H 145.6E	PCH 6	T4.0/4.0 /D1.0/24HRS	BASED ON EXTRAP	PGTU
35 36	180300	17.1N 144.6E 17.2N 144.6E	PCN 4	T4.0/4.0 /D1.0/24HRS	ULCC FIX	PG TW PG TW
37	100900	17.0N 144.5E	PCN 6			PGTW
		17.1N 144.1E 17.6N 144.8E			ULAC FIX ULAC FIX	PGTW PGTW
40	181800	18.3N 144.0E	PCN 6			PGTW
		18.4N 143.9E 18.7N 143.6E			ULAC FIX ULCC FIX	PGTW PGTW
43	190300	19.2N 143.4E	PCN 4	T4.5/4.5 /D8.5/24HRS	EYE OPEN SW-NW	PGTW
44	198688	19.9N 143.4E	PCN 2		EYE OPEN SSE	PG TW PGTW
46	191200	21.1N 143.3E	PCN 4		ULAC FIX	PGTW
47	191600	21.8N 143.6E	PCH 4			PGTW PGTW
49	191800	22.2N 143.3E	PCN 2			PGTW
58	192100	22.5N 143.4E	PCN 2			PGTW PGTW
52	200300	24.0N 144.3E	PCN 2	T5.5/5.5-/D1.8/24#RS		PGTW
53	200443	24.2N 144.5E 24.7N 144.8E	PCN 1			PGTW PGTW
		25.3N 145.4E				PGTW
56	201200	26.2N 146.1E	PCN 2			PGTU PCTU
		27.0N 147.0E 27.4N 147.2E				PGTW PGTW
			2001			PGTU PCTU
61	210000	29.5N 149.9E	PCN 2	T4.5/5.8 /WI.8/24#RS		PGTU PGTU
62	210431	29.5N 150.8E	PCH 4			PGTU
63 64	210600	29.9N 151.0E 30.1N 152.1E	PCN 4		HLCC FIX	PGTU PGTU
65	211200	30.6H 152.8E	PCN 6			PGTW
66 67	211688	30.9N 153.5E	PCN 6			PGT⊎ PGT⊎
90	£11000	30.30 134.16	ren p			PGTW
69 70	212100 220000	30.8N 154.7E 30.7N 155.1E	PCN 6	T3.0/3.0 /W1.5/21HPS	ULAC FIX	PGTU PGTU
71	220300	30.7H 155.5E	PCN 6		ULAC FIX'	PGTW
72 73	228419 228688	38.2N 156.1E 29.6N 156.7E	PCN 6 PCN 6		ULAC FIX ULAC FIX	PGTU PGTU
74	220900	29.2N 157.2E	PCH 6		ULAC FIX	PGTW
75 76	221200 221600	20.7N 157.9E 27.7N 150.2E	PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
77	221999	27.5N 158.5E	PCN 6		ULCC FIX	PGTW
78 79	222166 235666	27.2N 158.7E 26.9N 159.2E	PCN 6 PCN 4	T2.8/2.8 /W1.8/24HRS	ULCC FIX	PGTU PGTU
88	230300	26.7N 159.2E	PCN 4	12.0/2.0 /WI.0/24MKS	EXP LLCC	PGTW
81	238487	26.2N 160.1E	PCH 4		EXP LLCC	PGTW PGTW
82 83	230600 230900	26.2N 168.4E 25.7N 168.6E	PCN 6 PCN 6			PGTU
84	231298	25.7N 162.5E	PCH 6			PGTW

85	231688	25.BN 163.8E	PCN 6			PGTW
86	232188	25.3N 163.3E	PCN 6			PGTW
87	240000	25.7N 163.6E	PCN 6	T3.8/3.8-/D1.8/24HRS		PGTW
88	240335	25.6N 164.3E	PCN 5	(3.0/3.0/21.0/24163		PGTU
89	248688	25.7N 164.8E	PCN 4			PGTW
98	240900	25.7N 165.2E	PCN 6			PGTW
91	241200	25.6N 165.5E	PCN 6			PGTU
92	241688	25.7N 165.6E	PCN 6		ULCC FIX	PGTW
93	241639	25.4H 165.8E	PCN 6		OLCC FIN	KGUC
94	241649	25.6N 166.8E	PCN 6		ULCC FIX	PGTIJ
95	241800	25.6N 166.4E	PCN 6		OLUT FIN	PGTW
96	242100	25.6N 166.8E	PCN 6			PGTU
97	250000	25.BN 166.9E	PCN 6	T3.0/3.0-/S0.0/24HRS		PGTU
98	250386	26.1N 167.2E	PCH 6	15.0/5.0 / 50.0/2-4/85		PGTU
99	250342	26.2N 167.4E	PCN 6	T2.0/3.0-/U1.0/24HRS		KGUC
100	250343	26.1N 167.4E	PCN 5	1210-010 - 0110-2-110		PGTU
101	250680	26.3N 167.8E	PCN 6			PGTW
182	250900	26.4N 168.8F	PCN 6			PGTU
103	251200	26.5N 160.1E	PCN 6			PGTU
184	251600	26.9N 167.4E	PCN 4			PGTU
105	251627	27.1N 167.4E	PCH 4		ULCC FIX	PGTW
186	251627	27.8N 166.9E	PCN 6			KGWC
187	251800	27.5N 167.5E	PCN 6		ULCC FIX	PGTU
108	252180	27.7N 167.2E	PCN 6		ULCC FIX	PGTW
189	260000	27.9N 167.8E	PCN 6			PGTU
110	260300	27.7N 166.2E	PCN 6	T2.0/3.0-/W1.0/27HRS		PGTW
111	260330	27.7N 166.2E	PCN 6	T3.8/3.8 /D1.8/24HRS		KGWC
112	268688	28.3N 165.8E	PCN 6			PGTW
113	260900	28.5N 165.8E	PCN 6			PGTU
114	261200	29.1N 165.6E	PCN 6		ULAC FIX	PGTW
115	261688	29.2N 165.3E	PCN 6		ULAC FIX	PGTW
116	261800	29.4N 165.4E	PCN 6		ULAC FIX	PG IW
117	262100	29.7N 164.9E	PCN 6			PGTW
118	278888	29.5N 164.4E	PCN 4		EXP LLCC	PGTW
119	270300	29.9N 164.5E	PCN 4	T2.8/2.5-/\$8.8/24HRS		PGTW
120	278318	30.1N 165.8E	PCN 4	T2.0/2.0 /U1.0/24HRS	EXP LLCC ULAC 31.6N 165.6E	KGWC
121	278688	30.5N 164.9E	PCN 4		EXP LLCC	PGT⊎
122	278988	31.0N 165.0E	PCN 6			PGTU
123	271200	31.4N 165.5E	PCN 6		ULAC 32.7N 165.6E	PGTM
124	271688	32.1N 166.5E	PCN 6			PGTW
125	271603	31.8N 166.8E	PCN 4		EXP LLCC ULAC 33.3N 167.2E	KGUC
126	271866	32.4N 167.0E	PCN 6			PGT⊌
127	272180	33.0N 167.4E	PCN 6			PGTW
129	299999	33.6N 168.7E	PCN 4	T1.8/1.5 /U1.8/21HRS		PGTU

### AIRCRAFT FIXES

FIX NO.	TIME (Z)	F1X POSITION	FLT LVL	700MB HGT	085 HSLP		-SFC /BRG					-UND /RNG		CRY MET	EYE SHAPE		DRIEN- TATION	EYE TE			MSN NO.
1	142312	11.2N 158.8E	1500FT		1895	15	360	60	628	21	200	50	5	28				+24 +18	+18	27	1
2	152317	14.3N 152.5E	1500FT			30	198	35	246		168	58	5	5				+25 +25			Ž
3	160636	15.1N 150.8E	788MB	3036	995	45	120	15	646	35	278	68	5	4							3
4	160927	15.0N !50.1E	700HB	3041	999				170	45	878	70	5	4				+12 +11	+11		3
5	161422	15.6N 148.9E	700MB	3030	995				340	41	240	70	10	19				+10 +13	+11		4
6	161661	15.8N 148.8E	700MB	3023					149	37	858	90	9	18							4
7	162013	16.1N 148.4E	700MB	3022	992	30	260	68	360	43	260	120	8	8				+12 +13	+12		4
8	179228	16.2N 147.4E	1500FT		992		666	90	198		689	24	¥	5				+25	+24	38	5
9	170606	16.6N 147.3E	700MB	2987		75	130	60	190	46	150	30	8	10							5
10	170033	16.4H 146.8E	79 <b>9</b> H9	2986	988				228	54	130	119	5	4				+18 +16	+11		6
11	171122	16.4N 146.9E	7 <b>88</b> 118	2985					140		940	98	5	4							6
12	172054	17.1N 145.8E	700MB	2933	983	68	<del>990</del>	30	190	52	686	120	2	5				+13 +14	+13		7
13	172325	17.1N 145.3E	700MB	2945		68	828	90	270	61	199	140	3	4							7
14	100845	17.2N 144.4E	7 <b>001B</b>	2925	988				110	56	040	48	5	3				+13 +15	+14		9
15	181123	17.3N 144.3E	700MB	2914					298	60	110	60	10	8							9
16	182054	18.4H 143.BE	7 <b>9019</b>	2823	969		828	30	146	73	828	30	5	2				+13 +16	+ 9		10
17	182336	18.8N 143.6E	7 <del>00</del> 118	2800			220	60	300		220	60	5	2							10
18	190612	20.0N 143.5E	70 <del>011</del> 9	2776		65	140	120	218	75	140	78	6	3							11
19	190848	20.4N 143.2E	7 <b>9911</b> 9	2736	958				310		230	60	6	3	C IRCULAR	20		+14 +15			11
20	192056	22.5N 143.5E	700MB	2613			870		258		178	30	18	4	C IRCULAR	48		+11 +17	+10		13
21	192343	23.2N 143.8E	788MB	2616			270	28	320	70	230	30	10	4							13
22	200605	24.8N 144.BE	700MB	2616		78	320	10	230		140	40	5	5							14
23	200844	25.2N 145.3E	7 <b>0011</b>	2689	944				300		159	30	5	5	ELLIPTICAL		040	+15 +18			14
24	202040	28.8N 147.7E	799119	2555	939		868	5	240		150	30	5	2	ELL IPTICAL		858	+14 +28	+13		15
25	202254	28.5N 148.6E	700M	2573			170	30	210		170	25	5	3	CIRCULAR	60					15
26	210784	30.1N 150.9E	786MB	2655	950	55	110	135	200		120		10	5				+11 +19	+11		16
27	210948	30.5N 151.8E	7 <b>0019</b>	2679					290	74	210	113	4	5							16

NOTICE - THE ASTERISKS (#) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

	BEST TRACK	WARN ING ERRORS	24 HOUR FORECAST ERHURS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MD/DA/HR	POSIT WIND	POSIT WIND DST WIN		POSIT WIND DST WIND	POSIT WIND DST WIND
1121182	7.6 176.7 15		n. 8.0 86 88. 9.	0.6 0.0 00. 0.	6.8 8.8 80. 6.
112206Z	7.6 177.2 26		3. 9.6 9.6 96. 9. 3. 8.8 8.8 88. 8.	5.6 5.6 50. 8. 8.6 5.6 60. 6.	8.8 8.8 88. 8. 8.8 8.8 88. 8.
1122 <b>06</b> Z 112212Z	7.8 177.9 28 7.5 178.1 29	0.0 0.0 0. 0	9. 8.8 8.8 66. 6. 9. 9.8 6.8 68. 6.	8.8 8.8 8B. 8.	8.0 B.0 C0. C.
1122182	8.0 177.9 20	0.0 0.0 0. 0	3. 0.0 0.0 00. 0.	0.0 0.0 00. 0.	6.6 8.6 66. 6.
1123002	8.0 177.4 25		3. 0.0 0.0 00. U.	0.0 6.0 00. 6.	6.0 0.0 0. <b>-0. 0</b> .
112306Z	7.8 176.7 25		. O.O O.O OO. O.	0.8 0.0 00. 6.	6.0 0.0 08. 6.
112312Z 112318Z	7.6 176.3 25 7.3 175.8 25	2.2 2.0 2. 2. 2	0. 0.0 0.0 06. 0. 0. 0.0 0.0 08. 0.	0.8	0.0 0.0 00. 0. 8.0 0.0 00. 0.
1124002	7.1 175.2 30	8.0 0.0 00. 0		8.8 8.8 88. 6.	0.0 C.O S0. O.
1124062	6.9 174.8 38		6.2 172.6 35. 10615.	6.4 169.9 45. 17720.	6.9 167.2 55. 33440.
1124122	6.8 174.2 35	6.8 174.2 30. 05		8.0 169.1 50. 19120.	9.3 167.1 69. 31835.
1124182	6.9 173.3 45	6.8 173.5 48. 13. ··5		8.8 169.8 60. 22415. 11.2 164.9 70. 8815.	10.2 166.7 70. 34638. 12.8 162.1 70. 12125.
1125 <b>00</b> Z 1125 <b>0</b> 6Z	7.2 172.3 58 7.4 171.3 58		5. 9.2 168.3 60. 76. 0. 3. 9.6 167.5 78. 68. 5.	11.2 164.9 70. 8815. 11.6 164.8 88. 9215.	13.2 161.3 70. 9825.
1125122	7.5 170.4 55		8. 8.7 166.5 70. 32. 8.	10.0 163.2 80. 9315.	11.5 160.4 75. 11920.
1125182	7.6 169.7 55	7.4 169.7 60. 12. 5	5. 8.2 165.9 75. 96. 8.	9.5 162.4 88. 15128.	18.9 159.7 75. 15925.
112600Z	9.0 168.7 60		3. 8.7 165.8 75. 11910.	10.0 163.5 80. 22815.	10.7 158.7 89. 181. 10.
112606Z 112612Z	8.5 167.8 65 9.2 166.3 70	8.4 167.7 65. 8. 0 8.9 166.7 65. 305	3. 9.9 164.6 80. 10715. 5. 10.7 162.9 80. 5615.	10.5 161.8 80. 18115. 11.3 158.8 80. 11115.	10.8 156.9 99. 198. 35. 11.7 154.3 98. 234. 48.
1126122	9.6 165.1 75	9.8 165.2 78. 135		11.5 155.6 85. 21915.	11.6 151.9 94. 322. 35.
1127002	9.9 164.2 85	10.3 163.0 75. 3410		12.5 156.1 95. 152. 15.	12.7 153.4 95. 160. 25.
1127 <b>06</b> Z	10.5 162.9 95	10.5 162.9 100. 0. 5	5. 11.9 158.6 130. 80. 35.	12.7 155.4 125. 174. 78.	12.9 151.8 128. 184. 68.
1127122	11.0 162.0 95	11.0 161.7 110. 10. 15		12.8 154.4 125. 200. 75.	13.2 150.8 126. 179. 65.
	11.6 161.0 100 12.0 160.2 95	11.7 160.8 110. 13. 10 11.9 160.2 90. 65		13.0 153.2 125. 234. 70. 13.5 152.7 100. 211. 40.	13.2 149.6 129. 173. 78. 13.5 148.9 98. 128. 48.
1128062	12.7 159.7 95		5. 13.5 155.5 105. 158. 50.	13.8 151.1 110. 242. 50.	13.8 146.8 115. 123. 78.
	13.1 159.2 95		5. 14.8 155.5 185. 144. 55.	14.5 151.4 110. 212. 55.	14.2 146.8 115. 158. 78.
1128182	13.4 158.8 100		3. 13.7 154.8 105. 146. 50.	14.1 150.5 110. 182. 60.	14.1 146.0 115. 195. 75.
	13.7 158.4 70	13.8 150.5 100. 18. 30		15 2 151.2 105. 229. 55.	14.7 147.1 118. 378. 75.
1129067 1129122	13.7 158.2 55 13.4 157.9 58	14.2 158.2 100. 30. 45 13.6 157.8 60. 13. 10		15.2 151.0 100. 268. 55. 13.2 151.4 80. 364. 35.	14.6 147.0 105. 474. 75. 13.3 144.9 100. 448. 70.
	13.0 157.2 55		). 12.8 155.5 65. 227. 15.	12.6 150.1 80. 399. 40.	13.6 143.6 100. 451. 65.
	12.3 156.1 60	12.6 156.2 65. 19. 5		13.2 145.8 86. 277. 51.	15.0 141.4 90. 396. 45.
113006Z	12.0 154.8 60		5. 12.1 150.4 60. 153. 35.	13.2 145.2 85. 352. 55.	14.9 140.9 90. 454. 40.
	11.5 153.3 55	11.8 153.6 65. 25. 10		13.5 144.4 88. 428. 58. 14.6 142.8 85. 413. 58.	16.1 140.2 96. 467. 40.
	11.4 151.9 50 11.6 149.9 50	11.4 151.9 65. 0. 15 11.5 150.4 50. 30. 0		14.6 142.8 85. 413. 50. 14.8 140.3 50. 331. 5.	17.1 138.3 90. 401. 35. 16.0 135.4 60. 244. 5.
	12.0 147.8 45	12.2 147.7 50. 13. 5		15.8 135.7 40. 15710.	15.0 131.3 45. 5815.
1201122	12.0 145.3 45		13.2 139.2 40. 121. 10.	13.7 134.3 45. 1455.	15.5 130.9 45. 5220.
1201102	12.2 143.3 48	12.4 143.4 35. 135		17.4 134.7 30. 21825.	0.0 0.0 0. <del>-0</del> . 0.
120200Z 120206Z	12.1 141.2 35 12.1 139.3 30		3. 13.9 133.9 30. 47, -15. 5. 14.3 132.3 30. 47, -20.	17.4 128.0 38. 17925. 17.2 127.0 25. 22635.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1202122	12.4 137.3 30	12.2 137.3 35. 12. 5		0.0 0.0 00. 0.	0.0 0.0 00. 0.
128218Z	13.0 135.9 35		. 14.1 129.6 30. 13725.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
120300Z	13.8 134.7 45	13.4 134.2 40. 305		17.1 124.5 30. 29250.	10.3 120.3 25. 53430.
120306Z 120312Z	14.3 133.1 50 15.8 132.2 50		3. 16.3 129.7 65. 115. 5. 5. 17.1 127.9 65. 146. 0.	17.8 124.9 55. 27320. 18.5 124.8 58. 38915.	18.8 120.9 50. 476. 0. 19.0 119.8 45. 5885.
1203122	15.0 132.2 50 15.3 131.6 55		5. 17.1 127.9 65. 146. 0. 9. 16.8 127.3 65. 1485.	17.8 123.7 55. 3555.	18.7 120.0 40. 46820.
1284882	15.5 131.2 55		5. 17.2 129.8 55. 6225.	21.1 130.3 40. 31115.	9.0 9.0 90. 0.
	15.7 130.6 60	15.8 138.9 68. 13. 0	3. 18.9 129.0 45. 158, -30.	23.9 131.2 35. 54715.	0.0 0.0 00. 0.
1 <b>20</b> 412Z 1 <b>20</b> 418Z	15.9 130.1 65 15.9 129.7 70		9. 19.3 120.8 50. 15115.	25.8 131.1 30. 71120. 24.8 130.8 35. 67725.	9.8
1204182 12 <b>6588</b> 2	15.9 129.7 78 16.2 129.5 98	16.2 129.7 65. 18. ~5 16.2 129.3 85. 12. 5	5. 19.0 127.8 55. 175, -5. 5. 18.7 127.8 75. 183. 20.	24.8 130.0 35. 6((, -25. 8.8 8.8 88. 8.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1285862	16.3 129.4 75	16.3 129.4 85. 6. 10		0.0 0.0 00. 0.	0.0 0.0 00. 0.
1205122	16.8 129.1 65	16.5 129.0 60. 195	5. 17.8 127.9 48. 201, -10.	0.0 0.6 00. 6.	0.0 0.0 00. 8.
120518Z 1 <b>20608</b> Z	16.8 129.8 68	16.8 128.7 55. 635		0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1206002 1206062	16.0 129.3 55 15.2 120.3 50	17.8 128.4 55. 79. 8 15.2 128.3 58. 8. 8	9. 18.1 126.7 40. 30530. 9. 14.2 123.0 60. 935.	0.0 0.0 00. 0. 14.5 118.0 55. 273. 20.	0.8 0.0 90. 0. 9.8 0.8 00. 0.
1206122	14.5 127.3 50		9. 13.8 123.2 50. 124. 0.	13.9 110.3 50. 250. 20.	0.0 0.8 00. 0.
1206182	14.8 126.5 68	14.2 126.3 58. 17. 18	D. 13.8 121.3 45. 169. 5.	14.3 116.8 55. 258. 25.	0.0 0.0 00. 0.
1297882	13.2 125.3 70		. 13.4 126.5 68. 191. 25.	14.5 115.8 65. 268. 40.	0.0 0.0 00. 0.
120706Z 120712Z	12.7 124.2 65 11.0 122.7 50		3. 13.5 119.3 68. 222. 25. 8. 13.3 118.3 65. 216. 35.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	6.0 0.0 60. 0. 6.0 6.0 66. 6.
1207122	11.0 122.7 50	12.0 122.0 50. 60. 10 13.2 121.7 50. 130. 10		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
120000Z	18.4 119.5 35	18.8 119.4 48. 25. 5		P.O 0.0 86. 0.	8.0 8.0 SO. O.
1200062	18.8 118.1 35	9.9 118.1 38. 65		8.8 8.8 B8. B.	0.0 0.0 00. 0.
120012Z 120018Z	9.9 117.1 38	9.6 116.8 38. 25. 8		0.0 0.0 00. 0.	0.0 0.0 00. C. 0.0 0.0 06. 0.
	18.6 116.1 38 16.2 115.2 25		). 8,6 8.8 80, 9. 9, 8,8 6.8 66, 8.	0.8 0.0 0. <del>-</del> 0. 0. 0.0 0.6 00. 0.	0.8 0.8 0. <del>-8</del> . 8. 0.0 0.6 0. <del>-</del> 8. 8.

	ALL	FORECAS	TS		TYPHO	IONS UNII	LE OVER	35 KTS
	LIRNG	24-1歳	46-HR	72-HR	LIRNG	24-4収	48-HR	72-HR
AVG FORECAST POSIT ERROR	20.	139.	263.	200.	21.	136.	258.	269.
AVG RIGHT ANGLE ERROR	14.	79.	149.	140.	15.	74.	145.	141.
AVE INTENSITY MAGNITUDE ERROR	5.	19.	31.	39.	6.	19.	30.	37.
AVG INTENSITY BIAS	3.	6.	11.	22.	3.	5.	θ.	19.
NUMBER OF FORECASTS	68	56	45	34	54	51	40	32

PISTANCE TRAVELED BY TROPICAL CYCLONE IS 4291. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

## TYPHOON PARELA FIX POSITIONS FOR CYCLONE NO. 27

### SATELLI IF FINES

	TIME (Z)	FIX POSITION	ACERY	DVORAK CODE	COMMENTS	SITE
	``_'	700111011	MOUNT.	STORIN COPE		3110
1 2	21 <b>0300</b> 210319	9.6H 176.6E	PCH 6 PCN 6	T1.8/1.8 T1.8/1.0	INIT DBS U.CC FIX INIT DBS ULAC 8.8N 176.1E	PG TW KGUC
3	211604	8.5H 176.FE	PCN 6		ULAC R. SH 175.96	KGUC
	220300 220307	6.9N 178.1E 8.8N 178.1E	PCN 6 PCN 4	T1.8/1.8 /S8.8/24IRS T2.8/2.8 /D1.8/24IRS	ULAC 8.0N 177.5E	PGTU KGUC
6	221200 221551	7.5N 177,9E	PCH 6		ULAC 8.6N 177.2E	PGTU KGWC
8	221600	8.3N 177.6E	PCN 6		ULHC 8.0H ITT.ZE	PGTW
	238868 238254	7.9H 177.6E 8.2H 176.9E	PCN 4 PCN 4	T2.0/2.0 /S0.0/24HRS	EXP LLCC	PGTU KGUC
11	230300 230600	8.1N 177.1E 8.2N 176.7E	PCN 4	T2.0/2.0 /S0.0/24HRS T1.0/1.0-/S0.0/24HRS		PGTU PG (W
13	230033	7.BN 176.3E	PCN 6		ULAC 9.4N 174.BE	KGLIC
	2312 <b>00</b> 231539		PCN 6 PCN 6			PGTW KGWC
16	231688 231931	7.5H 176.2E	PCN 6	T2.5/2.5 /D0.5/16HRS		PG (U
18	232100	7.5N 175.5E	PCN 6	12.3/2.3 /bd.3/10mks		KG <b>U</b> C PGTU
19 20	240000 240242	7.5N 175.3E 7.1N 174.3E	PCN 6	T2.0/2.0~/D1.0/21HRS T3.0/3.0 /D0.5/06HRS	ULAC 7.1N 173.7F	PG TW KGMC
21	240300	6.9N 175.1E	PCN 6		M CC 7 70 174 7F	DC TIJ
23	240689	6.8N 174.7E	PCN 6		ULCC 7.3N 174.3E ULAC 6.4N 174.1E	PGTW KGUC
24 25	240900 241200	6.9N 174.5E 7.8N 174.3E	PCN 6 PCN 6			PGTU PGTU
26	241527	6.6N 172.9E	PCN 6		ULAC 6.6N 173.2E	KGUC
28	241888	6.9N 173.2E	PCN 6		ULCC FIX	PGTW PGTW
29 38	242048 242049	6.8N 171.9E 7.8N 172.5E	PCN 5	T4.8/4.8+/D1.8/19HR\$	ULAC 7.1N 173.7E  ULCC 7.3N 174.3E  ULAC 6.4N 174.1E  ULAC 6.6N 173.2E  ULCC FIX  ULCC FIX	KGMC PGTM
31	250000	7.3N 172.3E	PCN 4	T3.5/3.5 /D1.5/24HRS		PGTU PGTU
33	250412	7.2N 171.5E	PCH 6			KGUC
	250600 250746		PCN 6 PCN 6			PGTU KGMC
	258968 251288	6.8N 170.9E	PCN 6		ULCC FIX	PGTU PGTU
38	251515	7.3N 169.9E	PCN 6		OLCC FIX	KGMC
	251600 251000					PGTU PGTU
41	252024 252100	7 6N 169 TE	PCN 1	T1.5/4.5 /08.5/24HRS	W 66 F 14	KGM
43	260000	8.8N 168.8E	PCN 4	T4.8/4.8 /D0.5/24HRS	ULCC FIX	PG I W PG TW
	260300 260400	8.2N 168.3E 8.3N 168.1E	PCN 4 PCN 3			PGTU PGTU
46	268488 268688	8.2N 167.8E	PCN 1 PCN 4			KGUC PGTU
46	268988	8.6N 167.6E	PCN 4			PGTU
49 50	268906 261200	8.9N 167.BE 9.1N 166.4E	PCN 6 PCN 6			KGMC PGTM
51	261688 261645	9.5N 165.7E	PCH 4			PGTM PGTM
53	261645	9.5N 165.2E	PCN 2			KGMC
	261 <b>999</b> 262 <b>999</b>			T5.5/5.5 /D1.8/24HRS		PGTU KGUC
56 57	2621 <b>88</b>	9.7N 164.7E	PCN 2	T4.5/4.5 /D0.5/24IRS	EVE OPEN SE	PGTW PGTW
58	278348	18.3N 163.3E	PCH 2	with a second second	with or all ord	PGTU
68	278988	10.5N 163.0E 10.7N 162.6E	PCN 2			PGTW PGTW
61 62	271/00	11.0N 162.IE 11.4N 161.4E				PGTW PGTW
63	271986	11.6N 161.2E	PCN 2	TS.5/5.5 /01.0/24HRS		PGTM
64 65	299999	11.7N 161.0E	PCN 3	T5.5/5.5 /01.8/24RS		PGTU PGTU
66 67	200336	12-3N 159.8E	PCN 2		EYE DIA 35NM	PGTW PGTW
00	200200	12.31 133.36	F C 17 -		18 CO E 14	PGTM
69 78	2812 <b>66</b> 2816 <b>66</b>	12.5N 159.0E 12.6N 158.8E	PCN 6		ULCC FIX	PGTW PGTW
71 72	281900 282054	13.1N 150.7E 13.5N 150.7E	PCH 6 PCH 3			PGTU PGTU
73	290000	13.7N 158.4E	PCN 2	T4.5/5.8+/U1.8/24RS		PGT⊌
74 75	290386 290686	13.6N 150.3E 13.7N 150.2E	PCN 4 PCN 6			PGTU PGTU
76 77	290900 291200	13.7N 150.2E 13.7N 157.0E	PCN 6		ULCC FIX	PGTW PGTW
78	291688	13.4H 157.7E	PCN 6		ULAC FIX	PGTW
79 <b>86</b>	291688 291888	13.4H 157.7E 13.3H 157.6E	PCH 5 PCH 6		ULAC FIX ULAC FIX	PGTW PGTW
8 1 82	292100 300000	13.0N 157.2E 12.4N 156.0E	PCN 6 PCN 4	T3.5/4.0+/U1.0/24/RS	END LLCC	PG TU
83	386386	12.4H 155.5E	PCH 6	~ . ~	21- 22-0	PGTM

84	300453	12.3N	155.2E	PCH 5			PG IM
85	300600		155.1E	PCN 6			PGTU
	300909			PCH 6			PGTW
86			154. 1E				
87	381268	11.5N	153.5E	PCN 4		ULAC 12.1N 155.6E	PGTW
68	381686		152.5E	PCN 4		EXP LLCC	PGTW
89		11.7N		PCN 3			PG (W
98		11.7N		PCH 4			PCTU
91	302100	11.8N	151.1E	PCH 4			PGTU
92		11.7N		PCN 5			PGTW
93		11.BN		PCN 6			PGTW
94	010300	12.0N	148.9E	PCN 6			PGIW
95		12.1N		PCH 3	13.8/3.8+/WB.5/28HRS		PGTU
					1010-0101-010-2010-		PGTU
	010600	12. IN	147.4E	PCN 4			
97	010900	12.2N	146. IE	PCN 6			PGTW
98	011200			PCN 4			PGTW
	011600			PCN 6		ULCC FIX	PGTU
	011000		143.2E	PCN 6		INCC FIX	PGTW
101	012100	12.0N	141.7E	PCN 6		ULCC FIX	PGTW
102	012305	12.8N	141 BE	PCN 5			PGTW
	020000	12.011	141 55				PGTM
163	070000	12.01	141.35	PCN 4			
104	<b>020300</b>	12.3N	140.3E	PCN 4	T1.5/2.5 /W1.5/22HRS	EXP LLCC	PGTW
185	020300	12.0N	140. IE	PCN 4	T2.8/2.8+	INIT OBS	RPMK
				PCN 3	12.00	EXP LLCC	PGTM
	020611					tre title	
	02 <del>0900</del>			PCN 6			PGTW
108	821200	12.8N	137.2E	PCH 6		ULCC FIX	PGTW
	021600			PCH 6			PGTW
						HEC CIV	
	0218 <b>00</b>			PCN 6		ULCC FIX	PGTW
111	022100	13.5N	134.8E	PCN 6			PGTW
	022241						PRITU
							PSTU
113	030 <del>000</del>	13.68	134.7E	PCH 6			
114	030300	13.8N	134. IE	PCH 6	T3.0/3.0 /D1.5/24HRS		PGTW
115	030559	14.4N	133.4F	PCN 5		ULAC FIX	PGTW
116	070000	14 71	173 05	PCN 6		ULAC FIX	PGTU
	030900	14,71	132.8E 132.1E 131.6E			OCHC TIV	
117	031200	15.84	132.15	PCN 6			PGTW
118	031600	15.2N	131.6E	PCH 6			PG (NJ
119	031800	15.3N	171 45	PCN 6			PGTU
	031000	13.30	131.46				
120	031943	15.4N	131.3E	PCN 5			PGTW
121	<b>832188</b>	15.4N	131.3E	PCN 6			PGTM
122	032217	15 3N	131.5E	PCN 3			RPMK
				PCN 6		ULAC FIX	PGTW
		15.6N					
124	040300	16.8N	130.7E	PCN 4	T4.8/4.8-/D1.8/24HRS	ULAC FIX	PGTW
125	040546	16.3N	130.BE	PCN 5		ULAC FIX	PCTU
		16.3N		PCN 6		ULAC FIX	PGTU
							1.01.0
127			130.5E			ULAC FIX	PGTW
128	841288	15.BN	130.2E	PCH 4			PGTU
	841688			PCN 2			CGTU
							PGTW
	041931			PCH 1			
131	042100	16.0N	129.6E	PCN 2			PGTW
132	842335		129.9€	PCN 1	T5.0/5.0	INIT ODS	RODH
	050000	16.00	120 55	PCN 2	1010-010		PGTIJ
133		10.21	129.5E				
	<b>0</b> 50300	16.2N	129.4E		T5.8/5.0-/D1.0/24HRS		PGTW
1.35	050534	16. IN	129.4E	PCN 1			PGTW
	050600			PCN 2			PGTW
						IN AC ETY	
	050900			PCN 6		ULAC FIX	PGTW
130	<b>0</b> 512 <b>00</b>	16.7N	129.3E	PCN 6			PGTW
	851688			PCN 6		ULCC FIX	PGTW
		17.1N		PCN 6		ULCC FIX	FGTM
14!	<b>052 100</b>	16.7N	130.5E	PCH 6		BRKS CONTINUITY	PGTW
142	952319	16.4N	129.7E	PCN 5	T4.0/5.0 /U1.0/24HRS	ULCC FIX	RODH
	060000					ULAC 16.8N 128.4E	PGTW
					** * * * *	OWNER TO OUT TER THE	
144			129.0E		T3.5/4.5-/⊌1.5/24#RS		PGTW
145	<b>0</b> 60552	15.5N	128.3E	PCN 6			PGTW
146		15.3N		PCN 6			PGTW
						JE OC ETV	
147		14.8N		PCN 6		ULAC FIX	PGTW
148	8612 <del>8</del> 8		127. IE	PCN 6			PGTW
149	061600		126.2E	PCN 6			PG TW
				PCN 5			PGTU
150	061007		126.2E				
151	062100	13.BN	125.7E	PCN 6			PGTU
152	862247		125.7E	PCN 1	T4.0/4.0-	INIT UBS	RPHK
			125.3E	PCH 4		- •·•	PGTU
153							
154		13.3N		PCH 6			PGTW
155	878688	13.0N	124.8E	PCN 4	T4.8/4.5-/D8.5/27HRS		PGTW
156	070652		123.9E	PCN 5			RPMK
157		13.6N		PCH 6			PGTW
158	871288	13.0N	122.6E	PCN 6			PI-TW
159	071537		120.7E	PCN 3		FXP LLCC	RPMK
							RPIN
168	000004	9.8N	113.bE	PCN 3			KF I W

### AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	788MB HGT	ORS MSLP		-SFC- ⁄PRG				-I.VI /BPG/				EYE SHAPE		RIEN- ATION			MP (C) DP/SST	MSN NO.
1	251915	7.5N 169.4E	780MB	2959		45	200	10	330	36	288	10	7	3							1
2	252016	7.7N 169.2E	700MB	2963	985	60	130	15	200		120	30	7	4	EI LIPTICAL		120	+11	+14	+ 9	1
3	268625	8.5N 167.6E	700MB	2099	980				340		230	40	7	3	C IRCULAR	12		+13 -			2
4	260844	8.8N 167.0E	700HB	2894					200		110	5	5	2	CIRCULAR	5		+13	+16	+12	2
5	261826	9.6N 164.9E	7 <b>99</b> MB	2817			188		050		340	18	7	2	C IRCULAR	22					3
6	262055	9.8N 164.5E	700:18	2016	967		178	7	658		318	7	. 5	2	CIRCULAR	25		+12			3
7	270630	10.5N 162.8E	790MB	2585	940	90	828	8	110		826	30	19	2	CIRCULAR	12		+15			5
8	270907	10.8N 162.3E	760119	2577					300		200	30	.5	2	CIRCULAR	15		+14	+18	+12	5
. 9	271855	11.6N 160.9E	700119	2647					178		090	30	10	2	CIRCULAR	15					6
18	272119	11.7N 168.6E	786MB	2673	953	26	350	48	670		320	15	10	2	C (RCULAR	20		+11 -			6 9
11	288827 281126	12.8N 159.7E	700MR	26 42 2653	947				240	189		20 20		5 18	CIRCULAR	35		+13	+IR	+10	9
13	282185	13.8N 159.2E 13.5N 158.7E	786HB 786HB	263 <b>8</b>	958	118	150	18	218	110		15	7	3	CIRCULAR	15		+12 -			18
14	290000	13.7N 158.4E	7881B	2786	330		166	10	158	100		18	7	3	CIRCULHIK	13		¥12 ·	F20	T 3	10
15	290640	13.7N 158.1E	7881B	2914	979			38	288		218	14	5	5	CIRCULAR	48		+28 -	421	412	12
16	298928	13.6N 158.0E	788HB	2967	J. J	-	200	50	626		298	50	10	ě	CINCOLIN			+13 -			12
17	292126	12.8N 156.5E	7001B	3016	992	75	220	12	020		280	28	8	5				+14			13
18	388822	12.3N 156.0E	78019	3029			360	70	120	59	360	21	6	6						• •	13
19	388813	11.9N 154.2E	788MB	3056	998				929	50	278	45	18	5				+11 -	+17	+ 5	14
28	301104	11.5N 153.5E	7001B	3073					998	63	330	130	10	5					+18		14
21	302127	11.5N 150.BE	788NB		1002	35	898	190	206	26	<b>090</b>	30	8	3				+13 -	+12	+ 6	16
22	010013	11.7N 149.7E	706MB	3102		55	270	18	100		646	78	8	3							16
23	<b>818626</b>	11.9N 147.6E	700MB	3075	999	45	310	17	868		320	127	6	4							17
24	010903	11.6H 146.8E	7 <b>00MB</b>	3102					120		360	135	6	3				+10 -		+ 7	17
25	011532	12.1N 143.8E	7 <b>00</b> MB	3083					968		366	38	10	3					+13		18
26	012150	12.2N 142.0E	700MB		998	35	360	10	150	48		15	10	5					+13		18
27	020850	12.2N 138.2E	950MB						999		100	68	16	5				•	+19	+15	19
28 29	021155 022126	12.5N 137.4E	956MB	2050	000		710		140		848 318	38 30	10	5							19 20
30	030019	13.4N 135.1E 13.8N 134.5E	700MB 700MB	3058 3020	998		310 270	15 7	949 150		060	40	10	5				+18 -	112	+ 9	28
31	630663	14.4N 133.2E	790MB	3010	989		320	é	160		898	13	18	3							21
32	030853	14.6N 132.8E	780H9	2964	983		260	10	238		148	68	18	2				+12 -	410		21
33	032135	15.4N 131.3E	700MB	3002	988		050	30	150		650	55	18	3	ELL IPTICAL	28 18	180		+17		22
34	040034	15.5N 131.1E	788MB	3006			298	15	820		200	7	10	3					+16		22
35	J40841	15.8N 130.4E	788MB	2947	983		300	5	120		830	20	5	5	CTRCULAR	28		+18			23
36	041127	15.9N 130.2E	700MB	2922				_	300	62	240	10	12	5				+10	+17	+ 8	23
37	042100	15.9N 129.7E	700MB	2769					300	98	218	7	6	2	C IRCULAR	15		+16	+19	+ 8	24
38	042332	16.1N 129.5E	70011B	2744	958	90	310	7	368	94	310	10	4	2	CIRCULAR	10		+16	+24	+ 5	24
39	<b>858682</b>	16.3N 129.4E	700MB	2871		60	278	10	330	90	200	10	10	3					+22	+ B	25
48	050040	16.4N 129.2E	700MB	2984	9R5	60	290	15	358	63	2 <b>90</b>	15	10	5					+21	+ 5	25
41	060633	15.2N 128.2E	700MB	3014				12	190		100	6	18	3					+12		27
42	060903	14.8N 127.8E	700MB	2977	987			5	350		270	10	10	2	ELLIPTICAL	8 6	020	+13			27
43	062156	13.5N 126.RE	700MB	3004	994		258	5	100		360	5	5	2	ELL IPTICAL	15 18	910	+14	+15	+ 6	28
44	<b>07003</b> 2	13.2N 125.2E	700MB	3044		90	368	5	178	55	989	10	5	3							28
							ı	RADAR	FIXE	5											

Ety	TIME	FIX			EYE	EYE	RADOB-CODE		RADAR	SITE
	(Z)	POSITION	RADAR	ACURY	SHAPE	DIAM	ASUAR TODEF	CONTENTS	POSITION	LIND NO.
1	260330	8.2N 167.9E	LAND	FAIR					8.7N 167.7E	91366
2	268438	8.3N 167.8E	LAND	FAIR					8.7N 167.7E	91366
3	260930	8.8N 167.0E	LAND	FAIR					8.7N 167.7E	91366
4	261030	9.6N 166.8E	LAND	FAIR					8.7N 167.7E	91366
5	261130	9.1N 166.4E	LAND	FAIR					8.7N 167.7E	91366
6	261230	9.2N 166.2E	LAND	POOR					8.7N 167.7E	91366
7	811250	12.3N 145.1E	LAND	FAIR					13.6N 144.9E	91218
Θ	011345	12.3N 144.8E	LAND	FAIR					13.6N 144.9E	91210
9	011435	12.4N 144.4E	LAND	POOR					13.6N 144.9E	91218
10	011535	12.6N 144.2E	LAND	POOR					13.6N 144.9E	91218
11	861488	14.4H 127.8E	LAND				35226 42215		14.8N 124.3E	98447
12	861588	14.2N 127.0E	LAND				35219 41811		14.8N 124.3E	98447
13	061600	14.2N 126.9E	LAND				10331 42406		14.0N 124.3E	98447
14	861788	14. IN 126.7E	LAND				18221 42460		14.8N 124.3E	98447
15	661986	14.1N 126.4E	LAND				18211 52418	EYE CIRCULAR	14.8N 124.3E	98447
16	<b>061900</b>	13.8N 126.2E	LAND				18211 52219	EYE CIRCULAR	14.0N 124.3E	98447
17	079999	13.4H 125.4E	LAND				10331 52707	EYE CIRCULAR	14.8N 124.3E	98447
10	079600	12.6N 124.1E	LAND				10432 42710		14.0N 124.3E	98447
19	070700	12.5N 123.9E	LAND				18412 42518		14.6N 124.5E	98447
20	070900	12.4N 123.7E	LAND				10412 42610		14.8N 124.3E	98447
21	9711 <del>9</del> 0	11.9N 122.9E	LAND				10312 42713		14.00 124.3E	98447
22	871888	11.0N 122.8E	LAND				10312 42512		14.8H 124.3F	98447

### SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
	250420 260610	7.3N 171.8E 8.5N 167.7E	850 865	825 815	UHD 9	1376 1366 KWAJALETH
7	878988	12 2N 127 7F	8.45	816	LEND O	05.47

### TYPHOON ROGER BEST TRACK DATA

	BEST	TRACK		LINRN		ROPS		24 H	OUR FO	DRECA:			48 11	OUR F	DRECA!			72 HO		RECAS	
MD/DA/HR	POSIT	MIND	POSIT	MIND	DST	MIND	P05	iT.	GHIU	DST	WIND	POS	T	WIND		WIND	POS	ĮT.	MIND	DST	UIND
1207062	10.1 130.		0.0 B.		-8.	8.	8.8	8.8	8.	-8.	8.	0.0	0.8	0.	-0.	■.	8.8	0.0	8.	-●.	6.
1207122	10.0 129.		8.8 8.	D 0.	-8.	8.	8.8	0.0	ø.		e.	0.0	0.6	0.	-A	€.	8.8	0.0	8.	-a.	0.
120718Z	11.5 127.	2 48	8.0 8.	D 8.	··B.	e.	8.0	0.0	8.	-8.	ø.	0.8	8.6	0.	-0.	8.	8.8	<b>8.8</b>	₩.	-0.	8.
120000Z	12.4 125.	5 50	11.8 125.	7 58.	30.	ē.	13.5	120.3	45.	134.	-20.	13.3	116.8	55.	433.	15.	8.6	8.8	0.	-8.	8.
1208062	13.2 124.	2 55	12.8 124.	2 58.	24.	-5.	13.8	119.8	58.	202.	-15.	14.8	114.2	55.	549.	25.	0.0	8.8	8.	<b>-8</b> .	٥.
1200122	13.8 123.	3 55	14.2 123.	5 55.	30.	ð.	16.3	120.0	50.	127.	-19.	18.4	118.1	35.	243.	10.	0.0	0.0	8.	-8.	٠.
120818Z	14.5 122.	4 60	14.4 122.	4 68.	6.	ø.	16.9	119.3	45.	105.	~5.	18.9	17.0	35.	307.	18.	6.6	6.6	0.	-8.	ð.
1209002	15.0 122.	0 65	15.1 122.	B 65.	6.	₽.	17.4	119.5	50.	175.	10.	0.0	0.8	0.	-0.	8.	8.6	8.8	e.	-0.	٥.
120906Z	15.8 121.	8 65	15.6 121.		21.		17.9	119.8	50.	158.	20.	0.0	6.0	0.	-8.	8.	0.0	8.8	0.	<b>-0</b> .	0.
1209122	16.5 122.	2 68	16.4 122.	2 68.	6.	8.	19.8	122.4	45.	25.	20.	8.9	6.0	0.	-0.	Ø.	Ø.0	0.0	8.	-0.	0.
1209182	17.3 122.	5 58	17.4 122.	4 55.	8.	5.	19.8	122.8	45.	29.	20.	9.0	8.8	8.	-Ð.	9.	0.0	0.0	٥.	-0.	٥.
121000Z	18.6 122.	5 40	17.8 122.	B 55.	21.	15.	8.0	0.0	e.	-0.	e.	0.6	0.0	Θ.	-0.	8.	0.0	0.0	0.	-Ð.	٥.
1218062	18.5 122.		18.5 122.		0.	e.	8.8	0.6	ย.	-0.	0.	0.0	0.0	0.	-0.	Θ.	0.0	8.0	₩.	-8.	8.
1219122	19.2 122.		18.7 122.		31.	5.	6.8	0.0	ē.	~0.	ø.	6.6	0.0	6.	- <b>6</b> .	ø.	8.8	0.0	8.	-0.	8.
1218182	19.9 122.	_ ==	19.8 122.	2 25.	8.	ē.	0.0	0.0	ø.	-8.	ø.	0.0	9.0	0.	-0.	0.	0.0	0.0	Θ.	-Ð.	₽.

	ALL	FORECAS	TS		TYPHO	ONS WHI	LE OVER	35 KTS
	LIRNG	24-HR	48-HR	72-HR	LENG.	24-HR	48 -HR	72-HR
AVG FORECAST POSIT ERRUR	17.	129.	383.	0.	18,	165.	433.	0.
AVG RIGHT ANGLE ERROR	12.	116.	329.	6.	15,	148.	319.	0.
AVG INTENSITY MAGNITUDE ERROR	3.	15.	15.	0.	3,	12.	15.	0.
AVG INTENSITY BIAS	2.	3.	15.	8.	2,	-8.	15.	0.
MINERED DE ENDECORTS	12		4		9	5	1	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 986. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON ROGER
FIX POSITIONS FOR CYCLONE NO. 28

### SATELLITE FIXES

F1X NO.	TIPE (Z)	FIX POSITION	ACCRY	DVDRAK CODE	COPPENTS	STIE
		5.3N 145.3E	PCN 6		ULCC FIX	PGTW
1	841888 850000	6.8H 145.7E	PCN 6	T1.8/1.8	INIT OBS	FGTU
3	050300	4.4H 142.2E	PCN 4	11.0-1.0		PGTW
3	050534	4.6N 141.7E	PCN 3			PGTW
5	858688	4.8N 141.7E	PCN 4			POTU
6	858988	4.3H 141.1E	PCN 6		ULAC FIX	Politi
7	851260	4.7N 141.8E	PCN 6		ULCC FIX	FGIU
ė	651688	5.3M 138.9E	PCN 6		ULCC FIX	PGTM
9	868888	7.4H 137.5E	PCN 6	T8.5/8.5 /WB.5/24HRS		PGTIA
18	868388	7.7N 137.1E	PCN 6			PGTIJ
ii	871888	11.2N 127.0E	PCN 6		ULCC FIX	PG TIJ
12	872188	11.3N 126.6E	PCN 6			PGTW
13	888888	12.6N 126.0E	PCH 4	T3.5/3.5-	INIT OBS	PGTW
14	866664	12.1N 126.0E	PCN 3	T3.0/3.0	INIT OBS	RPIK
15	898388	12.6N 124.0E	PCN 6			PG FU
16	000600	13.4H 124.5E	PCH 4			PGTW
17	000639	13.2H 124.1E	PCH 3			RP11K PG (U
18	080900	13.8N 124.4E	PCH 6			PG TU
19	881288	14. IN 123.9E	PCH 6			PGTIJ
28	<b>88</b> 1688	14.5H 122.9E	PCN 4			PGTU
21	<b>66</b> 1896	14.7N 122.6E	PCH 4			RPIN
22	<b>68</b> 1924	14.5H 122.3E	PCH 3			PGTLI
23	862166	14.8N 122.2E	PCN 2			RETR
24	692346	15.8N 122.2E	PCN I	T4.5/4.5 /D1.5/24/RS		PSTU
25	696668	15.8H 122.1E	PCN 2	T4.5/4.5-/D1.8/24根S		PG III
26	696366	15.3N 121.8E	PCN 2			PGP4
27	<b>090</b> 627	15.6N 121.7E	PCH 3			PGTW
28	090900	16.0N 121.7E	PCN 4			PPLK
29	J <b>90900</b>	15.9N 122.1E	PCN 2			rgru
30	891288	16.4N 121.9E	PCH 6			PG IW
31	891688	17.1N 122.4E				PGTU
32	091000	17.4H 122.5E	PCN 6		EXP LLCC	RETT
33	891912	16.7N 123.0E			LIV ELEC	RODII
34	<del>69</del> 1912	17.2N 122.5E	PCH 6			

35	892188	17.7N 122.8E	PCN 6			PGTU
* 36	892316	17.5N 124.2E	PCN 5	T3.5/4.5-/U1.0/24HRS		RPI 6:
37	100000	17.7N 123.4E	PCN 6	T3.8/4.8-/U1.5/24/RS	ULCC FIX	PG (W
* 38	199399	17.5N 124.BE	PCN 6		ULCC FIX	PGIU
39	100615	18.6N 122.5E	PCH 5			PGTW
48	101660	19.8N 122.2E	PCH 4			PGTU
41	102100	28. IN 122.4E	PEN 4		EXP LLCC	rsru
42	110000	20.5N 122.7E	PCH 4	18.5/1.5 /LZ.5/24#RS	FXP LLCC	raru
43	118308	28.8N 122.9E	PCH 4			PGTW
44	110603	21.3N 123.3E	PCN 3		EXT LLCC	PGTW

### AIRCRAFT FIXES

	TIME (Z)	FIX POSITION	FLT LVL				MAX-FLT-LVL-WHD DIR/VEL/BRG/RNG		EYE SHAPE	EYE OF LEH-	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
2	100627	18.5N 122.5E	70016	3113	–	38 248 9	160 65 888 18 288 34 898 128 184 15 368 158	5 3			+12 + 8 +15 + 7	1 2

### RADAR FIXES

FIX	TIME	FIX			EYE	EYE	RADOS-CODE		RADAR	SITE
NO.	(Z)	POSITION	RADAR	ACCRY	SHAPE	DIAM	INSUING TODEF	COM ENTS	POSITION	UND NO.
		10011101	KHUMK	THOUSE !	31 m L	D 21111	HOWART (DDT)	CONTENTS	rovillon	www.
1	<del>00</del> 0400	12.8N 125.0E	LAND				10402 50000		14.0H 124.3E	96447
Z	966666	13.6N 124.5E	LAND				10422 42710		14.6H 124.3E	98447
3	<b>000</b> 930	13.7N 123.BE	LAND				10433 42911		14.6H 124.3E	98447
4	06 i 000	13.8N 123.8E	LAND				25/43 42909		14.9H 124.3E	98447
5	00 1 1 <del>00</del>	13.6N 123.7E	LAND				20/21 62203		14, 111 123.0E	98440
6	<b>0</b> 812 <b>00</b>	13.0N 123.4E	LAND				10121 43222		14, III 123.0E	93440
7	<b>0</b> 01300	13.9N 123.4E	LAND				20/31 40900		14.14 123.9E	90 4 10
8	<b>861466</b>	14.4N 123.2E	LAND				20/21 43211		14.1H 173.8F	90447
9	861688	14.5N 122.6E	LAND				11131 42789		14, 81 (23,05	90448
16	<b>981788</b>	14.5N 122.4E	LAND				22131 42707		14.10 123.0E	38440
11	<b>091700</b>	14.7N 122.5E	LAND				1863/ 48000	EYE 100 PCT CIR DIA 35KHS	16,34 129.65	98321
12	661736	14.7N 122.5E	LAND				1063/ 42802	EYE 90 PCT LIR DIA 35U S DPH GC	16.3H 120.5E	98321
13	<b>6</b> 618 <b>66</b>	14.7N 122.4E	LAND				1179/ 42702	EYE 100 PCT ELPTCL DIA 40/30/06	16.31 128.6F	98321
14	881988	14.7N 122.3E	LAND				1179/ 40090	EYE 100 PCT ELPTCL DIR 48/30KHS	16.30 120,6E	96321
15	090100	15.2N 121.9E	LAND				10312 42902		16.3H 129.6E	98.21
16	<b>090400</b>	15.5N 121.8E	I AND				18222 4368?		16.3H 120.6F	98321
17	890738	15.9N 122.0E	LAND				10412 40303		16.3H 128.6F	9H321
18	090830	16.0N 122.1E	LAND				10412 40381		16.3H 129.6E	90321
19	<b>090900</b>	16.1N 122.1E	LAHD				10412 40204		16.3N 120.6E	98321
20	891130	16.5N 122.3E	LAND				10411 40103		16.3H 120.6F	98321
21	891288	16.6N 122.3E	LAND				1811/4914		16.30 120.65	98321
22	<b>09</b> 1238	16.7N 122.3E	LAND				1641/40104		16.31 128.6F	90321
23	691466	16.9N 122.3E	LAND				1851/ 58204		16.3H 128.6F	96321
24	091430	17.0N 122.3E	LAND				1941/ 43684		16.311 120.65	38321
25	Ø9 1500	17.8N 122.3E	LAND				1041/ 40000	EYE 90 PCT CIT OPEN NE	16.3N 128 6F	99321

### SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
	081400		055 050 850	020 905 030	W10 98444, W10 98446 W10 98333	98447

NUTICE - THE ASTERISKS (#) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR PEST TRACK PURPOSES.

### 2. NORTH INDIAN OCEAN TROPICAL CYCLONES

TROPICAL CYCLONE 28-82 BEST TRACK DATA

		BEST	TRACK			WARN I				24 H	OUR FO	ORECAS			48 HC	IUR FO	PRECAS			72 HO		RECAS	
							ERF	RORS				ERRO					FREGI					RRURS	
MO/DA/HR	POSI	T I	MIND	POS	IT	UH1111	DST	MIND	POS	IT.	MIND	PST	MIND	FOS	I T	LIIND	DST	MIIII	POS	[T	MIHD	DST	MIND
043002Z	11.4	82.7	20	0.0	9.0	0.	-8.	Ø.	0.0	0.0	€.	-0.	0.	0.0	9.0	0.	- И.	Ð.	0.8	0.0	ø.	-:0.	0.
<b>8438882</b>	12.8	82.4	25	0.0	0.0	0.	-⊌.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-Ø.	0.	8.0	0.0	P.	-0.	0.
0430147	12.7	82.1	25	0.0	8.0	a.	-0.	8.	0.0	0.0	9.	-0.	ø.	9.0	9.0	ø.	·ø.	9.	8.0	0.0	n.	-0.	e.
043020Z	13.5	82.0	25	0.0	0.0	Ñ.	-ð.	ø.	0.0	8.0	e.	-0.	ä.	0.0	0.0	ø.	-A.	0.	0.0	0.0	и.	-d.	a.
050102Z	14.3	82.2	30	0.0	0.0	ă.	-0.	e.	0.0	8.0	ø.	-a.	ø.	0.0	0.0	ø.	Θ.	ø.	8.0	9.0	n.	-0.	A,
950106Z	14.8	82.5	30	0.0	0.0	ä.	-0.	0.	0.0	0.0	0.	ъ.	ø.	U.0	0.0	ø.	· Ø.		0.0	81.0	Р	- И	и.
0501142	15.3	82.8	35	0.0	0.0	۵.	-0.	e.	6.6	6.6	я.	0.	0	9.0	0.0	6.	- A.	. 0	и.в	9.8		· e.	2.
0501142 050120Z	15.8	83.3	35	0.0	0.0	υ.			9.0		ø.	- 0.	Я.	8.0	0.0	ø.	- 0.	Ö.	9.0	0.0	9.	-tı.	9.
						٠.	-0.	0.		0.0						50.		7B.	19.8	89.3	69.	448.	19.
050202Z	16.2	83.6	40	16.2	82.8	25.	58.	-15.	17.8	84.1	49.	159.	-48.	19.6	86.2		304.						
050208Z	16.4	84.4	50	16.7	83.8	30.	39.	-20.	17.9	86.9	45.	55.	-45.	18.6	90.1	55.	194.	-10.	19.0	93.4	65.	232.	30.
05021 <i>42</i>	16.8	85.2	60	16.8	84.8	60.	23.	0.	18.1	B6.9	70.		-30.	18.8	89.2		330.	-25.	0.0	0.0	41.	.0	0.
050220Z	17.0	85.9	70	17.0	65.2	65.	10.	-5.	10.1	87.0	75.	186.	~35.	19.1	89.3	86.	из.	10.	0.0	0.0	ø.	-ი.	٤.
<b>05030</b> 22	17.2	86.8	89	17.3	96.8	65.	6.	-15.	10.2	89.5	75.	111.	- dä.	19.0	92.2	85.	277.	35.	0.0	0.0	H.	-0.	٩.
<b>0</b> 50308Z	17.4	87.7	90	17.5	87.8	75.	В.	- 15.	10.1	90.9	85.	142.	40 .	18.6	94.1	75.	189.	4PL	0.0	ย.ก	ß.	∙0.	0.
050314Z	17.4	88.9	100	17.6	88.7	85.	17.	-15.	19.1	92.0	85.	165.	-10.	0.0	0.0	8.	-⊌.	ø.	0.0	Ø.A	11	~B	я,
050320Z	17.5	90.2	110	17.7	89.8	95.	26.	-15.	17.8	94.2	90.	115.	20.	0.0	0.9	8.	-0.	0	0.0	0.0	1.	-0.	0.
858482Z	17.5	91.3	128	17.4	91.2	128.	В.	e.	17.7	95.6	90.	75.	43.	0.0	0.0	ø.	0.	ø.	9.8	0.0	ч.	-0.	0.
959498Z	17.5	93.3	125	17.5	93.8	130.	17.	5.	17.B	98.2	40.	52.	5.	0.0	0.0	e.	-0.	ø.	0.0	0.9	٠.	-0,	0.
050414Z	17.4	94.8	95	17.5	94.9	100.	В.	5.	0.0	9.0	Ã.	-0.	ē.	8.8	0.0	ø.	-0.	0.	0.0	0.0	q.	-0.	ø.
050420Z	17.6	96.2	78	17.5	95.9	65.	18.	-5.	0.0	8.0	ă.	-0.	è.	8.0	0.0	ø.	ñ.	ø.	0.9	3.0	n.	· 0.	e.
050502Z	17.8	96.9		17.4	97.2	50.	30.		0.0	B.0	ů.	· 8.	ø.	8.8	0.0	ø.	-0.	ย.	0.0	6.0	Р.	-A.	ø.
	••••		50	• · · ·				ø.			٥.					ø.	-9.	ø.	0.0	9.0	0.		В.
05050BZ	18.2	97.4	35	17.0	97.2	35.	27.	0.	0.0	Р. И	٠.	-0.	Θ.	ө.ө	0.0	ъ.	-9.	0.	0.9	71.17	ø.	∙ 6.	о.

	ALI	FORECAS	iT5		TYPHU	3145 149111	E BATE	30 1/15
	WRNG	24-HR	48-HR	72-HR	HRNG	24-HP	48 HP.	72 HR
AVG FORECAST POSIT ERROR	23.	118.	263.	3/10.	0.	0.	0.	Ю.
AVG RIGHT ANGLE ERROR	14.	43.	87.	116.	и.	a.	0.	Ю.
AVG INTENSITY MAGNITUDE ERROR	θ.	31.	42.	20.	0.	0.	0.	A.
AVG INTENSITY BIAS	-7.	-18.	-13.	20.	0.	Θ.	8.	0.
NUMBER OF FORECASTS	14	10	6	2	Ð	ы	n	U

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1135. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

9. KNOTS

TU28-82 FIX POSITIONS FOR CYCLONE NO. 28

### SATELL ITE FIXES

	1X 10.	TIME (Z)	FI) POSIT		ACCRY	DVORNK CODE	COMENTS	SITE
*	1	248828	4.3N	89.2E	PCN 5	T1.0/1.0	INIT OBS ULAC 2.4N 90.7E	KGUC
*	2	242115	4.7N	86.9E	PCH 6		ULAC 2.8N 87.DE	K! WC
	3	300900	12.0N	82.0E	PCN 5	T1.5/1.5	INIT OBS III AC 12.8N 81.BE	KGUC
	4	301435	12.2N	81.8E	FCN 6			KGUC
	5	302144	13.6N	82.1E	PCN 6		ULAC FIX	KGWC
	6	302145	13.BN	82.8E	PCN 6			FJDG
	7	010300	14.6N	82.4E	PCN 5	T2.0/2.0	INIT JBS ULCC FIX	PRTIJ
	8	010048	15.1N	82.6E	PCN 5	T3.0/3.0 /D1.5/24HR5	ULAC FIX	KUPIC
	ě	016848	15.6N	82.9E	PCN 6			FIDG
	10	011290	15. IN	91.7E	PCN 5			PGTW
-	ii	011412	15.3H	83. IE	PCN 6		ULAC FIX	KGUC
	12	011800	15.9N	82.8E	PCN 5			PGTW
_	13	012132	15.7N	83.0E	PCN 6		ULAC FIX	KGWC
	14	020250	16.BN	84.5E	PCN 5			KRUC
	15	020360	16.5#	93.2E	PCN 5	T3.8/3.8 /D1.8/24HR5		PGTH
	16	020836	16.3N	84.6E	PCH 5	T4.5/4.5 /D1.5/2/HRS		KUINC

17	821288	16.6N	84.2E	PCN 5			PGT⊌
18	821348	16.7N	85.8E	PCN 4		EYE DIA 6N	
19	821348	17.3N	84.5E	PCN 6			FJDG
28	821688	16.6N	84.8E	PCN 1			PGTU
21	821866	16.7N	85. IE	PCN 1			PGTU
22	822128	17.6H	86.8E	PCH 2		EYE DIA 6H	H KGLIC
23	838227	17.1N	86.9E	PCN 1		EYE DIA 16	NM KGHC
24	038300	17.2N	86.4E	PCN L	T4.5/4.5 /D1.5/24RS		PGTU
25	030680	17.41	87.8E	PCN 1			PGTW
26	030823	17.44	87.7E	PCH 1	T6.8/6.8 /01.5/24RS	EYE DIA 16	RM KGWC
27	<b>831288</b>	17.41	88.4E	PCN 1			PGTW
24	631324	17.6H	88.7E	PCH 2		EYE DIA 18	nm kgwc
29	831688	17.44	89.2E	PCN 1			PGTU
38	831886	17.44	89.6E	PCH 1			PGTW
31	<b>032100</b>	17.40	90.3E	PCN 1			PGTU
32	832188	17.49	90.2E	PCN 1		EYE DIA 10	
33	840203	17.3N	91.9€	PCN 1		EYE DIA 9N	
34	840388	17.5H	91.7E	PCH 1	15.5/5.5-/D1.8/24HRS		PGTU
35	648686	17.5N	92.5E	PCH 1			PGTU
36	848911	17.3N	93.5E	PCN 1	15.5/6.8-/W0.5/24HRS	EYE DIA 12	
37	040900	17.6N	93.4E	PCN 1			PGTW
38	841288	17.6N	94. IE	PCH 1			PGTU
39	841588	17.6N	94.8E	PCN 3			PGTW
48	841999	17.5N	95.4E	PCN 3			PGTW
41	042856	17.6N	96.6E	PCN 6			KGUC
42	842188	17.5N	96.4€	PCN 5		ULCC FIX	PGTU
43	050000	17.5N	96.8E	PCN 5			FGTW
44	050300	17.7N	97.0E	PCN 5	T3.0/4.0 /42.5/24HRS		PGTU
* 45	858759	17.7N	99.2E	PCN 5	T3.8/4.8 /42.5/24HRS		KGUC
* 46	250818	4. BN	85.2E	PCN 5	T0.5/1.0 /48.5/24RS		KGUC

NOTICE - THE ASTERISKS (\*) INDICATE FINES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

### TROFICM. CYCLONE 22-82 REST TRACK DATA

		BEST	TRACK	:		WARH I		RORS		24 H	OUR FO	ERRI ORFCN			49 HI	our io	DRECA!					RECAS RRORS	
MD/DA/HR	POS I	T	UIND	POS	11	MIND	DST	MINID	คกร	1T	MIND	DST	UIIID	1.05	11	HIHD	DS T	WIND	POS	IT	MIND	DST (	w'IND
8681282	16.9	89.3	5 25	0.0	0.0	8.	-8.	0.	9.6	0.0	Ø.	-0.	8.	0.0	9.9	0.	· B.	₽.	8.8	8.0	٥.	-0.	e.
8682822	17.3	89.	3 30	0.0	8.0	ø.	- 0.	ø.	9.8	8.A	ø.	-·U.	ø.	0.8	0.0	8.	-8.	0.	P.0	0.0	8.	0.	9.
9602082	17.7	89.	30	18.2	88.9	38.	32.	0.	19.6	98.3	40.	49.	·· 15.	21.0	88.2	40.	238.	16.	0.0	0.6	8.	-A.	8.
0602142	18.0	89.	7 35	18.5	88.8	35.	31.	8.	19.0	86.2	40.		-15.	9.6	Ø.6	0.	· 0.	0.	3.0	0.0	A.	- 3.	0.
0682282	10.3	88.	2 40	18.6	88.5	40.	25.	0.	19.5	87.9	45.	1 18.	0.	H.0	0.6	0.	-0.	0.	8.8	6.0	0.	-8.	Ð.
8683822	18.8	87.5	9 45	19.0	87.9	45.	12.	0.	20.8	96.8	45.	173.	5.	6.8	6.0	Θ.	и.	0.	0.0	0.0	0,	-0.	0.
8683882	19.6	87.6	5 55	19.7	87.2	45.	23.	-10.	22.2	86.8	40.	134.	10.	0.6	0.0	θ.	8.	8.	8.8	8.8	8.	-0.	0.
0603142	20.2	86.	7 55	20.2	87.1	45.		-16.	0.0	0.0	Ø.	-0.	u.	0.0	8.8	0.	- 0.	0.	0.0	8.0	8.	-0.	8.
	21.2	86.	8 45	21.6	86.2		16.	0.	0.0	0.0	0.	0.	Ö.	0.0	0.0	A.	0,	0.	8.9	0.0	0.	-6.	0.
8684822	22.2	85.	2 48	22.3	85.5		18.	e.	0.6	0.0	Θ.	-0.	0.	0.0	0.0	0.	~0.	ø.	0.0	0.0	9.	-0.	0.
0604082	23.3	84.	7 30	0.0	0.6	ø.	-8,	ø.	6.0	0.6	8.	-8.	ø.	8.8	Ø. H	A.	-8.	8.	8.0	8.8	ø.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	DNS WHIL	E DVER	35 KTS
	WRNG	24 HR	48 -HR	72-HR	UPHG	2:1-HR	40 HR	72-HR
AVG FORECAST POSIT ERROR	22.	1 <del>0</del> 6.	238.	0.	0.	8.	0.	8.
AVG RIGHT ANGLE ERROR	16.	36.	85.	₽.	0.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	3.	9.	10.	0.	0.	0.	0.	Ø.
AVG INTENSITY BIAS	-3.	-3.	10.	0.	0.	0.	Θ.	8.
NUMBER OF FORECASTS	8	5	1	0	0	0	9	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 482. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 8. KNOTS

TC22-82
FIX POSITIONS FOR CYCLONE NO. 72

### SATELLITE FIXES

FIX		FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMPENTS	SITE
1	300600	13.5N 87.8E	PCN 5	T1.5/1.5 .	INIT OBS	FGTU
2	31 <del>0600</del>	14.9N 90.6E	PCN 5	T2.0/2.0 /D0.5/24HRS		PGTU
3	310752	15.2N 91.1E	PCN 5	T1.0/1.0	INIT OBS ULAC FIX	KGWC
4	311600	15.9N 89.7E	PCN 5		ULCC FIX	Patu
5	312037	15.7N 89.3E	PCN 6		ULAC FIX	Kuti #0
6	010600	16.5N 92.3E	PCN 3	T1.5/2.0 /W0.5/24HRS		PG TW
7	011200	17.8N 92.6E	PCN 5			PGTW
8	011600	17.8N 88.9E	PCN 5		ULCC FIX	PGTW
9	012025	16.8N 89.4E	PCN 6		BASED OH EXTRAP	KGUC
18	012190	17.4H 89.9E	PCN 5		LLCC 16.0N 93.3E	PG TW
11	0200 <del>00</del>	17.8N 89.6E	PCN 5		ULCC FIX	PGTW
12	020225	16.8N 89.5E	PCH 5	T2.0/2.0 /D1.0/30HRS	ULAC FIX	KGUC
13	020600	17.9N 88.8E	PCH 5	T2.0/2.0 /D0.5/24HRS		PG TW
14	<b>0</b> 20910	18.8N 89.2E	PCN 5	T2.5/2.5 /D8.5/9GHRS		KGWC
15	<b>021600</b>	17.9N 88.4E	PCN 5			PGTW
16	021 <del>8</del> 00	18.3N 88.2E	PCN 5			PGTW
17	<b>0</b> 22100	18.6H 87.7E	PCN 5			PGTU
18	022155	18.6N 98.9E	PCN 6		ULAC FIX	KGWC
19	03 <del>000</del> 0	19.0N 97.8E	PCN 5			PGTW
20	<b>03030</b> 0	19.4N 87.7E	PCN 5			PGTU
21	030600	19.6N 87.5E	PCN 5	T2.0/2.0=/\$0.0/24HR5		PRTW
22	030058	19.9N 87.5E	PCN 3	T3,5/3.5 /D1.0/24HRS	EYE DIA 15NM	KGUC
23	8389 <del>88</del>	19.7N 86.9E	PCN 5	•		PGTW
24	031200	20.1N 87.0E	PCN 5			PGTW
25	<b>0</b> 316 <b>00</b>	28.5N 86.7E	PCH 5			PGTW
26	631866	21.0N 86.5E	PCN 5	a a		PG1W
27	832188	21.5N 85.9E	PCN 5	*		PGTU
28	032143	21.2N 85.8E	PCH 6			KGWC
29	<b>040000</b>	21.9N 85.5E	PCN 6		ULCC FIX	PGTW
38	040300	23.2N 05.7E	PCN 6	T1.5/2.0 /W.5/21HRS		PGTW
31	<b>640</b> 846	23.4H 84.5E	PCN 5	T1.0/2.0-/42.5/244PS		KGUC

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TROPICAL CYCLONE 23-82 BEST TRACK DATA

		BEST	TRACK			UARN I				24 H	OUR FO	ORECA	57		48 H	DUR H	URECA	51		72 H	DUR FO	WŁCAS	iΤ
							ER	RORS				FRR	)RS				FPPO	.'5			ε	RRORS	j
MO/DA/HR	POSI	T	MIND	POS	IT.	MIND	DST	MIND	POS	IT.	MIND	DST	WILLIAM	POS	IT	WILL	PST	MIND	POS	ΙT	MIHD	DST	UNIL
101320Z	13.2	91.	5 25	0.0	0.0	0.	-0.	0.	0.0	0.6	0.	-0.	0.	9.0	8.8	8.	Ð.	0.	0.0	6.6	0.	-0.	8.
1014022	13.8	90.	6 30	0.8	8.0	0.	-0.	0.	0.6	8.0	0.	-0.	e.	0.0	0.0	ø.	-0.	ø.	0.8	0.0	ø.	Θ.	0.
101409Z	14.2	89.	6 30	0.0	0.0	8.	-8.	ø.	0.0	0.0	8.	-8.	Ð.	B. 8	0.0	0.	-0.	Ü.	A.0	0.0	Ű.	-u,	0.
1814142	14.8	88.	2 30	14.2	89.6	30.	89.	ø.	15.2	87.3	40.	174.	-5.	16.7	84.9	45.	201.	10.	0.0	0.0	0.	-0.	0.
1014202	14.9	37.	1 35	15.3	87.0	30.	25.	s.	16.5	84.8	19	89	-10.	17 6	02.5	45.	100	20	P.P	5. C	2	- 8 .	8.
1015022	14.9	86.	2 48	15.2	86.6	30.	29.	-10.	16.6	84.5	40.	101.	-10.	0.0	9.9	0.	0.	Ø.	0.0	6.0	9.	-0.	ø.
1015082	14.9	85.	4 46	14.9	85.7	40.	17.	0.	16.2	83.1	50.	59.	5.	0.0	0.0	0.	-0.	8	0.0	0.0	9.	0.	9.
1015142	15.2	84.	3 45	15.0	84.5	45.	17.	ø.	16.2	81.3	50.	36.	15.	8.6	6.8	e.	-0.	ø.	8.8	8.9	e.	-0.	ø.
101520Z	15.7	83.	5 50	15.2	83.1	45.	38.	-5.	17 3	79.6	25.	69.	0.	0.0	0.0	ø.	-8.	ñ.	0.0	0.0	9.	0.	ø.
1816022	16.2	82.	8 50	15.9	82.4	50.	29,	ø.	0.0	0.0		-0.	ø.	0.0	6.0	0.	-0.	0.	9.6	9.0	ø.	-0.	ø.
1016082	16.4	82.	1 45	16.5	81.5	58.	35.	5.	0.0	0.0	e.	-0.	ø.	0.0	0.0	e.	а.	ē.	0.0	0.0	ű.	- e.	3.
1016142	16.8	81.	4 35	17.2	B1.7	35.	30.	ø.	8.0	0.0	ø.	-0.	ø.	0.0	8.0	ø.	-ñ.	ø.	0.0	0.0	q.	ø.	ø.
1016202	17.2	80.	8 25	0.0	0.0	0.	-0.	0.	0.0	8.6	ø.	-0.	e.	0.0	0.0	ē.	-8.	ø.	0.0	0.0	n.	Э.	ø.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72~HR	WRIIG	24-HR	43-HR	72 HP		
AVG FORECAST POSIT ERROR	34.	88.	151.	6.	е.	ø.	в.	8.		
AVG RIGHT ANGLE ERROR	18.	49.	86.	0.	8.	0.	8.	0.		
AVG INTENSITY MAGNITUDE ERROR	3.	8.	15.	Θ.	0.	0.	0.	Я.		
AVG INTENSITY BIAS	-2.	-1.	15.	6.	e.	ø.	0.	ø.		
MIMBED OF EDDECASTS	۰	•	2		0					

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 681. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOT

TC23-02
FIX POSITIONS FOR CYCLUNE NO. 23

### SATELL ITE FIXES

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	120802	11.8N 94.2E	PCN 5	T1.5/1.5	INIT 085	KGUE
ż	122047	13.0N 92.7E		11,3, 113	11111 003	KGUC
3	130300	11.9N 93.6E		T1.0/1.0	THIT ORS	PGTU
4	130600	12.2N 92.5E		11.0-1.0	DLCC FIX	PGTW
5	130750	14.0N 91.7E		T2.0/2.0 /D0.5/24HRS	02 <b>02</b> / 3//	KGWC
6	132033	13.6N 91.4E		12.0.2.0 . 20.0.2		KGMC
7	140000	14. IN 91.1E			ULAC CIX	PI-TW
è	140300	14.1N 90.8E		T2.0/2.0-/D1.0/24HRS	ULAC 13.8N 89.2E	PG Ju
ğ	140600	14.0H 90.6E		11110-210 - 2110-2 11110	ULAC 13.7H 88.6E	PGTO
เคี	140900	14.8N 90.7E				PG+tM
11	140920	13.41 88.65		T2.5/2.5 /D0.5/25HRS		(SCU)C
* 12	141200	15.5N 87.0E				PG161
13	141600	15.2N 87.2E				PG 114
14	141060	15.3N 87.8E				PGTU
15	142190	15.3N 86.5E			ULCC FIX	PGTH
16	142205	14.7N 86.6E			ULAC FIX	KGUC
17	150000	15.4N 86.1E			ULAC FIX	PGTW
18	150300	14.7N 86.2E		T3.0/3.0 /D1.0/24HRS		PGTU
19	150600	14.8N 85.8E		73.0		PISTU
20	150900	14.8N 85.2E			ULOC FIX	PGTW
21	150900	14.7N 85.16		T1.5/2.5 /W1.0/24HRS		KGUC
22	151200	15.1N 84.6E		1010-010-010-010-0	ULCC FIX	ratu
23	151600	15.2N 03.5E				PGTW
24	151880	15.2N 83.1E				PGT⊎
25	152100	15.3N 82.6E				PGTW
26	152152	16.8N 83.5E				KGWC
27	160000	15.9N 82.5E				PGTW
28	160600	16.3N 82.2E		T3.0/3.8-/S0.0/27HRS		PGTW
29	160856	17.UN 82.7E		T1.5/1.5-/S0.0/24HRS	ULCC FIX	KGUC

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND HOT USED FOR BEST TRACK PURPOSES.

TROPICAL CYCLINE 24-82 BEST TRACK DATA

	BE	ST 1	RACK			WARNI		RURS		24 H	UR FO	RECA!			48 H	OUR FO	RECA FPRO			72 H	OUR FO	RECAS	
MO/DA/HR	POSIT	L.	IND	POS	IT	MIND	PST	WIND	POS	IT	MIHD	DST	WIND	1'05	ΙT	MIND	DST	MIND	FUS	t T	WIND	DST	MIND
101700Z	10.4 8	33.7	30	0.0	0.0	0.	~⊎.	0.	0.0	6.6	0.	-8.	0.	0.0	0.0	P.	-0.	0.	0.0	6.0	8.	-0.	ø.
1817142	11.0 8	33.0	35	10.9	83.6	30.	36.	-5.	13.4	81.2	45.	50.	-5.	0.0	0.A	Θ.	- 9.	0.	0.0	0.0	8.	-0.	ø.
101720Z	11.6 B	32.2	40	11.8	82.4	40.	17.	0.	14.2	80.4	50.	58.	5.	0.0	0.0	ē.	-0.	ø.	9.0	0.0	0.	-0.	ø.
1019022	12.1 8	91.6	45	12.1	82.2	45.	35.	Ð.	14.2	80.4	50.	88.	20.	0.0	0.0	Ä.	-0.	ø.	6.6	0.0	ä.	-8.	Ä.
181909Z	12.9 8	11.1	45	12.8	81.7	50.	36.	5.	0.0	8.0	A.	-0.	e.	0.8	6.8	Ř.	-8.	ē.	8.8	8.8	я.	-0.	8.
1818142	13.8	99.3	50	13.8	80.2	58.	6.	ø.	0.0	6.8	ø.	-0.	A.	11.0	0.0	ø.	-0.	Ø.	0.0	0.0	ø.	-0.	ø.
1018202	14.6 7	9.5	45	14.5	79.6	45.	B.	ē.	0.0	0.0	0.	-0.	e.	Ð.0	0.0	ě.	ē.	ø.	0.0	0.0		-0.	ø.
1819022		9.2	30	14.9	79.4	30.	17.	ø.	0.0	P.0	ø.	-0.	ě.	0.0	a.e	e.	~0.	ē.	0.0	8.0	0.	-ð.	ø.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	7?-HR	WRNG	24-HR	48 11R	72-HR		
AVG FORECAST POSIT ERROR	22.	68.	0.	0.	ø.	ø.	ø.	e.		
AVG RIGHT ANGLE ERROR	15.	22.	0.	0.	0.	3.	ø.	ø.		
AVG INTENSITY MAGNITUDE ERROR	1.	10.	0.	в.	٥.	ø.	ย.	ø.		
AVG INTENSITY BIAS	0.	7.	Θ.	0.	θ.	ø.	ø.	ø.		
NUMBER OF FORECASTS	7	Ś	0	9	Ø	0	ø	Ø		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 389. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

9. KNNTS

TC24-82
FIX POSITIONS FOR CYCLONE NO. 24

### SATELLITE FROS

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DYDRAK CODE	COMENTS	SIIE
* 1 * 2 * 3 4 5 6	150908 160856 162140 170843 172129 180831	7.6N 88.0E 9.2N 83.0E 10.9N 84.2E 10.5N 83.5E 11.0N 81.3E 12.9N 80.1E	PCH 5 PCH 6 PCH 5 PCH 6	T1.5/1.5 T2.8/2.0 /D0.5/2/HRS T2.5/2.5 /D0.5/24HRS 13.8/3.8-/D0.5/24HRS	INIT OUS ULCC FIX ULCC FIX ULCC FIX ULCC IN.ON 81,4E ULGC IIX	KGWE KGWE KGWE KGWE KGWE KGWE

### SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	HEAREST DATA (NM)		COMMENTS
1	181588	14 AN 80 AF	945	ครด	LIMINA 3079	

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TROPICAL CYCLONE 25-82 BEST TRACK DATA

		BEST	TRACK			WARN				24 H	WR F	DRECAS			48 H	OUR FO				72 HC			
								RORS				Fiski					ERRO					RRURS	
MO/DA/HR	POSI	T	MIND	POS	ĮΤ	MIND	DST	MIND	POS	IT	W!HD	DST	MIND	POS	IŤ	MIHD	DST	MIND	POS	IT.	MIND	DST	MIND
110414Z	11.1	63.5	<b>20</b>	6.0	0.0	8.	-0.	9.	0.0	9.0	0.	-8.	8.	8.8	8.8	0.	-0.	0.	0.0	0.0	0.	-0.	8.
110420Z	11.3	63.6	25	0.0	0.6	0.	-8.	0.	9.8	0.0	Ø.	-8.	Ø.	0.0	0.0	Đ.	-0.	e.	9.8	0.0	ø.	-Ð.	0.
1105022	11.8	63.5	30	11.0	62.7	35.	67.	5.	12.6	59.9	40.	294.	5.	13.7	56.9	50.	503.	-5	15.7	54.2	55.	919.	- 25.
1105082	12.1	63.6	32	11.5	62.B	30.	69.	ø.	12.3	68.8	46.	273.	ē.	13.2	58.0	50.	582.	-10.	14.8	55.1	55.		-35.
110514Z	12.4	64.2	39	12.5	63.2	30.	59.	B.	14.1	61.4	40.	251.	-5.	15.2	59.2	45.	539.	- 20	16.3	56.9	35.	887.	-45.
110520Z	12.7	64.5	5 30	12.0	63.0	30.	97.	ø.	13.0	62.7	35.	223.	-15.	14.7	60.8	40.	513.	- 30.	15.8	58.6		884	25.
110602Z	13.1	64.9	35	14.2	62.8	35.	139.	ě.	16.4	68.5	45.	370.	-18.	18.1	58.0	50.	675.	- s8.	19.2	56.0	31.1	B22.	-5.
110608Z	13.5	65.3	3 40	14.0	62.2	35.	183.	-5.	15.7	59.6	45.	4'57		17.5	57.2	50.	275.	-46.	9 9	6.0	A.	-0.	ē.
1186142	13.9	65.7		13.6	65.8	45.	8.	ø.	15.9	67.6	55.	99	-10.	18.7	69.1	68.	220.	-20.	0.0	0.0	0.	-0.	ø.
1106202	14.5	66.2	50	14.3	66.2	50.	12.	0.	16.7	68.0	55.	109.	-15.	19.6	69.5	65.	238.	5.	0.6	0.0	e.	-8.	0.
1107027	15.3	66.6		14.9	66.6	68.	27.	= -	17.7	60.2	75.	168			69.8			20.			Ξ.		Ξ.
							• • •	5.	17.2	••••			-5.	20.4		60.	261.		6.0	9.0	₹.	-0.	ø.
1107082	16.3	67.5		15.4	67.8	60.	61.	Θ.	17.8	68.8	75.	160.	-15.	6.0	0.0	в.	-0.	0.	0.8	0.0	0.	-0.	0.
1107142	17.3	68.3	65	17.1	68.1	65.	17.	ø.	21.1	71.6	69.	41.	-29.	0.0	0.0	Ø.	- 6.	9.	8.6	9.6	0.	-0.	₽.
1107202	18.3	60.5		10.0	68.8	65.	19.	-5.	22.1	71.6	55.	57.	-5.	0.0	0.8	0.	-0.	e.	9.0	8.0	θ.	-0.	θ.
1108022	19.4	69.6	88	19.1	69.1	65.	44.	-15.	23.0	71.4	45.	142.	5.	9.0	8.8	Θ.	-Ð.	Θ.	0.0	0.0	9.	-0.	0.
110808Z	20.5	70.5	5 90	20.0	69.3	60.	74.	-30.	0.0	0.0	8.	-0.	٥.	0.0	0.0	€.	-8.	0.	9.0	0.0	0.	-0.	0.
11 <b>0</b> 814Z	21.6	71.5	5 60	21.3	71.2	80.	25.	8.	8.0	0.0	0.	~8.	6.	0.0	0.0	Ø.	-A.	٥.	0.8	0.0	Θ.	-8.	0.
1100202	22.3	72.6	68	22.2	72.1	65.	28.	5.	0.6	0.0	0.	-0.	ø.	8.8	8.8	e.	-0.	Ð,	8.8	9.0	0.	-0.	8.
110902Z	22.5	73.9	40	22.4	73.7	40.	13.	0.	0.8	0.8	₽.	-0.	P.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KIS					
	WRNG	24-HR	48-HR	72-HR	WRIG	7:1-HR	48 HR	72-HR		
AVG FORECAST POSIT ERROR	55.	205.	487.	931.	0.	Ð.	ø.	0.		
AVG RIGHT ANGLE ERROR	34.	113.	264.	519.	0.	6.	₿.	8.		
AVG INTENSITY MAGNITUDE ERROR	4.	10.	20.	27.	0.	0.	٥.	8.		
AVG INTENSITY BIRS	-2.	-8.	-14.	-27.	0.	0.	0.	0.		
NUMBER OF FORECASTS	17	13	9	5	8	8	ė	8		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 949. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

TC25-82
FIX POSITIONS FOR CYCLONE NO. 25

### SATELLITE FIXES

	1× 10.	TIME (Z)	FIX POSITIO		ACCRY	DVORAK CODE	CONTENTS	SITE
*	1	032307	12.5N 6	56.1E	PCN 5		ULAC 11.5N 66.4E	KGUC
*	2	841018	12.3N 6	52.4E	PCN 5	T2.5/2.5+/D1.5/24HRS	ULAC 12.3N 61.6E	KGUC
*	3	042255	10.6N 6	52.3E	PCN 5		ULAC 11.41 62.6E	KGWC
	4	050958	12.1N 6	53.3E	PCN 5	T3.0/3.0 /D0.5/24HRS	ULAC 12.9H 62.6E	KGWC
*	5	852243	14.0N 6	53.2E	PCN 5		ULAC 12.3N 63.8E	KGUC
	6	868946	13.3N 6	55.7E	PCN 5	T3.8/3.8 /S8.8/24RS	ULOC 12.5N 64.4E	Kern.
	7	062231	14.5N 6	56.3E	PCN 5			KGLIC
	8	979934	16.4N 6	57.7E	PCN 5	T3.5/3.5 /D0.5/24IRS	ULAC 16.8N 78.3E	KGWC
	9	072218	18.5N 6	58.9E	PCH 5		ULAC 18.5N 69.3E	KGUC
	10	080921	20.6N 7	70.6E	PCN 1		EYF DIA 24HT	KGWC

### SYNOPTIC FIXES

	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	CONTENTS
841288	11. <b>0</b> N 64.26	020	818	SHIP DBSFRVATION
060600	14.0N 62.2E	646	696	SHIP DOSERVATION
081500	21.8N 71.7E	868	968	UHD 42737
090000	22.3N 73.3E	646	86A	UPID 42647
	060600 081500	(Z) POSÍTION 841298 11.8N 64.2E 969698 14.8N 62.2E 981598 21.8N 71.7E	(Z) POSÍTION ESTINATE  041200 11.8N 64.2E 028 060600 14.0N 62.2E 848 081500 21.0N 71.7E 068	(Z) POSITION ESTINATE DATA (NH)  841296 11.8N 64.2E 828 818 868680 14.0N 62.2E 848 998 891598 21.8N 71.7E 868 968

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

# APPENDIX I

ACCRY	Accuracy	GOES	Geostationary Operational Environmental Satellite
ACFT	Aircraft	HATTRACK	Hurricane and Typhoon Tracking
ADP	Automated Data Processing		(Steering) Program
AFGNC	Air Porce Global Weather Central	HGT	Height
AIREP	Aircraft Weather Report(s) (Commerical and Military)	HPAC	Mean of XTRP and CLIM Techniques (Half Persistence and Climatology)
ANT	Antenna	HR	Hour(s)
AOR	Area of Responsibility	HVY	Heavy
APRNT	Apparent	ICAO	International Civil Aviation Organization
APT	Automatic Picture Transmission	INIT	Initial
ARWO	Aerial Reconnaissance Weather Officer	INJAH	North Indian Ocean Component
ATT	Attenuation		of TYAN
AVG	Average	INST	Instruction
AWN	Automated Weather Network	IR	Infrared
BPAC	Blended Persistence and Climatology	KM	Kilometer(s)
BRG	Bearing	KM/HR	Kilometer(s) per Hour
CDO	Central Dense Overcast	КT	Knot(s)
CI	Cirriform Cloud or Cirrus	LLCC	Low-level Circulation Center
	also Current Intensity (Dvorak)	LVL	Level
CINCPAC	Commander-in-Chief Pacific AF - Air Force, FLT - Fleet (Navy)	М	Meter(s)
CLD	Cloud	M/SEC	Meter(s) per Second
CLIM	Climatology	MAX	Maximum
CLSD	Closed	МВ	Millibar(s)
СМ	Centimeter	MET	Meteorological
CNTR	Center	MIN	Minimum
CPA	Closest Point of Approach	MOHATT	Modified HATTRACK
CSC	Cloud System Center	MOVG	Moving
CYCLOPS	Tropical Cyclone Steering Program	MSLP	Minimum Sea Level Pressure
C.C.D. D	(HATTRACK and MOHATT)	MSN	Mission
DEG	Degree (s)	NAV	Navigational
DIAM	Diameter	NEDN	Naval Environmental Data Network
DIR	Direction	NEDS	Naval Environmental Display Station
DMSP	Defense Meteorological Satellite Program	NEPRF	Naval Environmental Prediction Research Facility
EL	Elongated	NESS	National Environmental Satellite Service
ELEV	Elevation	NET	Near Equatorial Trough
EXP	Exposed	NET NM	Nautical Mile(s)
FI	Forecast Intensity (Dvorak)	N/O	Not Observed
FLT	Flight	•	
PNOC	Fleet Numerical Oceanography Center	NOAA	National Oceanic and Atmospheric Administration
FT	Feet (Foot)	NOCC	Naval Oceanography Command Center
GMT	Greenwich Mean Time	NWOC	Naval Western Oceanography Center

NR	Number	TC	Tropical Cyclone
NRL	Naval Research Laboratory	TCARC	Tropical Cyclone Aircraft
NTCM	Nested Tropical Cyclone Model		Reconnaissance Coordinator
OBS	Observation(s)	TCFA	Tropical Cyclone Formation Alert
OTCM	One-way (Interactive) Tropical	TCM	Tropical Cyclone Model
	Cyclone Model	TD	Tropical Depression
PACOM	Pacific Command	TDO	Typhoon Duty Officer
PCN	Position Code Number	TIROS	Televison Infrared Observation
PSBL	Possible	m.c	
PTLY	Partly	TS	Tropical Storm
QUAD	Quadrant	TY	Typhoon
RADOB	Radar Observation(s)	TYAN	Typhoon Analog Program
RECON	Reconnaissance	TYFN	Western North Pacific Component (Revised) of TYAN
RNG	Range	TUTT	Tropical Upper-Tropospheric Trough
RT	Right	ULAC	Upper-level Anticyclone
SAT	Satellite	VEL	Velocity
SFC	Surface	VIS	Visual
SLP	Sea Level Pressure	VSBL	Visible
SPOL	Spiral Overlay	WESTPAC	Western (North) Pacific
SRP	Selective Reconnaissance Program	WINO	World Meteorological Organization
STNRY	Stationary	WND	Wind
SST	Sea Surface Temperature	WRNG(S)	Warnings
ST	Subtropical	WRS	Weather Reconnaissance Squadron
STR	Subtropical Ridge	XTRP	Extrapolation
STY	Super Typhoon	z	Zulu Time
TAPT	Typhoon Acceleration Prediction Technique		(Greenwich Mean Time)

### APPENDIX II

### **DEFINITIONS**

BEST TRACK - A subjectively smoothed path, versus a precise and very erratic fix-to-fix path, used to represent tropical cyclone movement.

CENTER - The vertical axis or core of a tropical cyclone. Usually determined by wind, temperature, and/or pressure distribution.

CYCLONE - A closed atmospheric circulation rotating about an area of low pressure (counterclockwise in the Northern Hemisphere).

EPHEMERIS - Position of a body (satellite) on space as a function of time; used for gridding satellite imagery. Since ephemeris gridding is based soley on the predicted position of the satellite, it is susceptible to errors from vehicle pitch, orbital eccentricity, and the oblateness of the earth.

EXPLOSIVE DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 2.5 mb/hr for 12 hrs or 5.3 mb/hr for six hrs (ATR 1971).

EXTRATROPICAL - A term used in warnings and tropical summaries to indicate that a cyclone has lost its "tropical" characteristics. The term implies both poleward displacement from the tropics and the conversion of the cyclone's primary energy sources from release of latent heat of condensation to baroclinic processes. The term carries no implications as to strength or size.

EYE - "EYE" is used to describe the central area of a tropical cyclone when it is more than half surrounded by wall cloud.

FUJIWHARA EFFECT - An interaction in which tropical cyclones within about 700 nm (1296 km) of each other begin to rotate about one another. When intense tropical cyclones are within about 400 nm (741 km) of each other, they may also begin to move closer to each other.

MAXIMUM SUSTAINED WIND - Maximum surface wind speed averaged over a one-minute period of time. Peak gusts over water average 20 to 25 percent higher than sustained winds.

RAPID DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 1.25 mb/hr for 24 hrs (ATR 1971).

RECURVATURE - The turning of a tropical cyclone from an initial path toward the west or northwest to a path toward the northeast.

RIGHT ANGLE ERROR - The distance described by a perpendicular line from the best track to a forecast position. (See Figure 4-1).

SIGNIFICANT TROPICAL CYCLONE - A tropical cyclone becomes "significant" with the issuance of the first numbered warning by the responsible warning agency.

SUPER TYPHOON/HURRICANE - A typhoon/hurricane in which the maximum sustained surface wind (one-minute mean) is 130 kt (67 m/sec) or greater.

TROPICAL CYCLONE - A non-frontal low pressure system of synoptic scale developing over tropical or subtropical waters and having a definite organized circulation.

TROPICAL CYCLONE AIRCRAFT RECONNAISSANCE
COORDINATOR - A CINCPACAF representative
designated to levy tropical cyclone aircraft
weather reconnaissance requirements on
reconnaissance units within a designated area
of the PACOM and to function as coordinator
between CINCPACAF, aircraft weather reconnaissance units, and the appropriate typhoon/
hurricane warning center.

TROPICAL DEPRESSION - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 33 kt (17 m/sec) or less.

TROPICAL DISTURBANCE - A discrete system of apparently organized convection--generally 100 to 300 nm (185 to 556 km) in diameter-originating in the tropics or subtropics, having a non-frontal migratory character, and having maintained its identity for 24 hours or more. It may or may not be associated with a detectable perturbation of the wind field. As such, it is the basic generic designation which, in successive stages of intensification, may be classified as a tropical depression, tropical storm or typhoon (hurricane).

TROPICAL STORM - A tropical cyclone with maximum sustained surface winds (one-minute mean) in the range of 34 to 63 kt (17 to 32 m/sec) inclusive.

TROPICAL UPPER-TROPOSPHERIC TROUGH (TUTT)"A dominant climatological system, and a daily synoptic feature, of the summer season over the tropical North Atlantic, North Pacific and South Pacific Oceans," from - Sadler, J.C., Feb. 1976: Tropical Cyclone Initiation by the Tropical Upper-Tropospheric Trough (NAVENVPREDRSCHFAC Technical Paper No. 2-76).

TYPHOON/HURRICANE - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 64 kt (33 m/sec) or greater. West of 180 degrees longitude they are called typhoons and east of 180 degrees they are called hurricanes. Foreign governments use these or other terms for tropical cyclones and may apply different intensity criteria.

VECTOR ERROR - The distance described by a straight line from the forecast position to the position at verification time as found on the best track. (See Figure 4-1).

WALL CLOUD - A organized band of cumuliform clouds immediately surrounding the central area of a tropical cyclone. The wall cloud may entirely enclose or only partially surround the center.

# APPENDIX III NAMES FOR TROPICAL CYCLONES

Column 1	Column 2	Column 3	Column 4
ANDY	ABBY	ALEX	AGNES
BESS	Ben	BETTY	BILL
CECIL	CARMEN	CARY	CLARA
DOT	DOM	DINAH	DOYLE
ELLIS	RLLEN	RD	ELSIE
FAYE	FORREST	PREDA	FABIAN
GORDON	GEORGIA	GERALD	GAY
HOPE	HERBERT	HOLTA	HAZEN
IRVING	IDA	IKE	IRMA
JUDY	JOE	JUNE	JEFF
KEN	KIM	KEITA	
LOLA			KIT
	LEX	LYNN	LEE
MAC	Marge	MAURY	MAMIE
NANCY	NORRIS	NINA	nelson
OWEN	ORCHID	OGDEN	ODESSA
PAMELA	PERCY	PHYLLIS	PAT
ROGER	RUTH	ROY	RUBY
SARAH	SPERRY	SUSAN	SKIP
TIP	THELMA	THAD	TESS
VERA	VERNON	VANESSA	VAL
WAYNE			
WAINE	WYNNE	WARREN	WINONA

### NOTE:

Names are assigned in rotation, alphabetically. When last name (WINONA) has been used, the sequence will begin again with "ANDY."  $\,$ 

Source: CINCPACINST 3140.1 (series)

### APPENDIX IV

### REFERENCES

- Atkinson, G. D., and C. R. Holliday, 1977: Tropical Cyclone Minimum Sea Level Pressure - Maximum Sustained Wind Relationship for the Western North Pacific. Monthly Weather Review, Vol. 105, No. 4, pp. 421-427.
- Dunnavan, G. M., 1981: Forecasting Intense Tropical Cyclones Using 700 MB Equivalent Potential Temperature and Central Sea Level Pressure. NAVOCEANCOMCNE/JTWC TECH NOTE: JTWC 81-1, 12 pp.
- Dvorak, V. F., 1973: A Technique for the Analysis and Forecasting of Tropical Cyclone Intensities from Satellite Pictures. NOAA Technical Memorandum NESS 45, 19 pp.
- Herbert, P. H., and K. O. Poteat, 1975: A Satellite Classification Technique for Subtropical Cyclones. NOAA Technical Memorandum NWS SR-83, 25 pp.
- Holland, G. J., 1980: An Analytic Model of the Wind and Pressure Profiles in Hurricanes.

  Review, Vol. 108, No. 8, pp. 1212-1218.
- Huntley, J.E., and J. W. Diercks, 1981: The Occurrence of Vertical Tilt in Tropical Cyclones. Monthly Weather Review, Vol. 109, No. 8, pp. 1689-1700.
- Sadler, J. C., 1976: Tropical Cyclone Initiation by the Tropical Upper-Tropospheric Trough. NAVENVPREDRSCHFAC Technical Paper No. 2-76, 103 pp.
- Sikora, C. R., 1976: An Investigation of Equivalent Potential Temperature as a Measure of Tropical Cyclone Intensity. FLEWEACEN TECH NOTE: JTWC 76-3, 12 pp.
- Weir, R. C., 1982: Predicting the Acceleration of Northward-moving Tropical Cyclones Using Upper-Tropospheric Winds. NAVOCEANCOMCEN/JTWC TECH NOTE: NOCC/JTWC 82-2.

# APPENDIX V PAST ANNUAL TYPHOON/TROPICAL CYCLONE REPORTS

Copies of the past Annual Typhoon Reports can be obtained through:

National Technical Information Service 5285 Port Royal Road Springfield, Virginia 22161

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## ANNUAL TROPICAL CYCLONE REPORT (ATCR) EVALUATION SURVEY

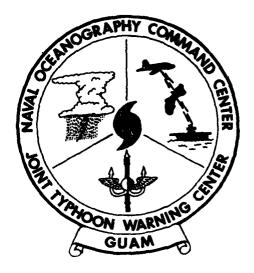
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